

INRIA Contribution  
3<sup>rd</sup> AIAA Sonic-Boom workshop

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## Near field cases:

bi-convex      provided-unstructured (not presented)  
c608            provided-unstructured and **adaptive grids**

## Improvements from previous workshops :

- ⇒ Only **RANS** computations
- ⇒ Fully adaptive unstructured boundary layer

## General context

- Tetrahedral meshes only
- Parallel computation 24 cores (48 threads), Xeon E7 , 128-512Gb
- Error estimate [Alauzet & Loseille, JCP 2008], [Loseille et al., JCP 2010]  
multi-scale (**Lp**)    interpolation error    Mach number

[Alauzet & Loseille, JCP 2012], [Menier et Al., AIAA 2014], [Frazza et al., AIAA 2018]

## Compressible Turbulent Navier-Stokes flow solver:

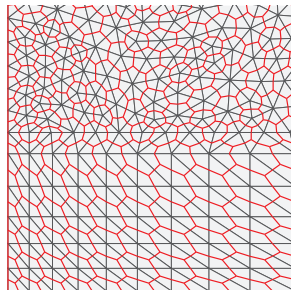
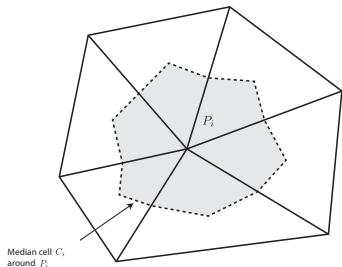
- Turbulence models: [Spalart-Allmaras](#)
- Full [unstructured tetrahedra](#)/hybrid meshes
- [Mixed-Element-Volume Method](#):
  - Convective and source terms by Finite Volume method
  - Diffusive terms by Finite Elements method or Edge Based viscous formulation
- Vertex centered: low complexity
  - [Median cells](#)
  - Containment sphere cells
- Edge-based fluxes computation with a 2<sup>nd</sup> order scheme using MUSCL reconstructions.
- [Full differentiation](#) with first order matrix.

## Compressible Turbulent Navier-Stokes Equations:

$$\frac{\partial W}{\partial t} + \nabla \cdot \mathcal{F}(W) = \mathcal{S}(W) + \mathcal{Q}(W)$$

Finite volume solution discretization:  $W_i = \frac{1}{|C_i|} \int_{C_i} W \, d\Omega$

$$|C_i| \frac{\partial W_i}{\partial t} = \int_{\partial C_i} \mathcal{F}(W) \, d\Gamma + \int_{C_i} \mathcal{S}(W) + \mathcal{Q}(W) \, d\Omega$$



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## Mixed-Element-Volume Method (MEV):

- Convective terms by Finite Volume method: Upwinding
- Diffusive terms by Finite Element method: Elliptic

**Vertex-centered:** low complexity, edge structure, extrapolation

Solve on each FV cell:  $|C_i| \frac{dW_i}{dt} + \mathbf{F}_i - \mathbf{S}_i - \mathbf{Q}_i = R_i$

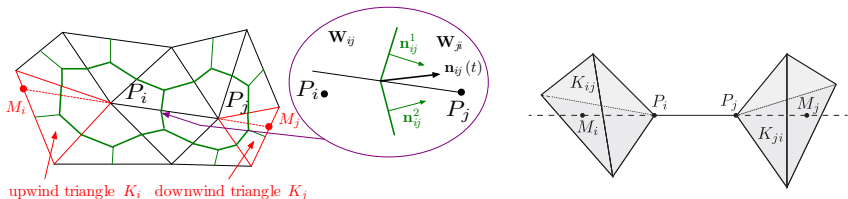
## Convective flux:

$$\mathbf{F}_i = \sum_{j \in \mathcal{V}(i)} F_{|\partial C_{ij}} \cdot \int_{\partial C_{ij}} \mathbf{n}_i d\Gamma = \sum_{j \in \mathcal{V}(i)} \Phi_{ij}(W_i, W_j, \mathbf{n}_{ij})$$

- $\Phi_{ij}$  with Riemann solvers: mainly **HLLC**, other available Roe, Van Leer, ...

**2<sup>nd</sup> order** scheme using a MUSCL-like reconstruction at the cell interface:

- **Low dissipation** reconstruction: V3-scheme, V4-scheme, V6-scheme  
Combination of centered, upwind-downwind, nodal gradients
- Limiters: Dervieux/Piperno for low dissipation, all the usual for V3-scheme



Element-based classical FEM formulation for viscous terms

$$\int_{\partial C_i} \mathbf{S}(W_i) \cdot \mathbf{n} \, d\Gamma = \sum_{P_j \in \mathcal{V}(P_i)} \int_{\partial C_{ij}} \mathbf{S}(W_i) \cdot \mathbf{n} \, d\Gamma = - \sum_{K \ni P_i} \int_K \mathbf{S}(W_i)|_K \cdot \nabla \phi_i \, d\mathbf{x}.$$

Turbulence model discretization:

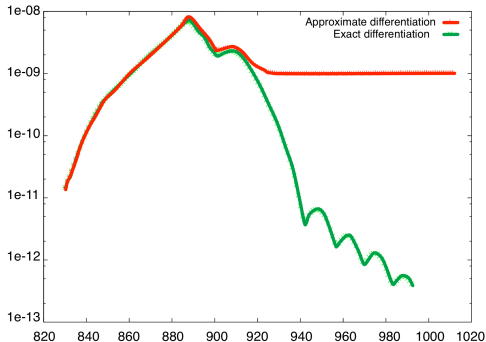
- Convective term: linear or non-linear convection
- Diffusive and dissipative terms: FEM formulation
- Production and destruction terms: FV source term formulation

**Accurate differentiation yields better results than approximate differentiation.**

**Convective fluxes**  $\frac{\partial \mathbf{F}_i^n}{\partial W_i}$  : Full first order differentiation (no MUSCL, no limiter). Differentiate HLLC solver !

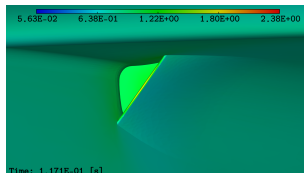
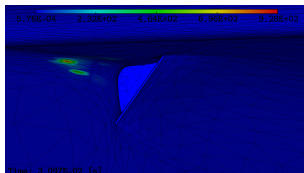
**Viscous fluxes**  $\frac{\partial \mathbf{S}_i^n}{\partial W_i}$  : Direct finite elements differentiation. Do not use spectral radius approximations !

**Turbulent source terms**  $\frac{\partial \mathbf{Q}_i^n}{\partial W_i}$  : Care for non-linearities.

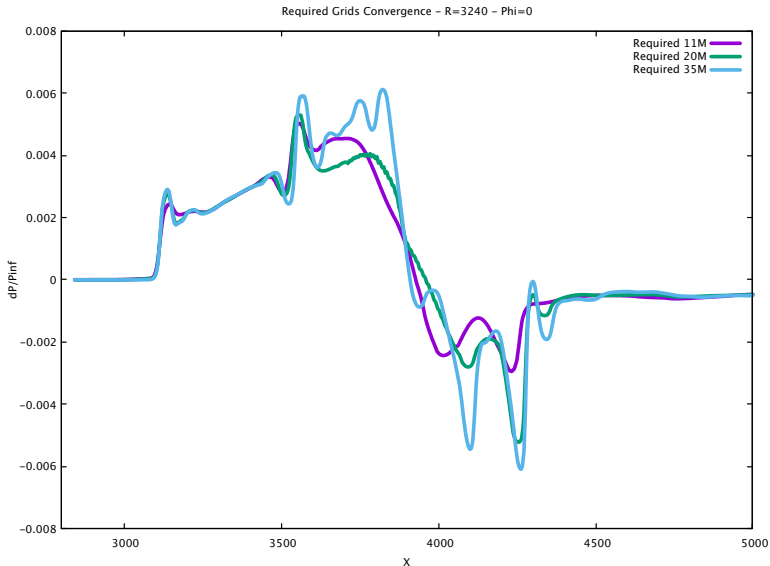


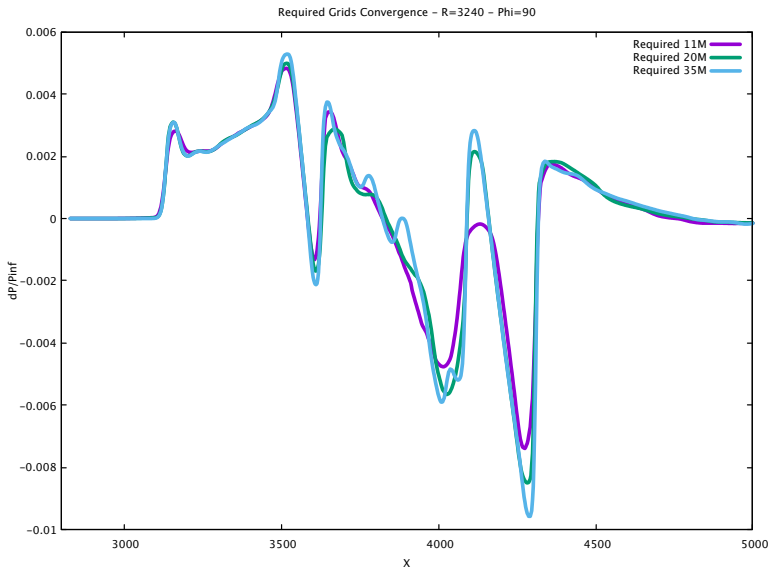


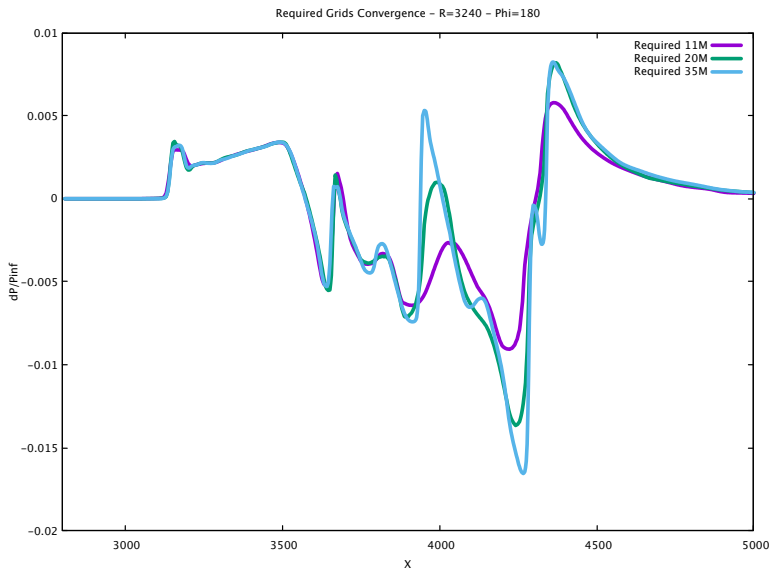
- All cases are initialised with first order solution and then second order
- All computations are using 4-th order dissipation terms.
- Issues with the boundary condition (ECS)



- 4 orders of magnitude reduction in the residual
- Limited to 30 million nodes grids







## Feature-based anisotropic mesh adaptation

Deriving the best mesh to compute the characteristics of a given solution  $w$

[Tam et al., CMAME 2000], [Pain et al., CMAME 2001], [Picasso, SIAMJSC 2003], [Formaggia et al., ANM 2004], [Bottasso, IJNME 2004], [Li et al., CMAME 2005], [Frey and Alauzet, CMAME 2005], [Gruau and Coupez, CMAME 2005], [Huang, JCP 2005], [Compere et al., 2007], ...

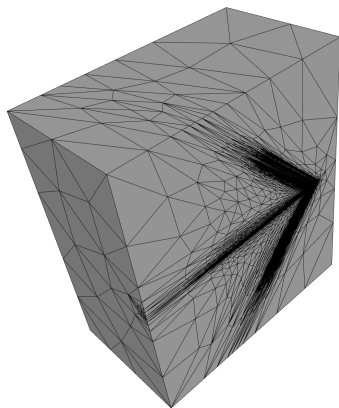
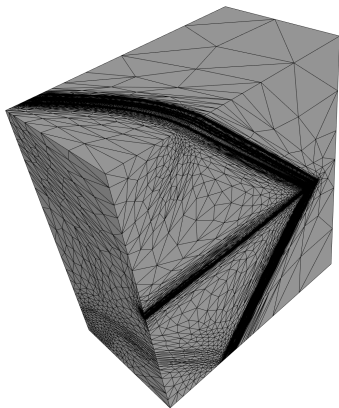
## Multiscale anisotropic mesh adaptation

[Loseille et al., AIAA 2007], [Alauzet, IJNMF 2008]

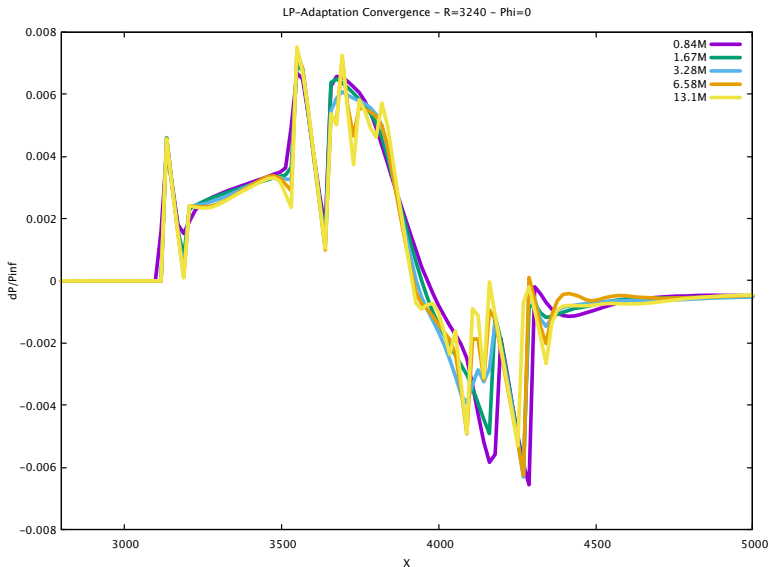
- Optimal control of the interpolation error in  $L^p$  norm :

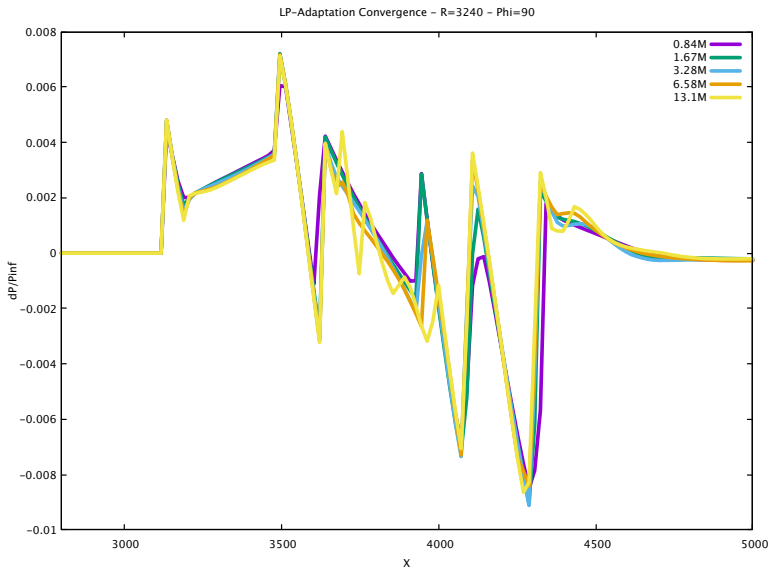
$$\|W - \Pi_h W\|_{L^p(\Omega_h)}$$

- Solve this problem in the continuous framework  $\implies \mathcal{M}_{L^p}(H_W)$
- Highly anisotropic meshes
- Capture all scales of the flow
- Global  $2^{nd}$  of mesh convergence for the mesh adaptation process
- Early capturing property: asymptotic convergence is reached faster

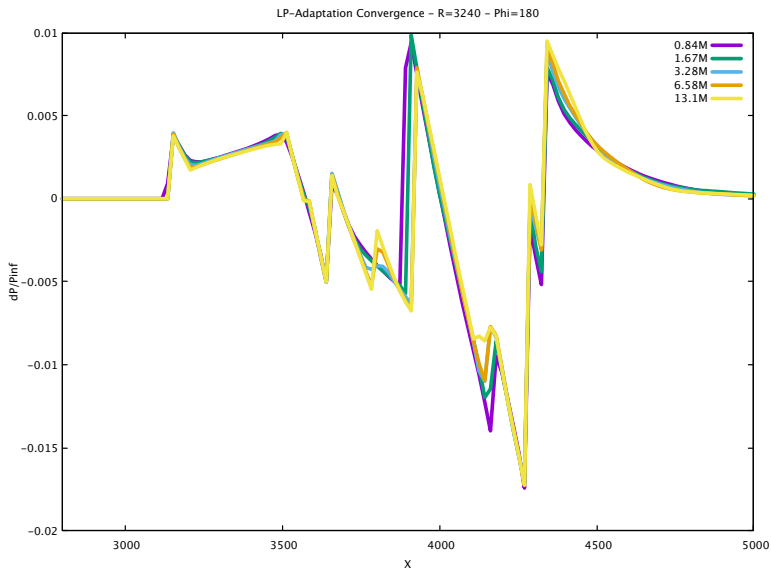


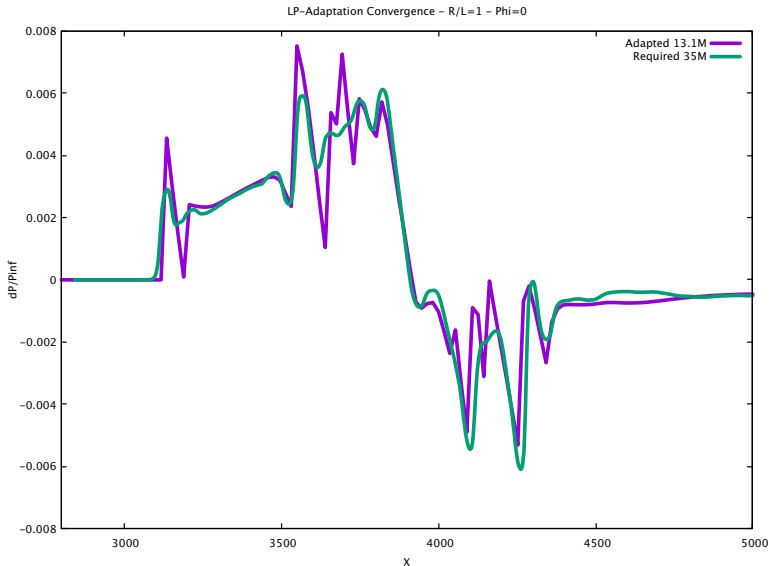
- Hessian anisotropic diffusion for  $R > 4000$
- 5 adaptations are performed at fixed complexity from 200000 to 1280000

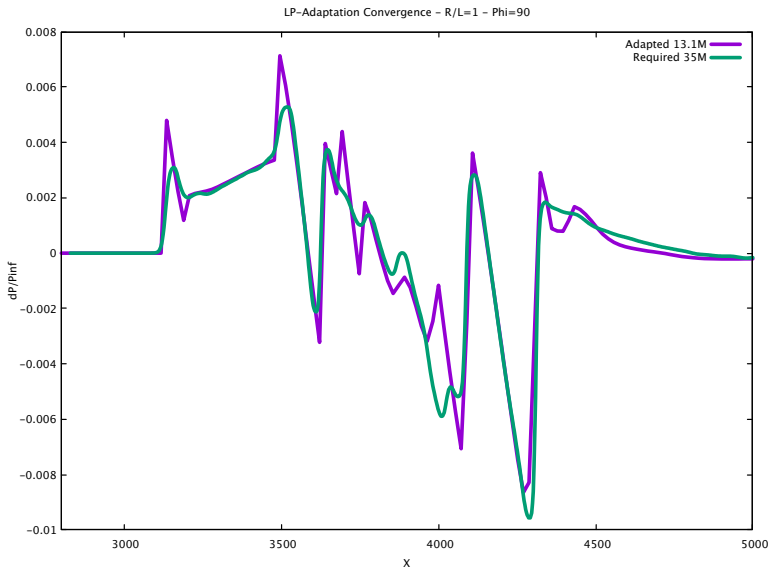


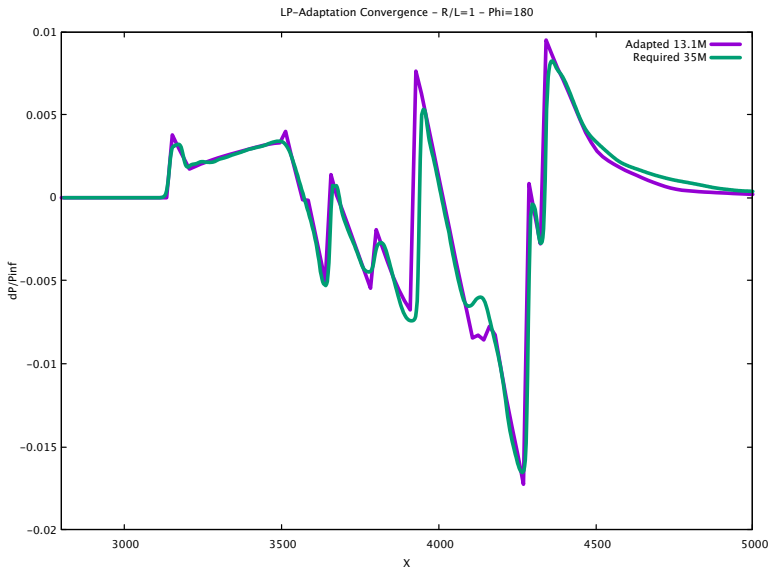


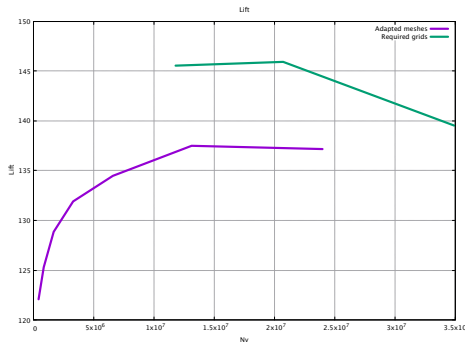
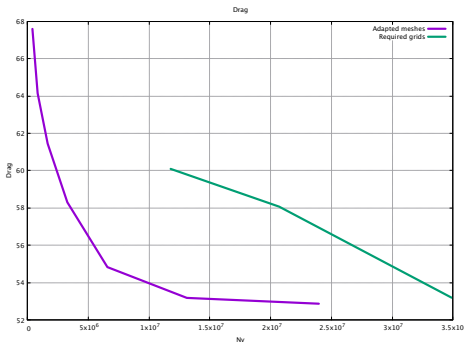


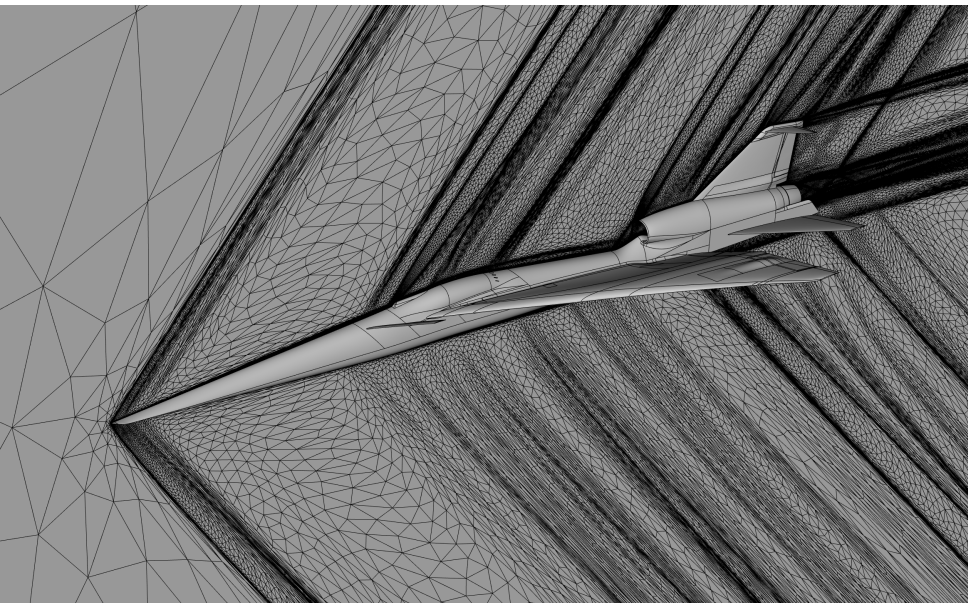


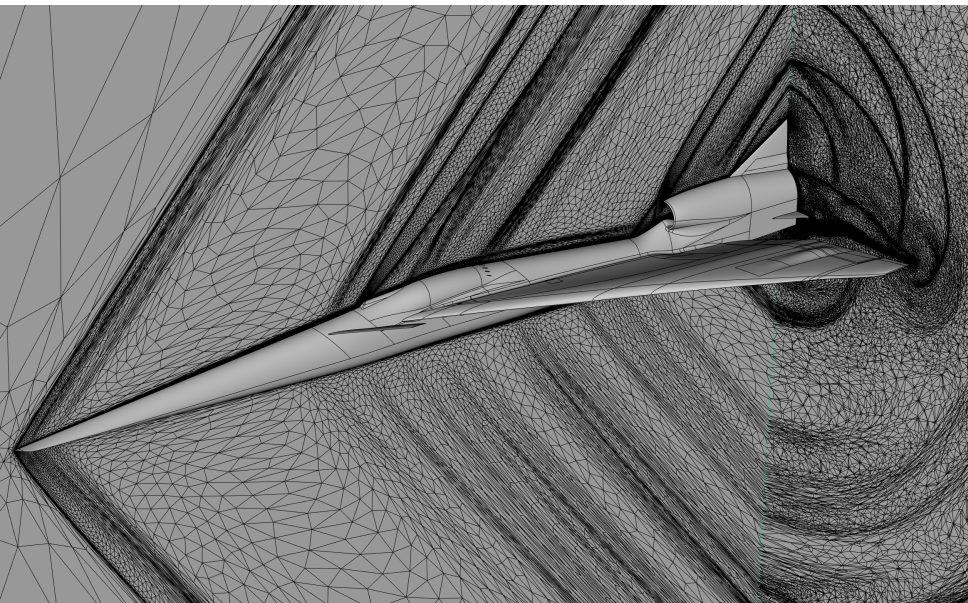


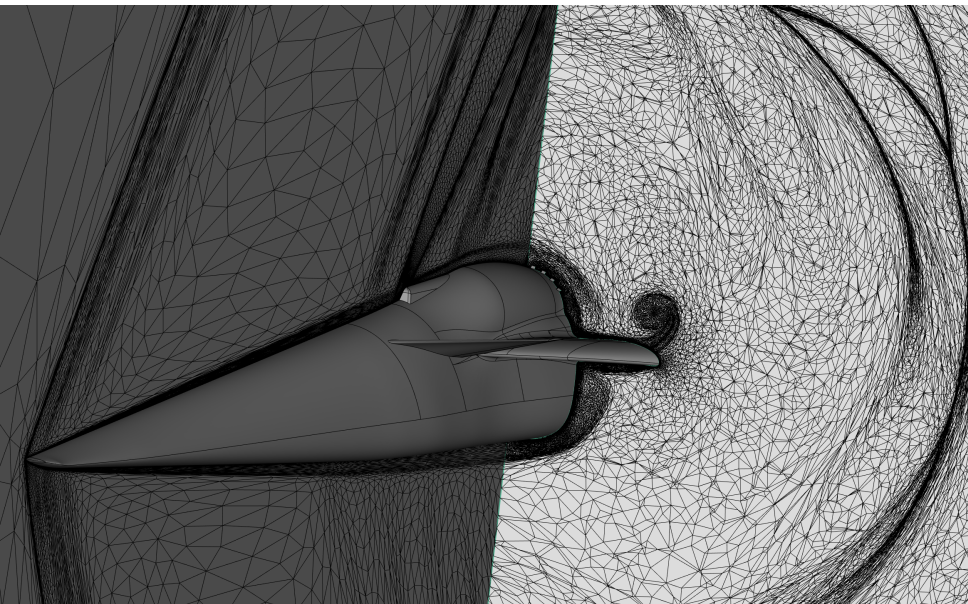




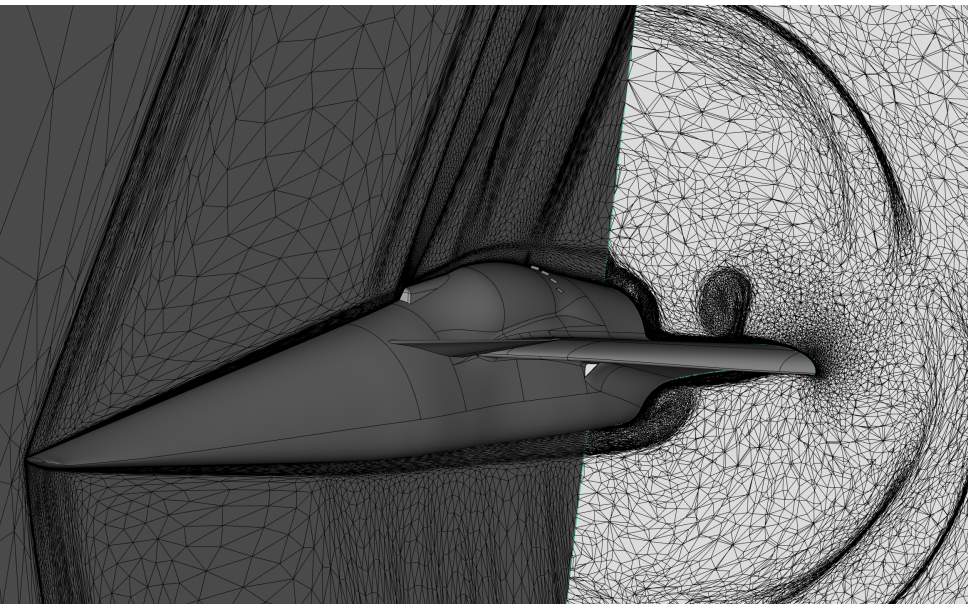


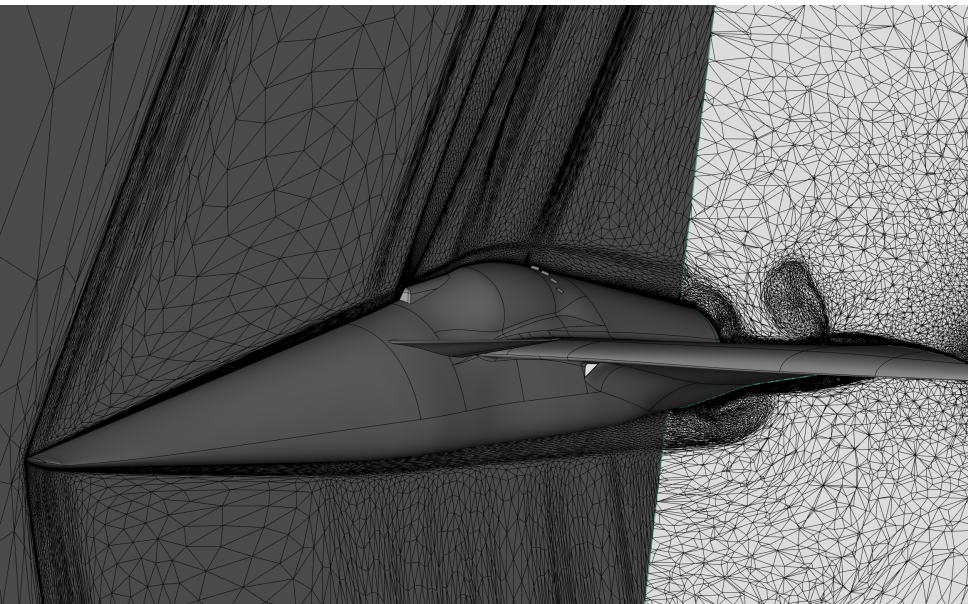


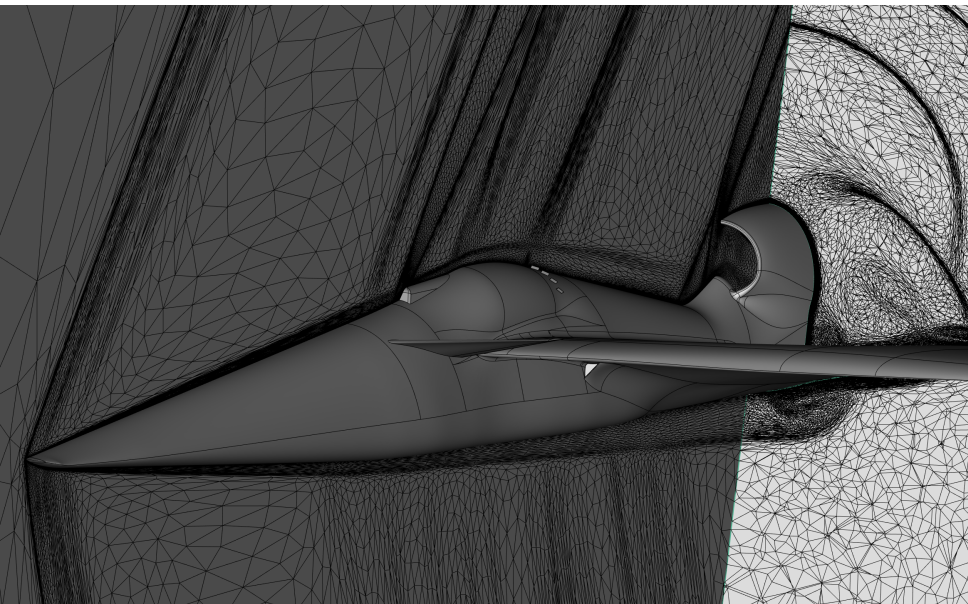












## Improvements over the previous workshops

- Powered conditions (Inflow/outflow)
- Fully RANS adaptivity
- CAD/Surface adaptivity

## On-going work/Current limitations

- Distributed parallelization of the flow solver
- Linear system resolution for the adjoint system, currently limited to 10 million vertices then we do not reach convergence
- Adjoint computation on implicit surface (cylinder)