



# THIRD AIAA SONIC BOOM PREDICTION WORKSHOP INTRODUCTION

Lori Ozoroski  
NASA Langley Research  
Center

# ORGANIZING COMMITTEE

## NASA

- Melissa Carter
- Sriram Rallabhandi
- Mike Park
- Alexandra Loubeau
- Lori Ozoroski
- James Jensen

## Boeing

- Todd Magee

## DLR

- Jochen Kirz

## Gulfstream Aerospace

- Tom Wayman

## JAXA

- Yoshi Makino

## Lockheed Martin

- John Morgenstern

## ONERA

- Gerald Carrier

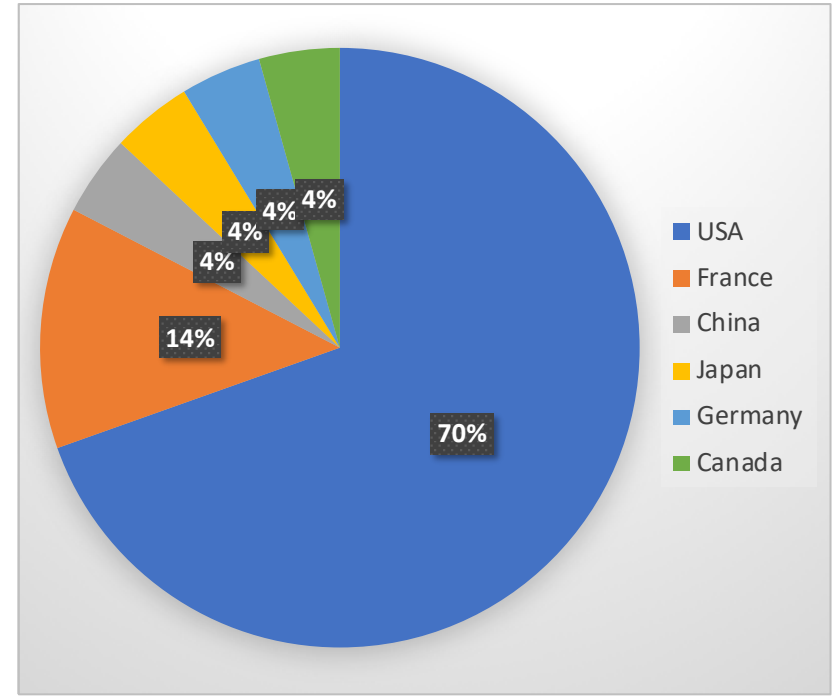
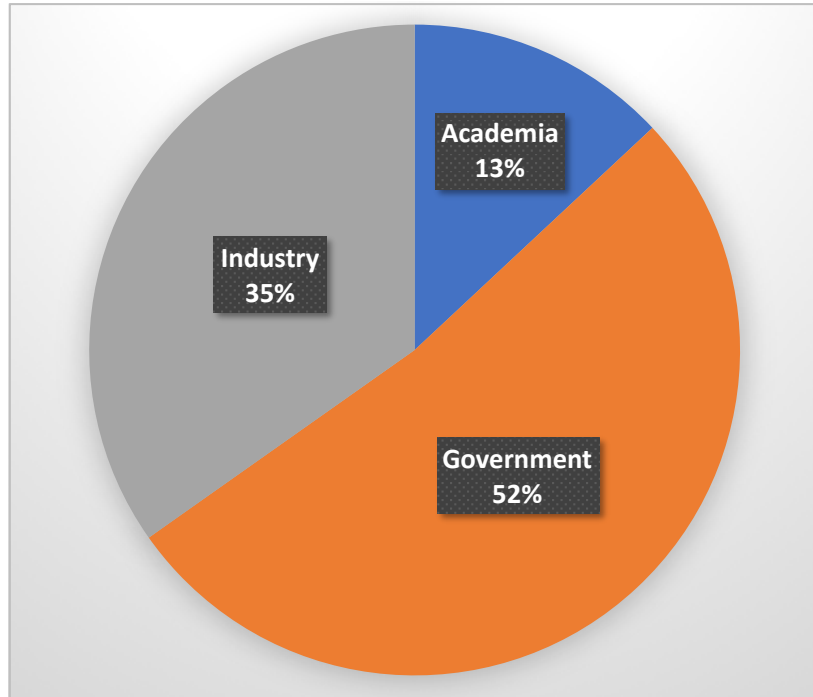
## Volpe, US DOT

- Juliet Page

# WORKSHOP OBJECTIVE

The objective of the Third Sonic Boom Prediction Workshop is to assess the state of the art for predicting near field signatures with computational fluid dynamics (CFD) and propagation codes used to propagate near field signatures to the ground.

# THIRD WORKSHOP: 23 PARTICIPANTS



ANSYS  
Boeing  
Boom Aero  
DASSAV  
DLR

FAA  
INRIA  
JAXA  
Lockheed  
Martin

Metacomp  
NASA  
Northwestern  
Polytech  
ONERA

Penn State  
Siemens  
Texas A&M  
Volpe

# WORKSHOP OVERVIEW

- Saturday, January 4, 2020 (Near Field CFD)
  - CFD to CFD comparison of near field
  - CFD to EXP comparison of near field
  - 2 required configurations
- Sunday, January 5, 2020 (Propagation)
  - Code to code comparison of propagated ground signatures
  - 2 required near field signatures

**January 4, 2020: Near Field CFD**

7:15 am - 8:00 am	<b>Breakfast</b>	
8:00 am – 8:05 am	Introduction	Lori Ozoroski
8:05 am – 8:30 am	Overview	M. Park & M. Carter
8:30 am - 8:55 am	DLR	Jochen Kirz
8:55 am - 9:20 am	Texas A&M University	Forrest Carpenter
9:20 am - 9:45 am	NASA Langley	Alaa Elmiligui
<del>9:45 am - 10:10 am</del>	<del>ONERA</del>	<del>Olivier Atinault</del>
10:10 am - 10:35 am	<b>Break</b>	
10:35 am - 11:00 am	Boeing	Todd Magee
11:00 am - 11:25 am	NASA Ames	Wade Spurlock
11:25 am - 11:50 am	NASA Ames	James Jenson
11:50 am - 12:15 pm	Northwestern Polytechnical University	Zhijin Lei (University of Miami)
12:15 pm - 1:15 pm	<b>Lunch</b> Provided by AIAA included in the registration fee	
1:15 pm - 1:40 pm	Siemens	Chris Nelson
1:40 pm – 2:05 pm	Boom Aero	Enrico Fabiano
2:05 pm - 2:30 pm	ANSYS	Isik Ozcer
2:30 pm – 2:55 pm	Metacomp	Amarnatha Sarma Potturi
2:55 pm – 3:20 pm	<b>Break</b>	
3:20 pm – 3:45 pm	NASA Langley	Mike Park
3:45 pm - 4:10 pm	INRIA	Adrien Loseille
4:10 pm - 4:35 pm	JAXA	Hiroaki Ishikawa
<del>4:35 pm - 5:00 pm</del>	<del>Lockheed Martin</del>	<del>John Morgenstern</del>
5:00 pm - 6:00 pm	Summary	M. Park & M. Carter
6:00 pm - 6:30pm	Discussion	

## January 5, 2020: Propagation

7:15 am - 8:00 am	<b>Breakfast</b>	
8:00 am – 8:05 am	Introduction	Lori Ozoroski
8:05 am – 8:30 am	Overview	Sriram Rallabhandi
8:30 am – 9:00 am	NASA Ames	Mike Aftosmis
9:00 am – 9:30 am	Dassault	Pierre-Elie Normand
9:30 am – 10:00 am	ONERA	Gerald Carrier
10:00 am – 10:30 am	<b>Break</b>	
10:30 am – 11:00 am	NASA Langley	Sriram Rallabhandi
11:00 am – 11:30 am	Volpe	R. Downs & J. Page
11:30 am – 12:00 pm	Penn State	Luke Wade
12:00 pm – 1:00 pm	<b>Lunch</b> Provided by AIAA included in the registration fee	
1:00 pm – 1:30 pm	NASA Langley	Joel Lonzaga
1:30 pm – 2:00 pm	JAXA	Masashi Kanamori
2:00 pm – 2:30 pm	Boeing	Hao Shen
2:30 pm – 3:00 pm	<b>Break</b>	
3:00 pm – 3:30 pm	Boom Supersonic	Enrico Fabiano
<del>3:30 pm – 4:00 pm</del>	<del>Lockheed Martin</del>	<del>John Morgenstern</del>
4:00 pm – 4:30 pm	FAA	Sandy Liu
4:30 pm – 5:00 pm	Summary	S. Rallabhandi & A. Loubeau
5:00 pm – 5:30 pm	Discussion	



# THIRD AIAA SONIC BOOM PREDICTION WORKSHOP NEAR FIELD CFD INTRODUCTION

Melissa Carter & Mike  
Park  
NASA Langley  
Research Center



# MOTIVATION

Commercial supersonic overland flight is currently prohibited

- Supersonic overland flight is an enabler for entry into new vehicle market



Replacing the prohibition with a certification standard requires an international effort to quantify the accuracy and reliability of prediction methods



Deficiencies in existing methods should be noted to focus research on addressing weaknesses



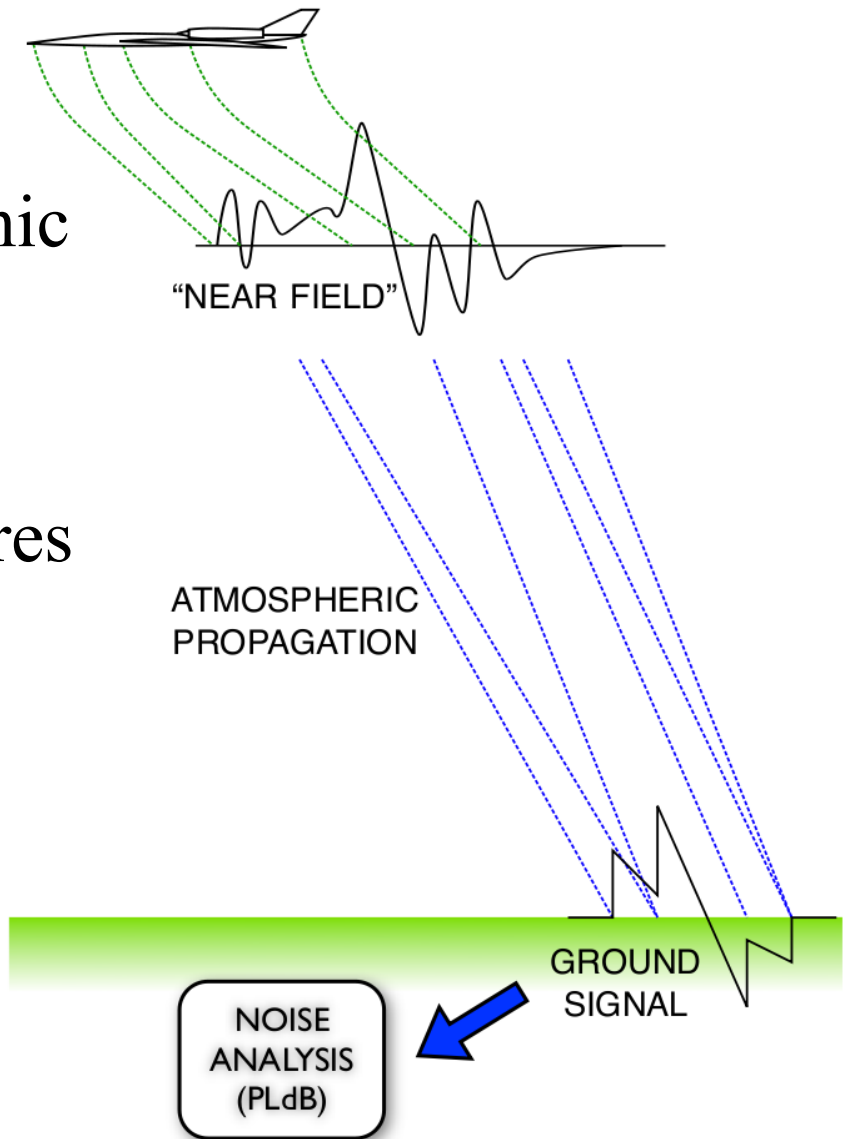
# MOTIVATION

Near field CFD is part of sonic boom prediction

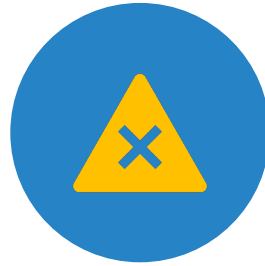
Explore the issues

Impartially compare signatures by uniform application of

- Near field statistics
- Propagation
- Loudness measures



# WORKSHOP CULTURE



Adjectives such as good, bad, right, and wrong oversimplify issues and should be avoided



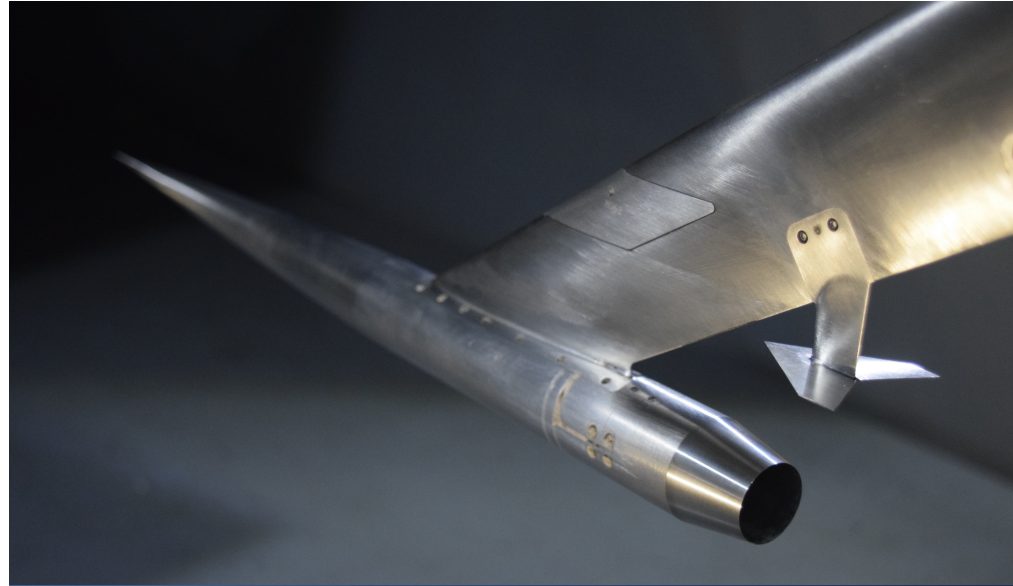
Focus on describing observed differences and communicate why things are different

# MODELS AND CASES

Ames 9'x7' Biconvex  
Plume-Shock Interaction  
Case

C608, an early X-59  
Prototype

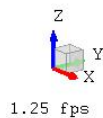
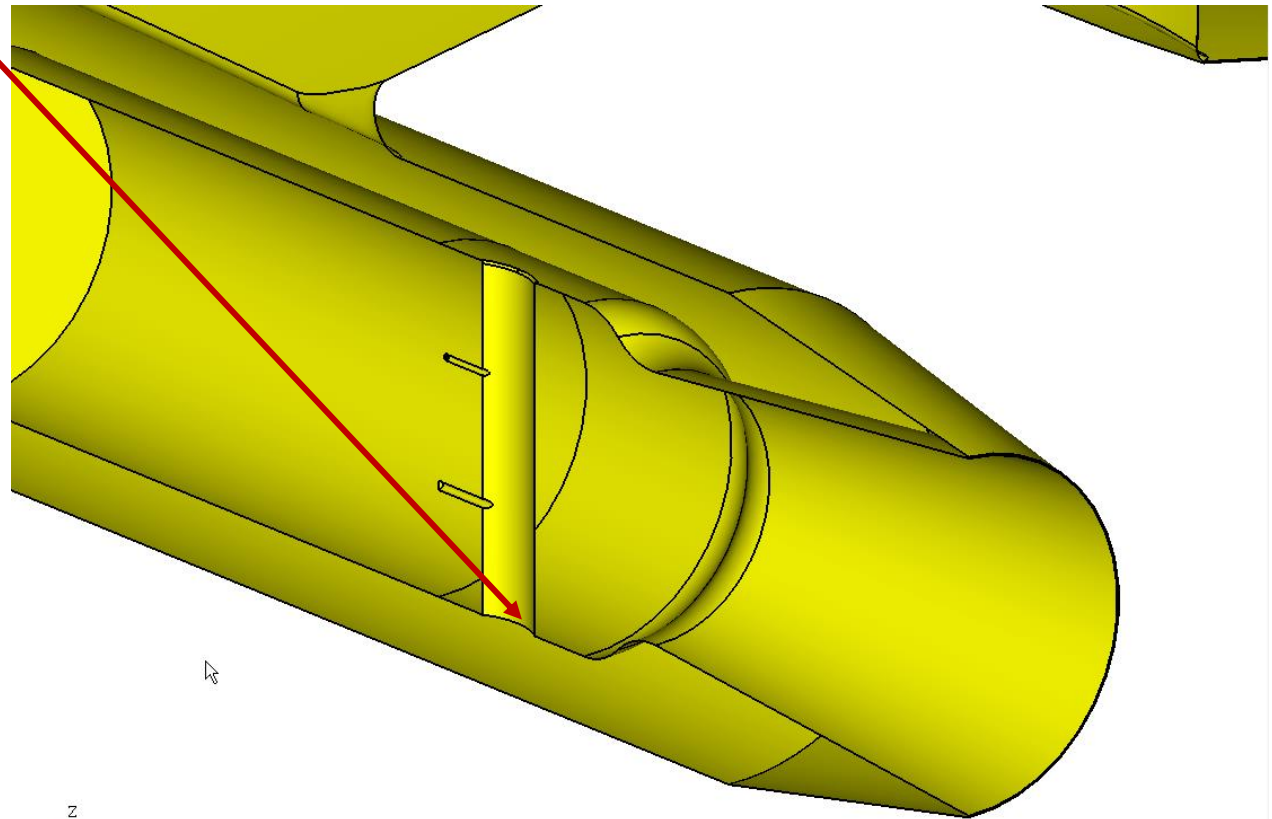
IGES and STEP  
geometry files along with  
workshop generated grids  
provided



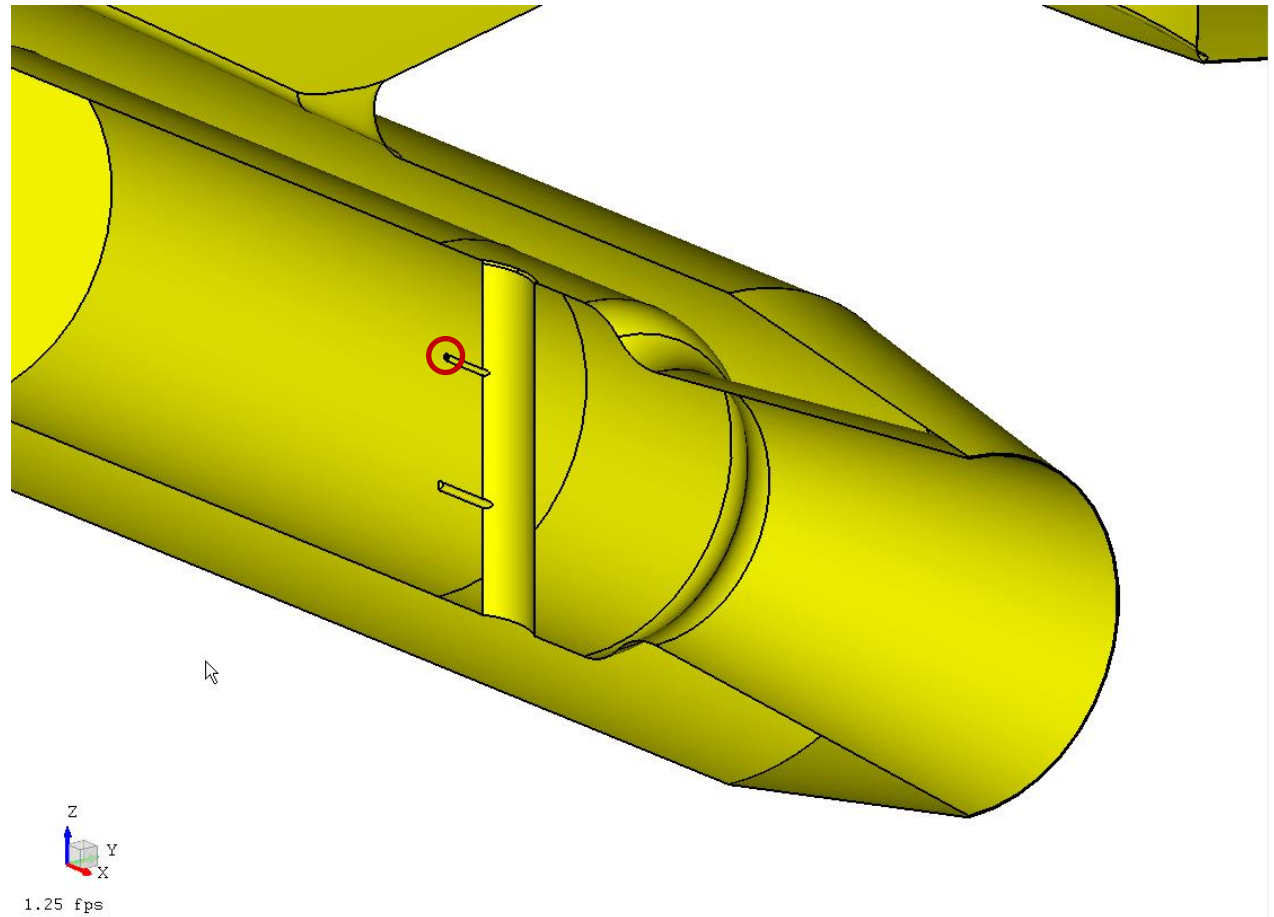
# BICONVEX GEOMETRY ASSESSMENT

3.5e-5 inch edge

Mark Gammon (CADfix)



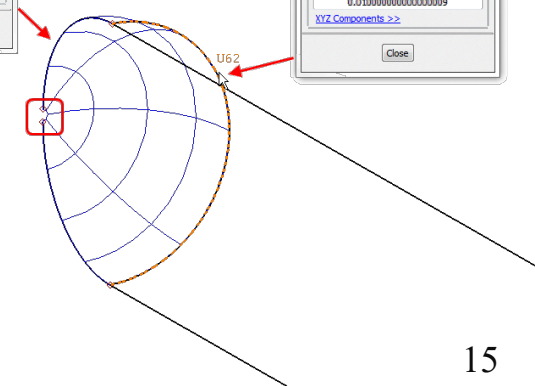
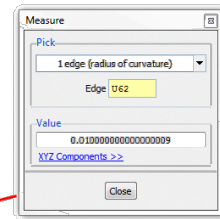
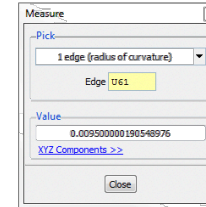
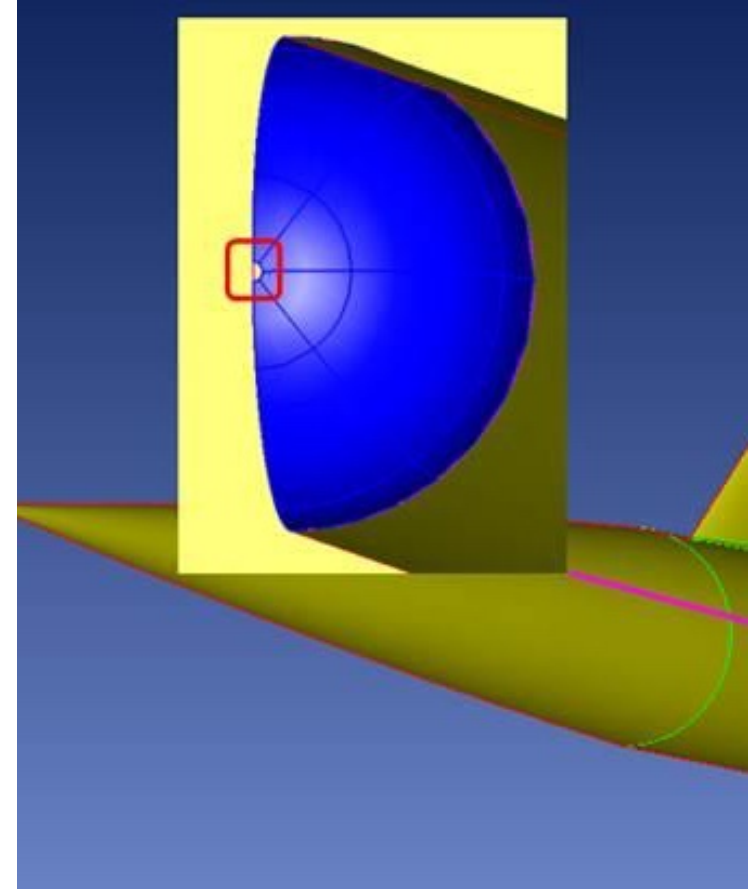
# BICONVEX GEOMETRY ASSESSMENT



# BICONVEX GEOMETRY ASSESSMENT

IGES (from OpenCASCADE) has a spherical cap on cylinder with a slightly smaller radius resulting in a torus surface and a gap at the pole. Face topology is not closed.

STEP (from NX) has closed the loop by merging the vertices but the underlying NURBS curves/surfaces are the same as in IGES



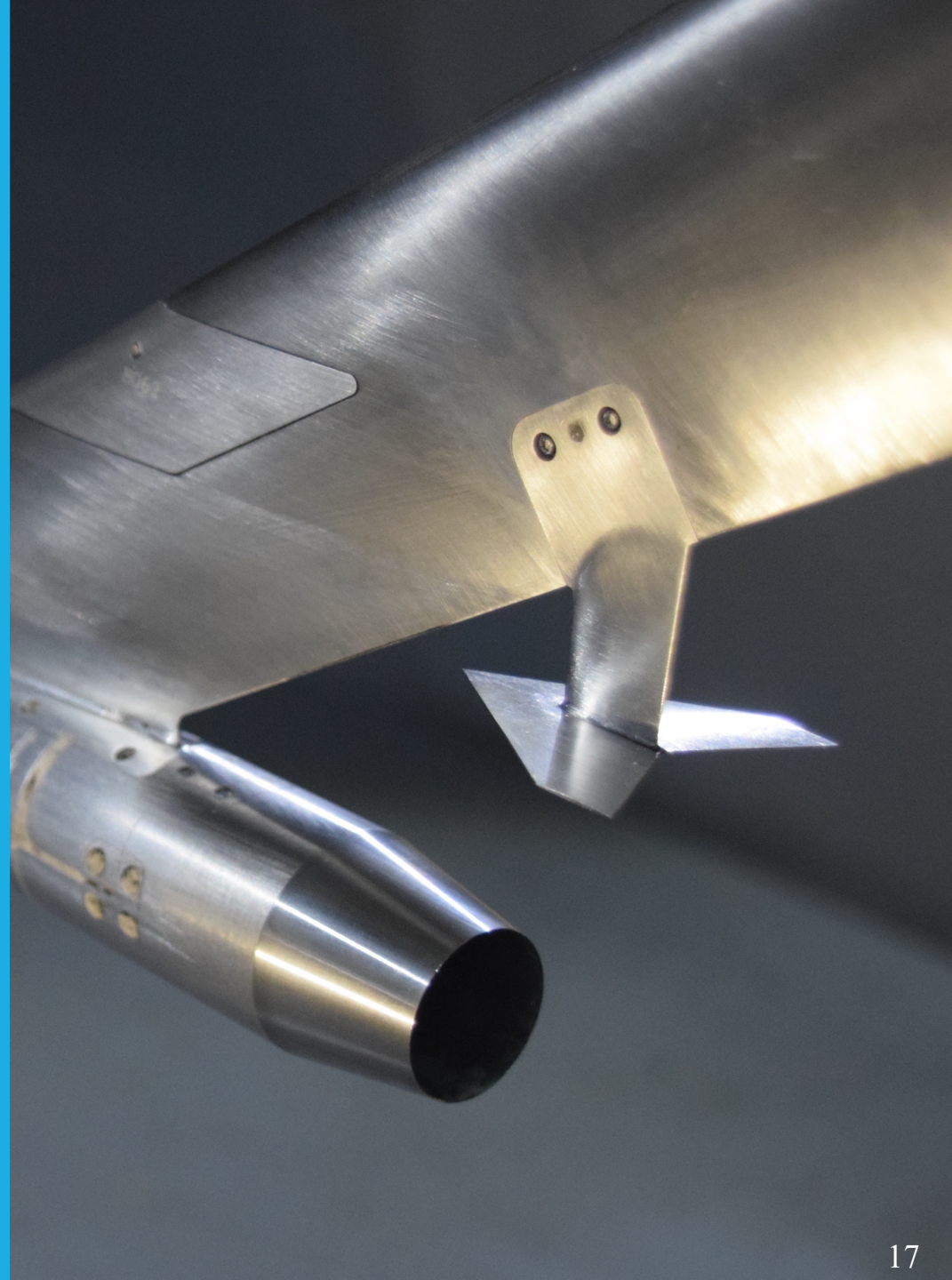
# C608 GEOMETRY ASSESSMENT

- Less detailed examination
- Geometry is well-formed, with some inconvenient sliver faces (some curved)
- Both configurations had internal revisions through iterating with Geolab
- Participants are asked to report any geometry issues or modifications required for meshing

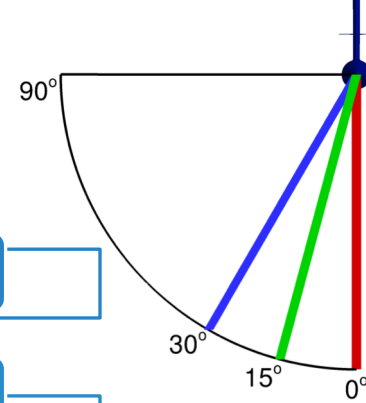


# BICONVEX INTRODUCTION

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# SIMULATION CONDITIONS



1.6 Mach

0.0° angle of attack

Geometry and grid provided in correct orientation

22.4-inch-long model

374 Rankine temperature

376,850 Reynolds number per inch

- 8.4 million Reynolds number based on model length

8.0 Engine plenum pressure ratio,  $P_T/P_\infty$

1.768 Engine plenum temperature ratio,  $T_T/T_\infty$

Data extracted at  $Z=15.0$  inches, at 3 Phi angles

- Phi angles of approx. 0°, 15° and 30°

# GRID DETAILS

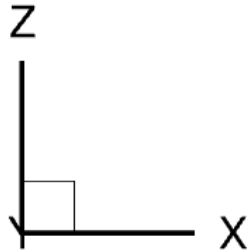
## Tetrahedral Grids

Scale	Nodes	Tetrahedral
1.57	846,227	4,785,786
1.28	1,576,352	8,977,516
1.00	3,286,221	18,815,990

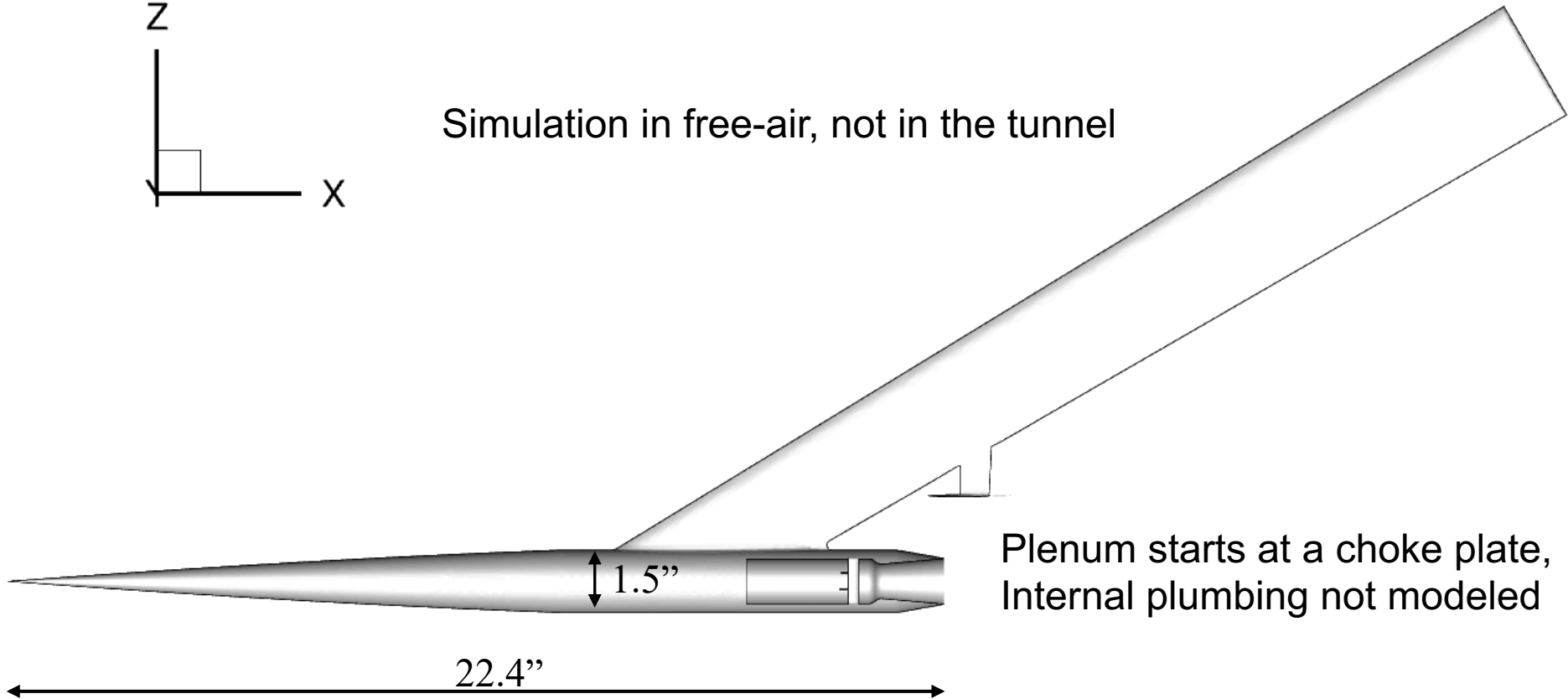
## Mixed-Element Grids

Scale	Nodes	Tetrahedral	Prisms
1.57	846,227	2,825,421	650,469
1.28	1,576,352	5,984,989	993,489
1.00	3,286,221	14,627,534	1,388,470

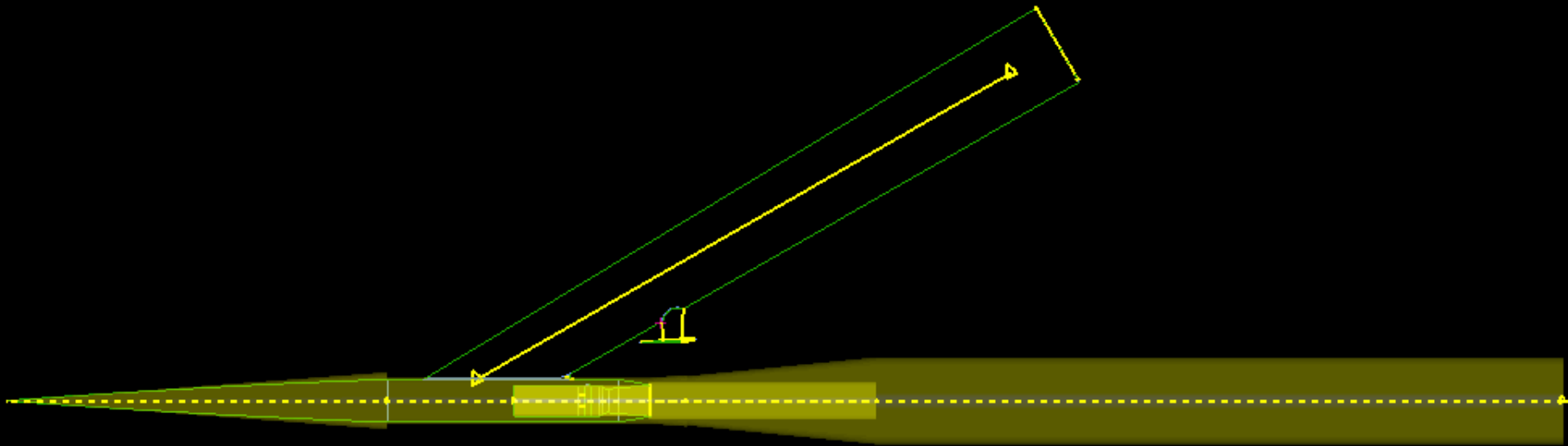
# BICONVEX GEOMETRY



Simulation in free-air, not in the tunnel



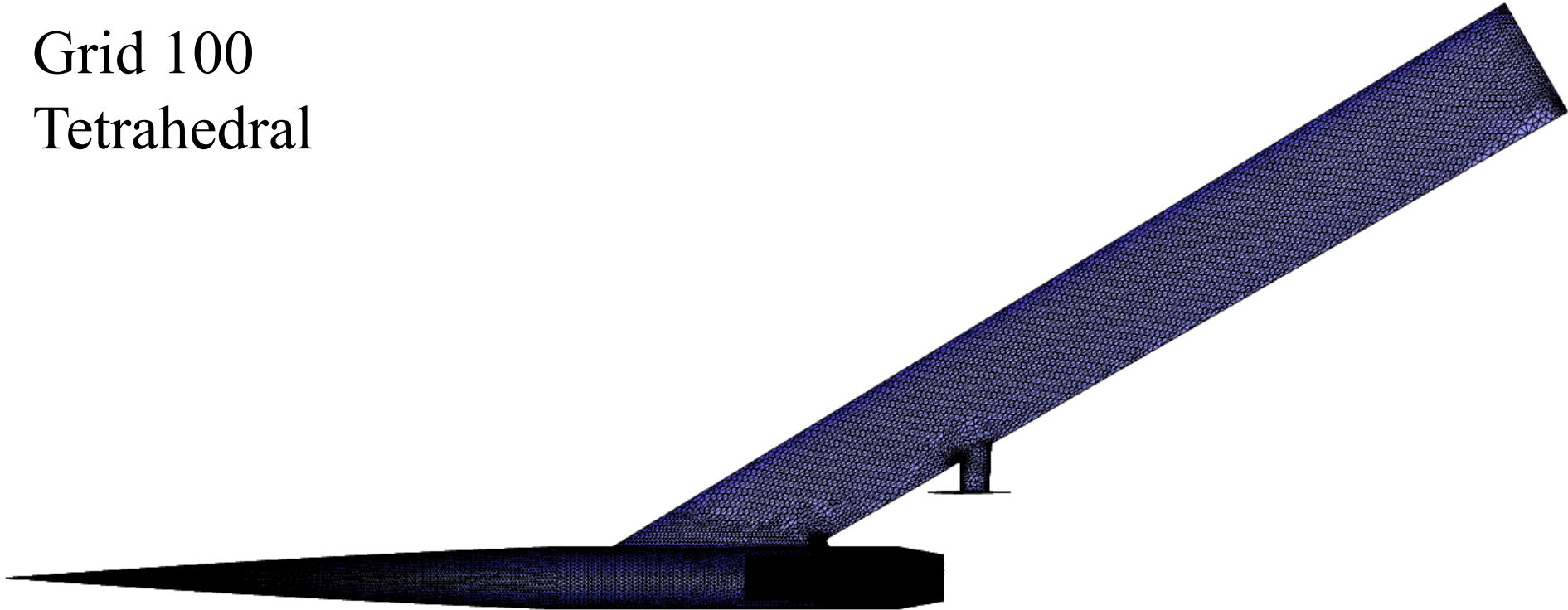
# BICONVEX SOURCING



# BICONVEX SURFACE GRID

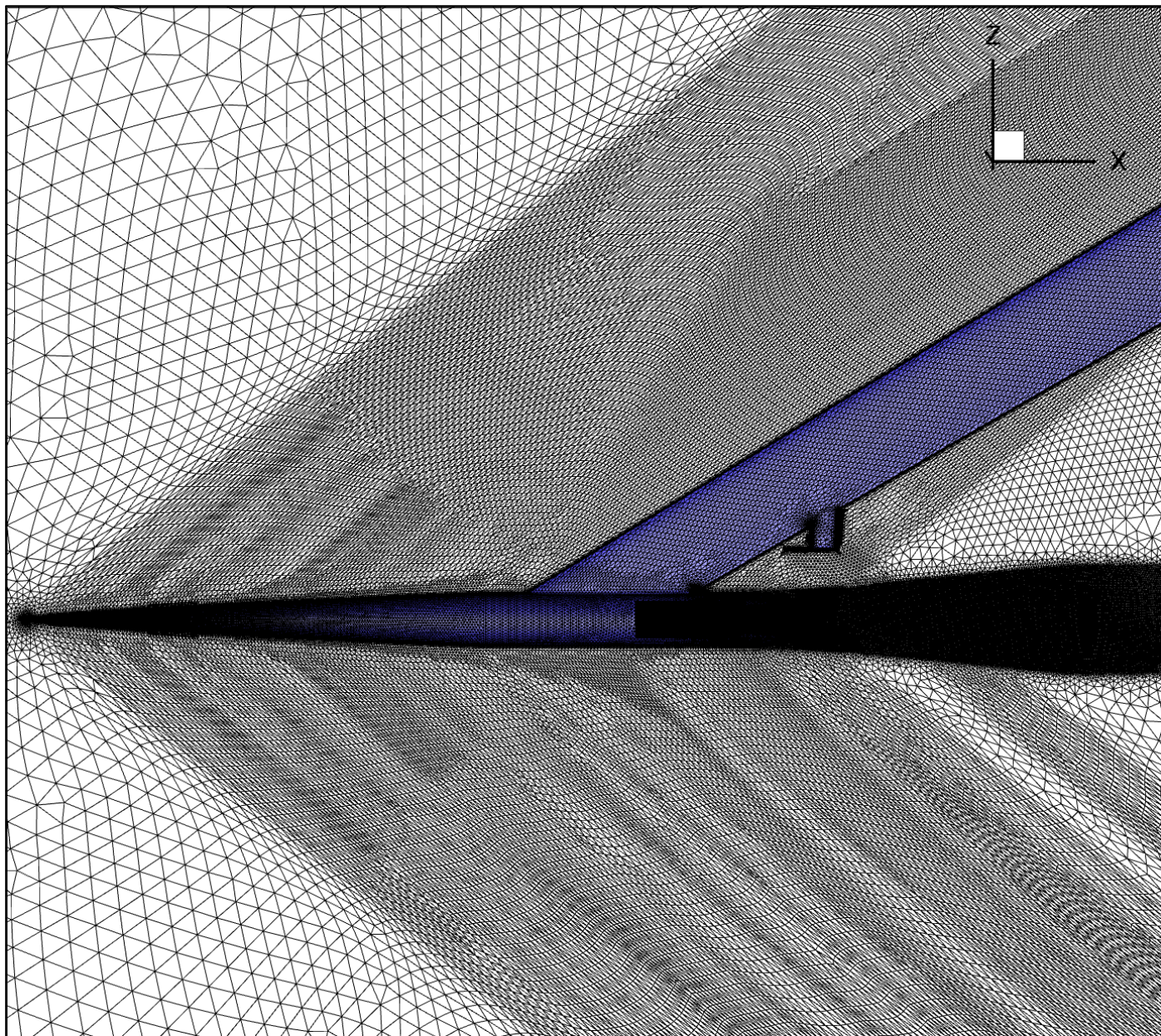
Grid 100

Tetrahedral



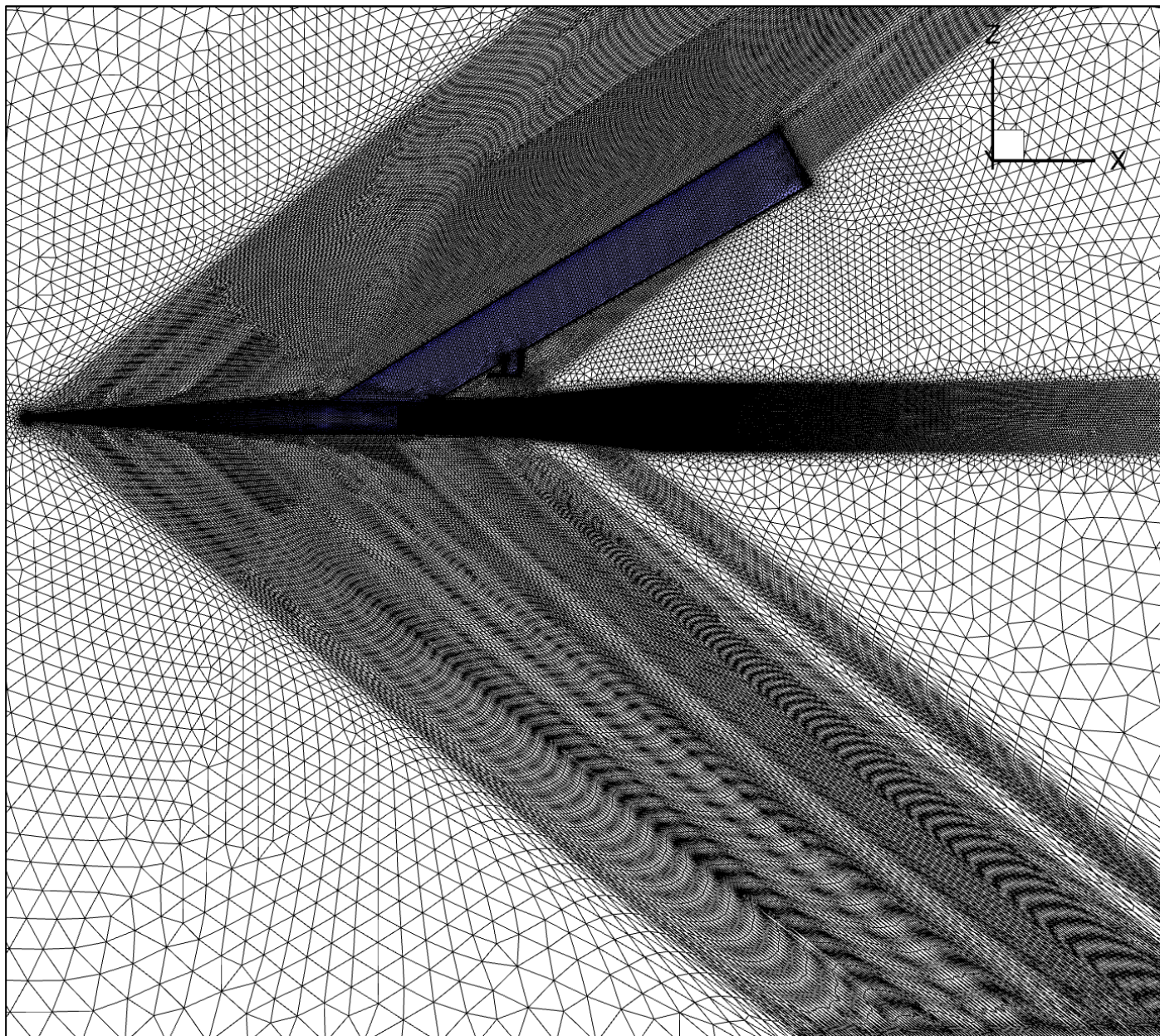
# BICONVEX SYMMETRY PLANE GRID

Grid 100  
Tetrahedral  
Prescribed



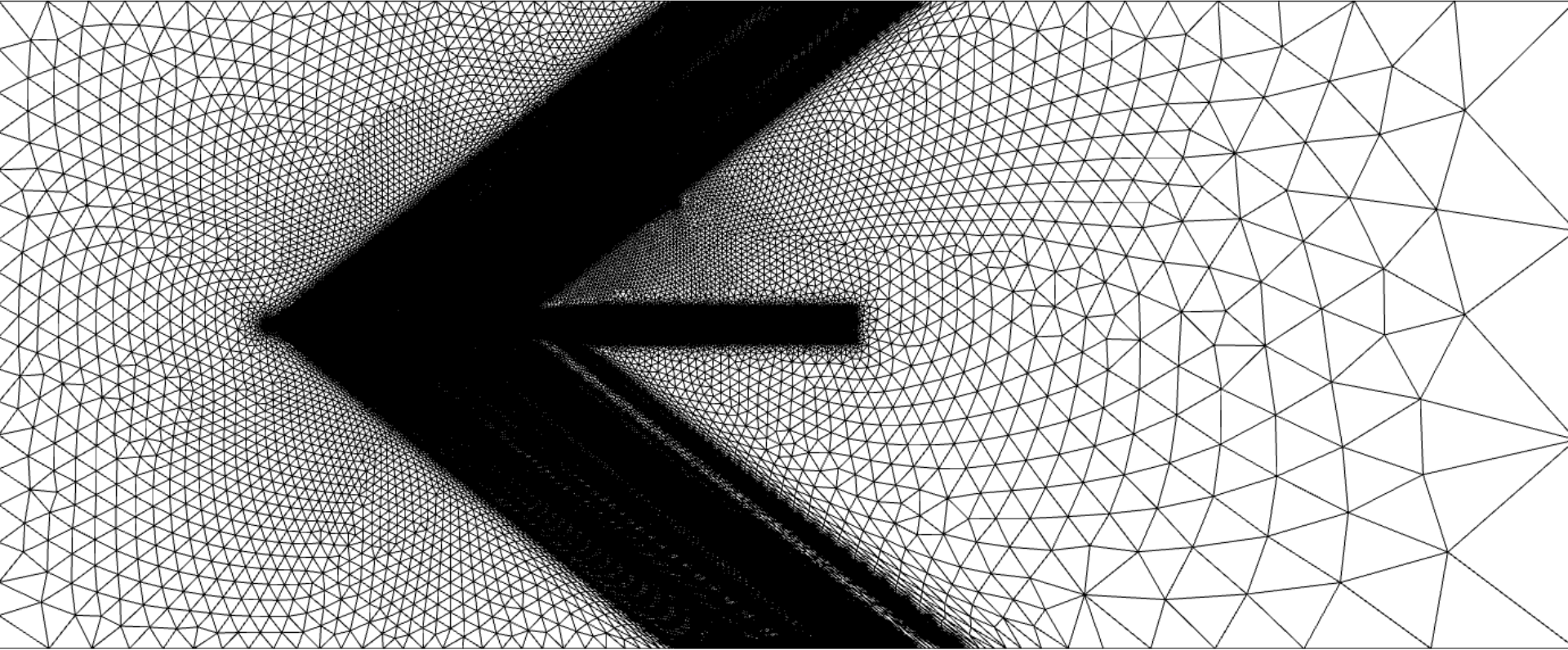
# BICONVEX SYMMETRY PLANE GRID

Grid 100  
Tetrahedral  
Prescribed





# BICONVEX SYMMETRY PLANE GRID



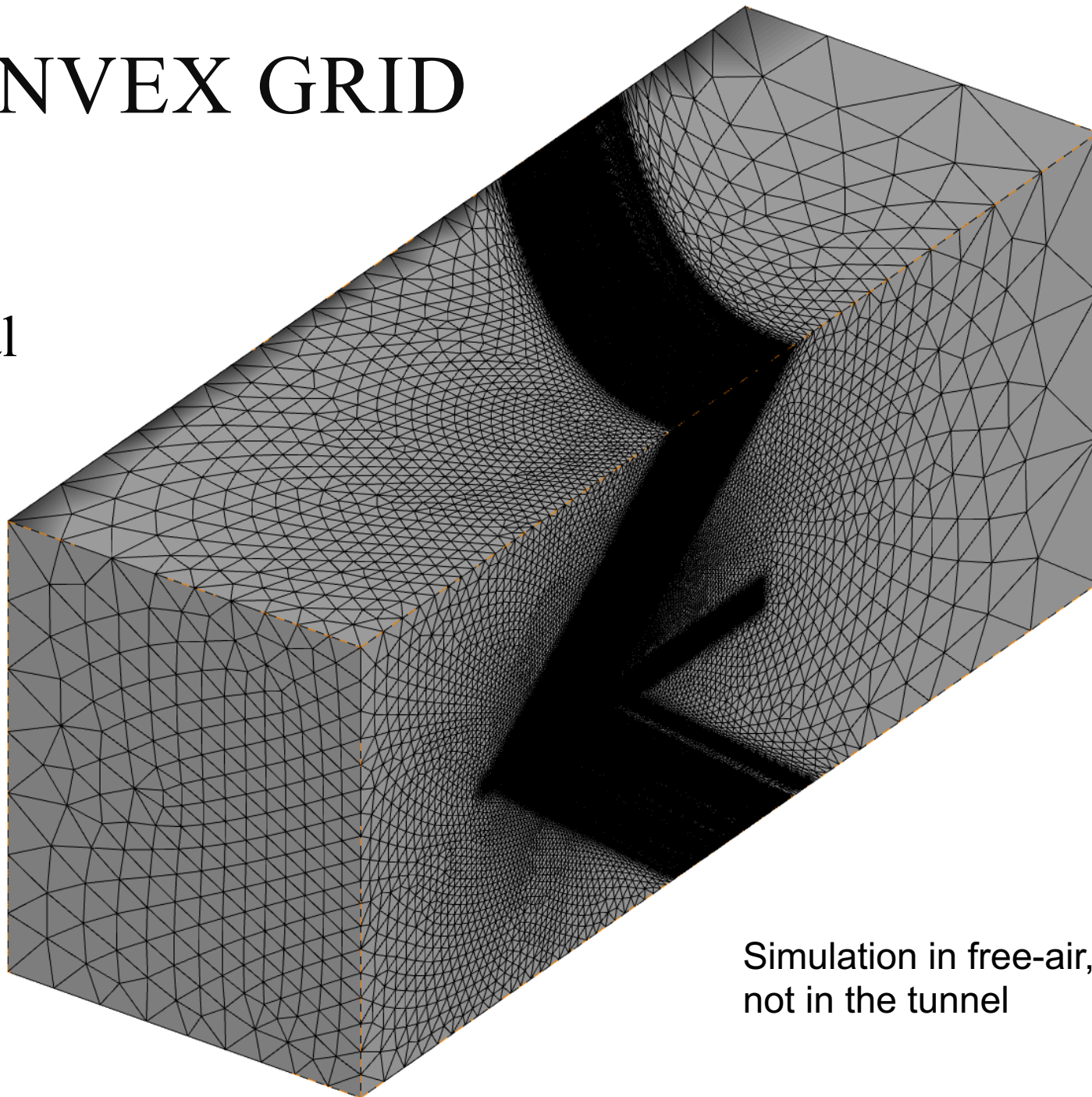
Grid 100  
Tetrahedral  
Prescribed

# BICONVEX GRID

Grid 100

Tetrahedral

Prescribed



Simulation in free-air,  
not in the tunnel

# BICONVEX $dp/p_{INF}$

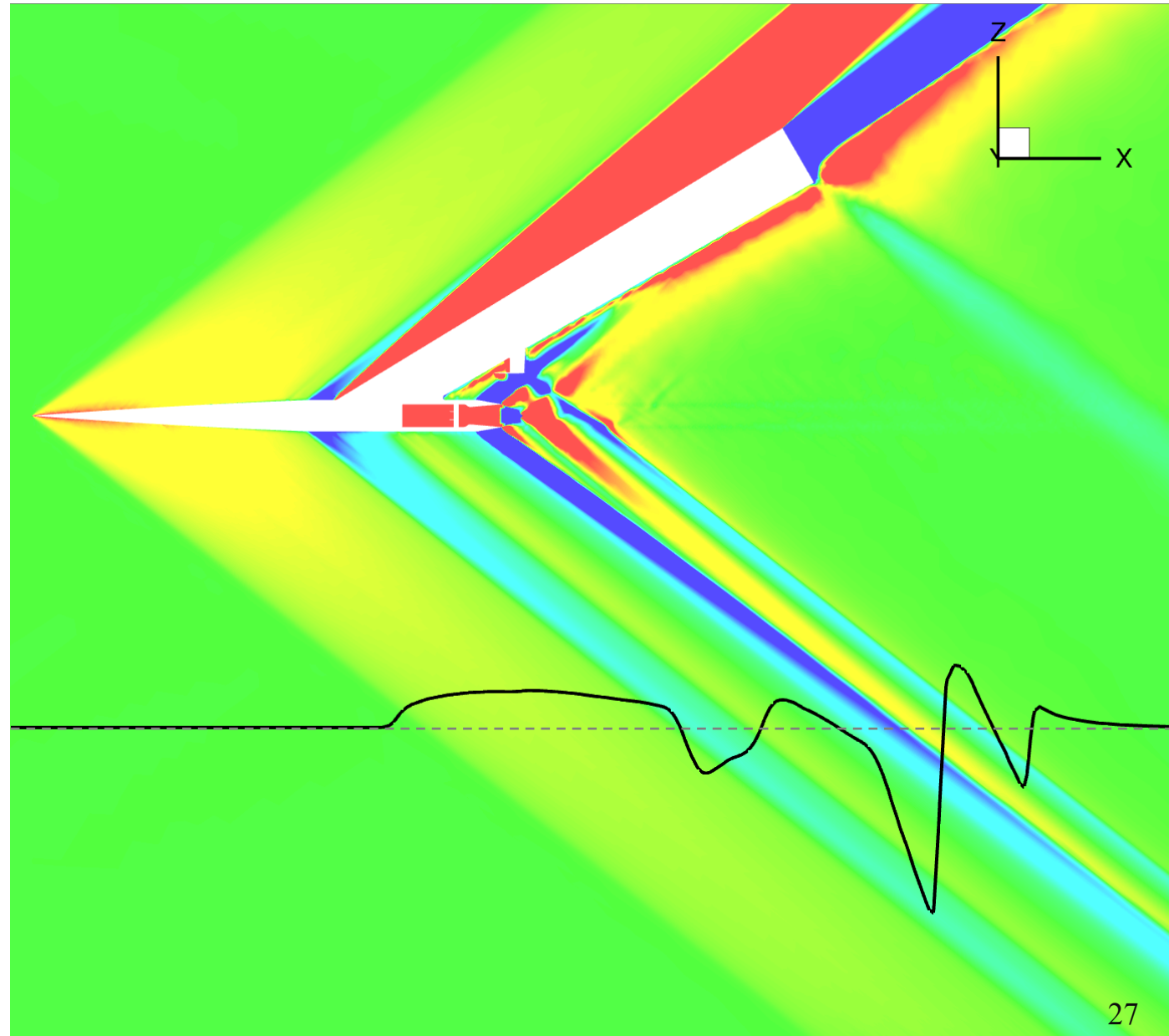
Grid 100

Tetrahedral

USM3D

Production  
code

$dp/p_{\infty}$  which  
is the pressure  
disturbance  
normalized by  
freestream  
pressure

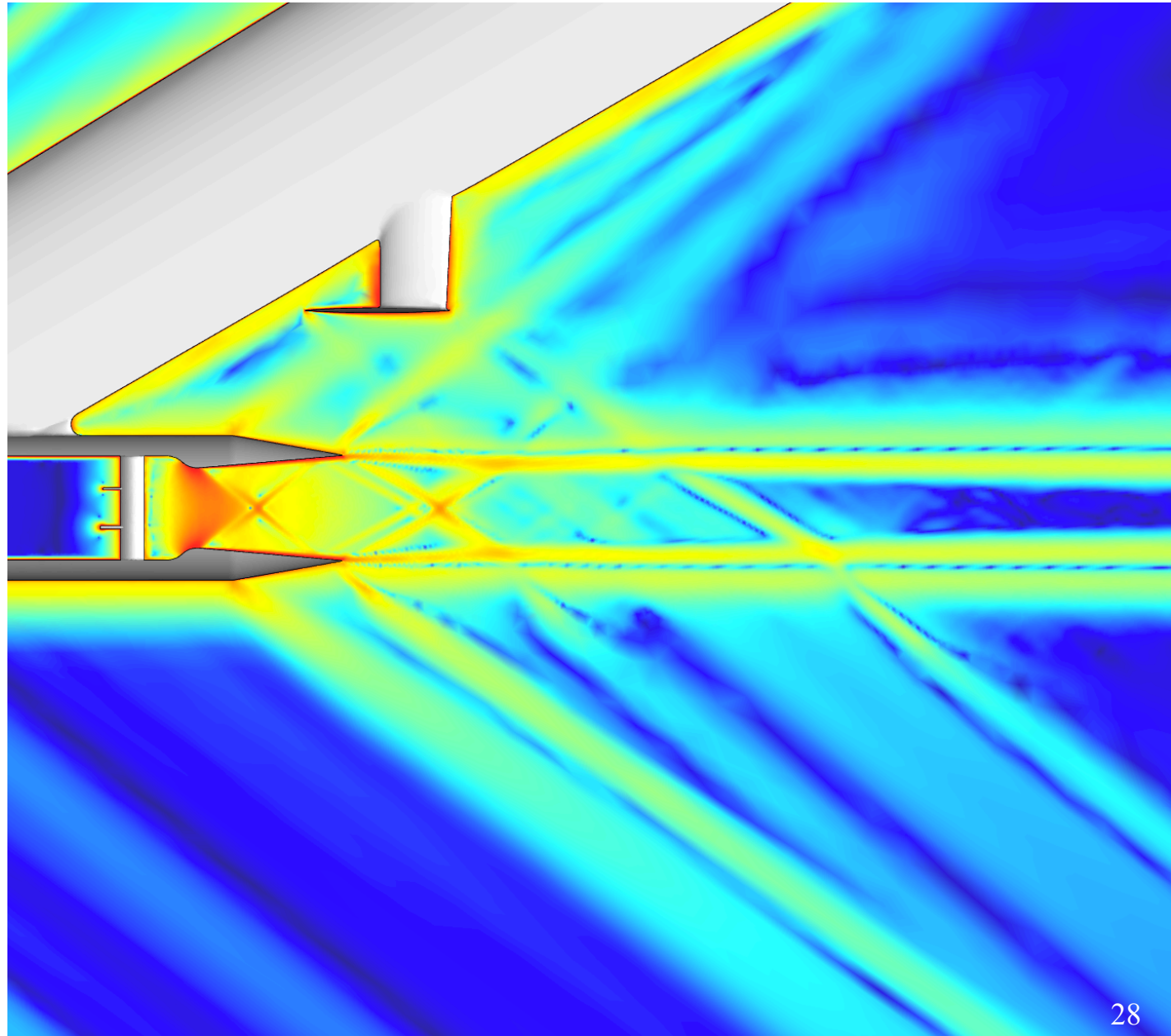


# BICONVEX DENSITY GRADIENT

Grid 100  
Tetrahedral

USM3D  
Production  
code

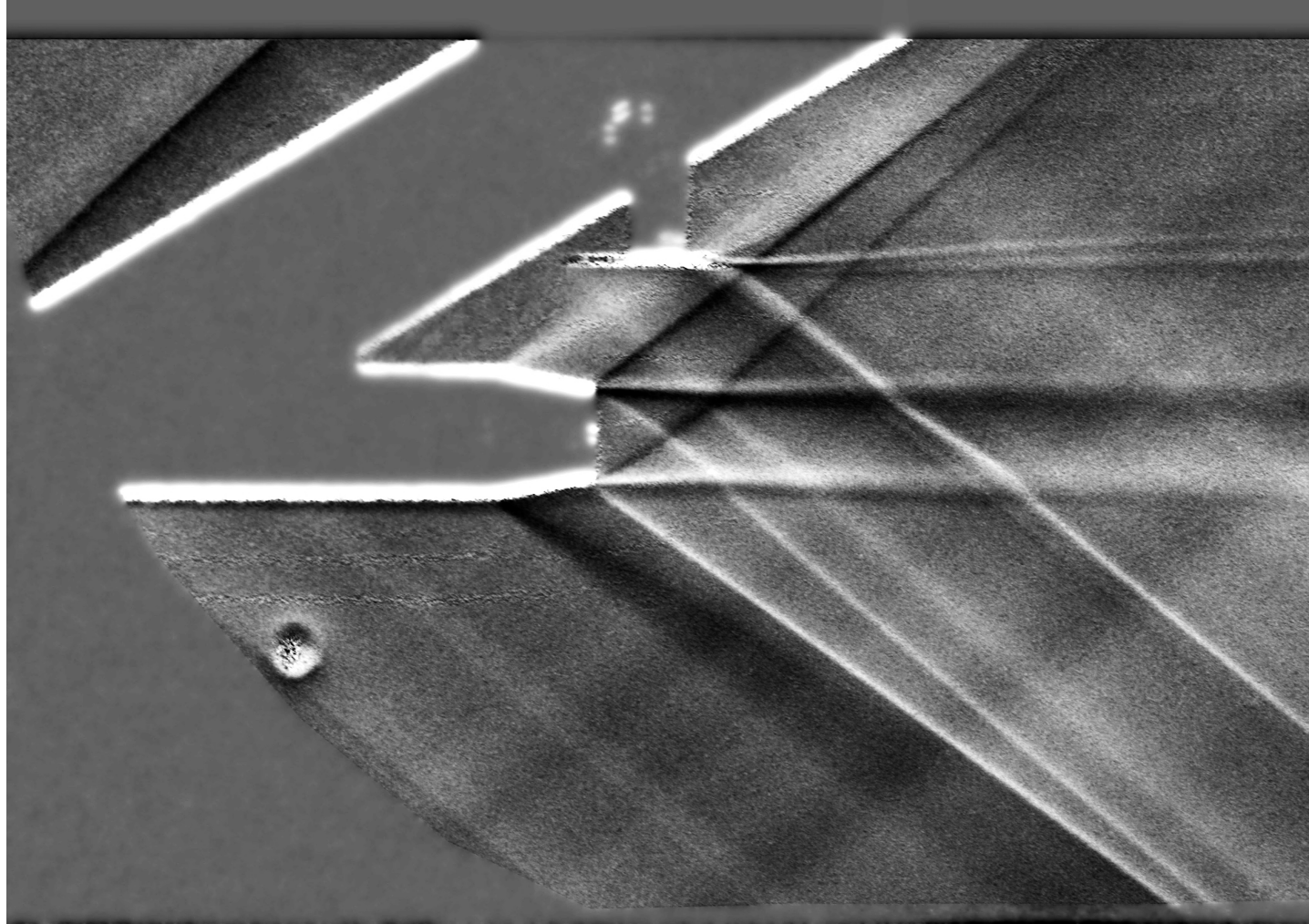
Density  
gradient  
(numerical  
schlieren)



# BICONVEX RETROREFLECTIVE BACKGROUND ORIENTED SCHLIEREN (RBOS)

Ames 9' x 7'  
Wind Tunnel  
RBOS data

Contrast was  
increased  
from original  
photo



C608, AN  
EARLY X-59  
PROTOTYPE,  
INTRODUCTION

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# SIMULATION CONDITIONS

1.4 Mach

0.0° angle of attack

- Geometry and grid provided in correct orientation

1,080 inch-model length

389.9 Rankine temperature

109,776 Reynolds number per inch

- 118.5 million Reynolds number based on model length

10.0 Engine plenum pressure ratio,  $P_T/P_\infty$

7.0 Engine plenum temperature ratio,  $T_T/T_\infty$

2.6 pressure ratio,  $P/P_\infty$  at engine fan face

- Alternate: 0.40 Mach number at engine fan face

1.4 pressure ratio,  $P/P_\infty$  at ECS inlet face

- Alternate: 0.35 Mach number at ECS inlet face

2.4 Bypass pressure ratio,  $P_T/P_\infty$

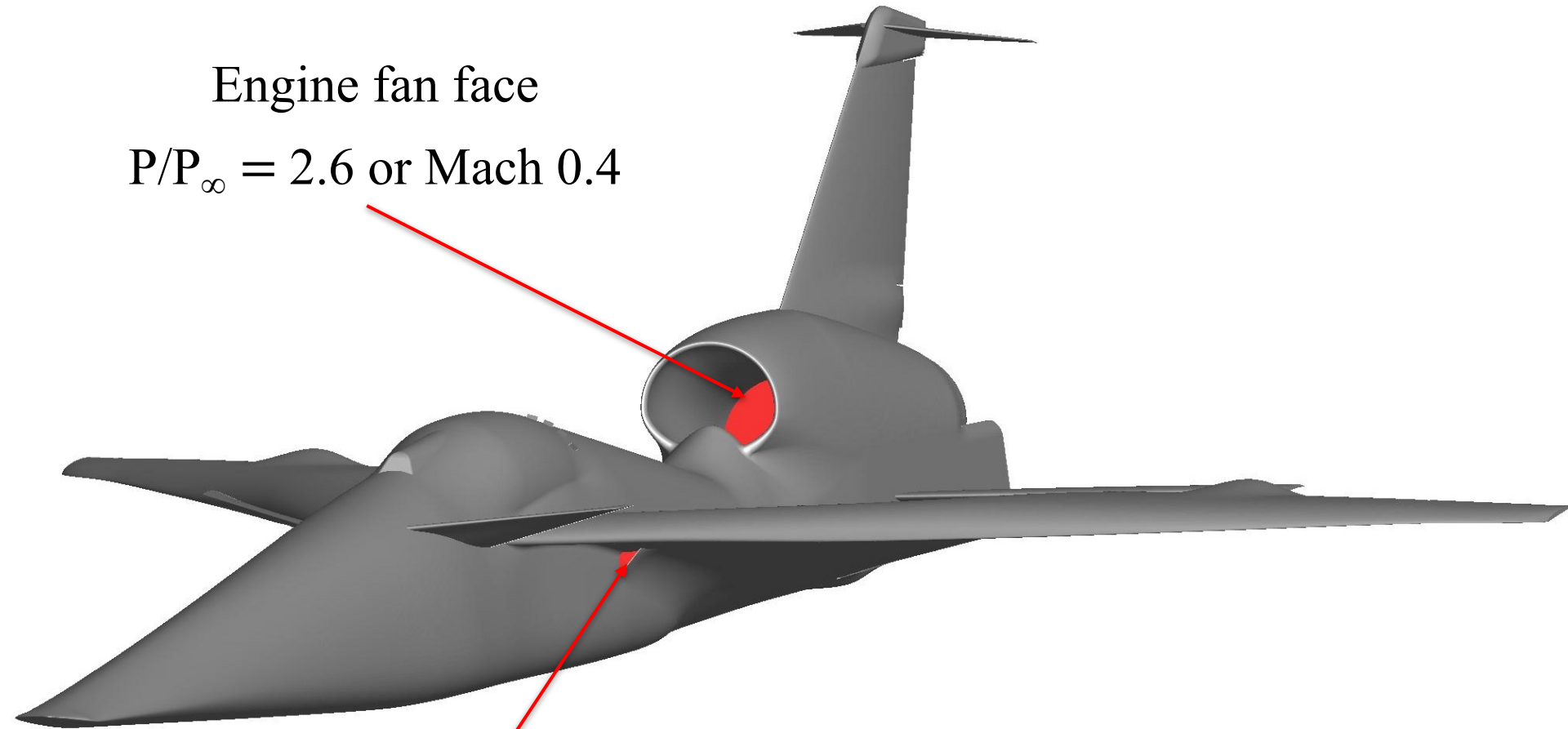
2.0 Bypass temperature ratio,  $T_T/T_\infty$

Data extracted at 3 body lengths below the model

- Phi from 0°-180°, 2° increments

Engine fan face

$P/P_\infty = 2.6$  or Mach 0.4



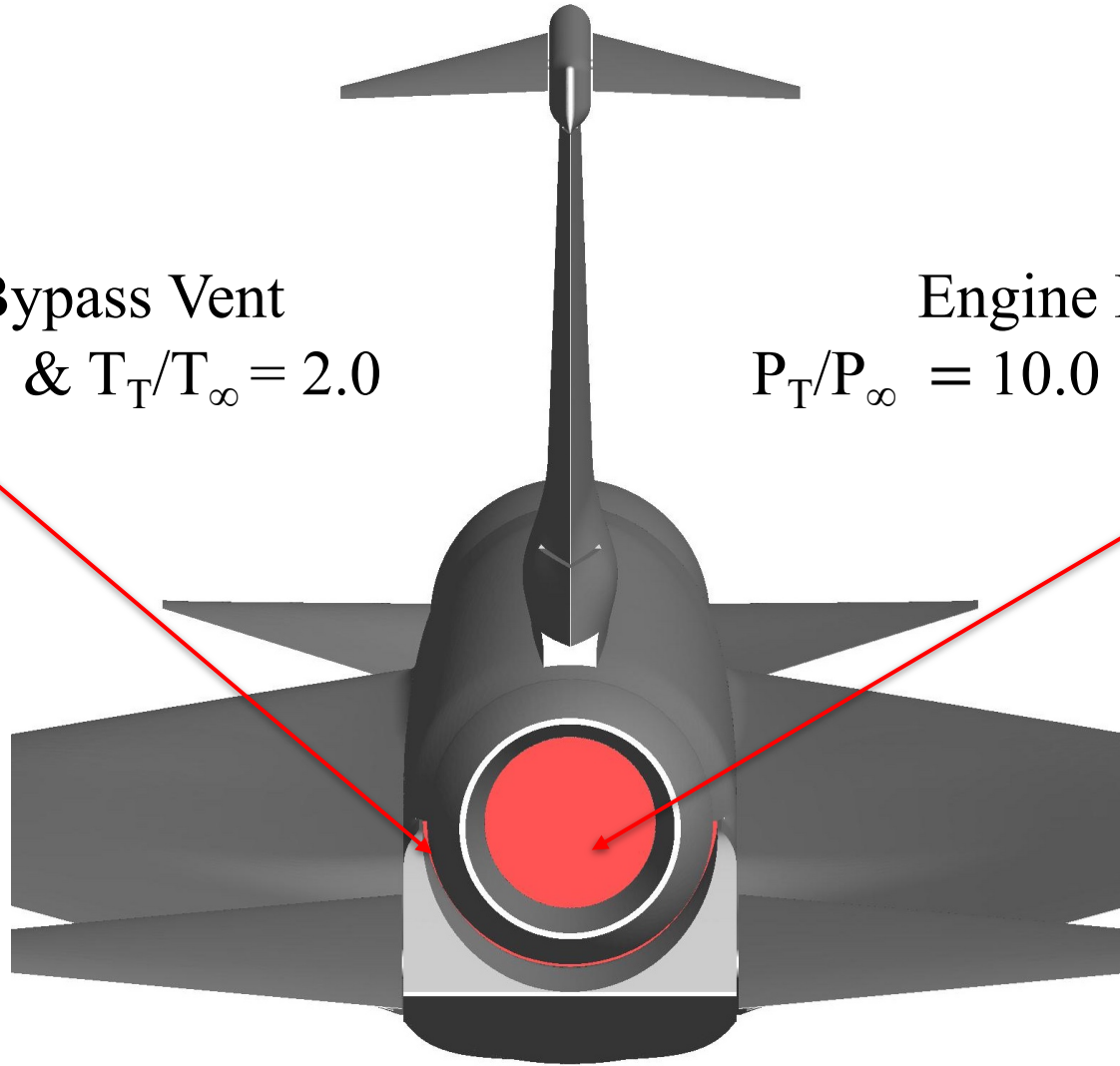
Environmental Control System (ECS) Intake face

$P/P_\infty = 1.4$  or Mach 0.35



Engine Bypass Vent  
 $P_T/P_\infty = 2.4$  &  $T_T/T_\infty = 2.0$

Engine Plenum  
 $P_T/P_\infty = 10.0$  &  $T_T/T_\infty = 7.0$



# GRID

## DETAILS

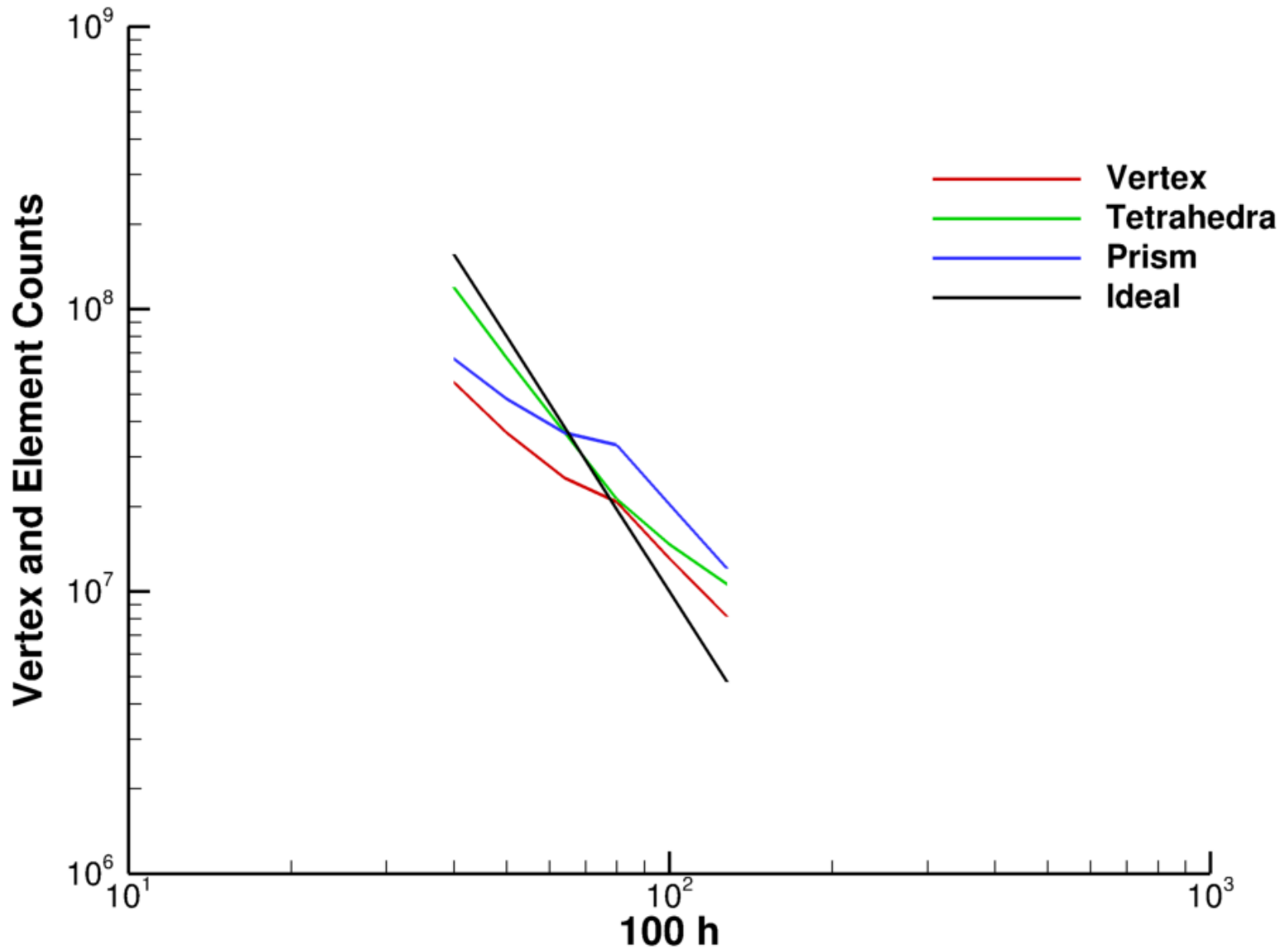
# Tetrahedral Grids

Scale	Nodes	Tetrahedral
0.40	162,970,101	964,796,522
0.50	89,458,689	527,864,565
0.64	50,215,130	295,275,952
0.80	34,879,443	204,705,976
1.00	20,701,451	121,014,955
1.28	11,782,783	68,486,582

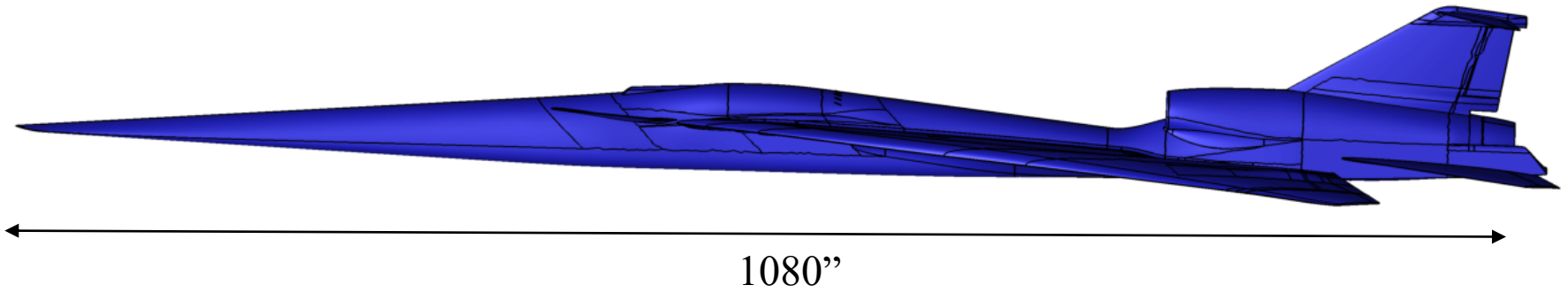
# Mixed-Element Grids

Scale	Nodes	Tetrahedral	Prisms
0.40	162,970,101	119,456,686	281,557,286
0.50	89,458,689	67,138,507	153,392,736
0.64	50,215,130	36,567,810	86,083,502
0.80	34,879,443	21,266,609	61,007,871
1.00	20,701,451	14,681,692	35,346,643
1.28	11,782,783	10,599,974	19,224,816

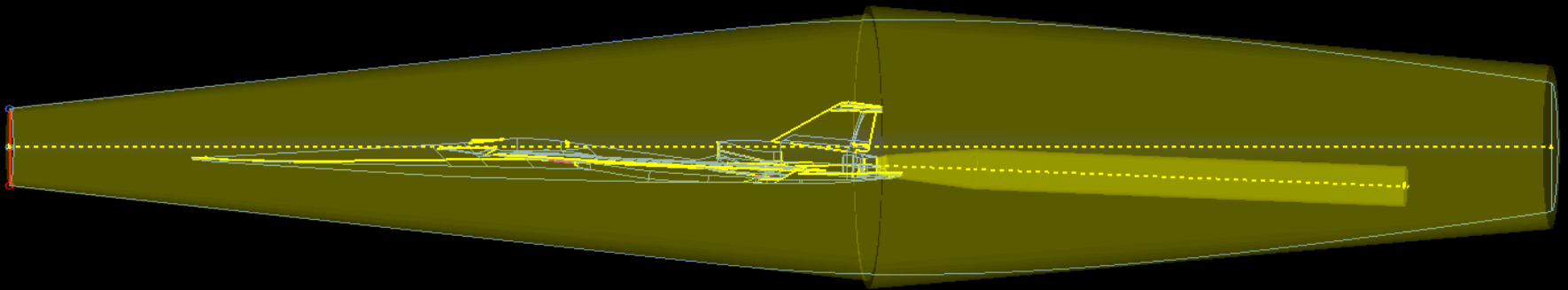
# ELEMENT COUNT



# C608 GEOMETRY



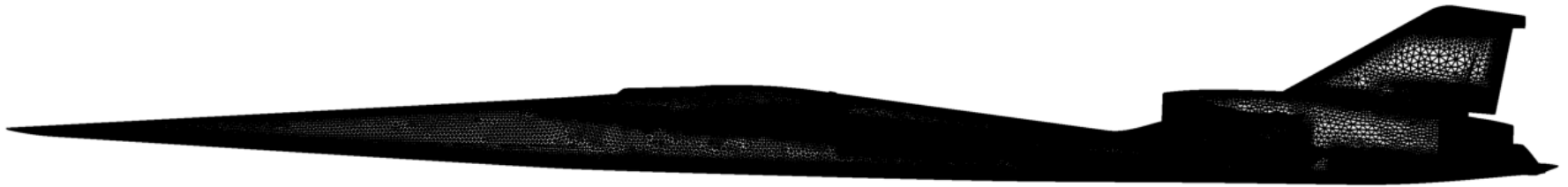
# C608 SOURCING



# C608 SURFACE GRID

Grid 100

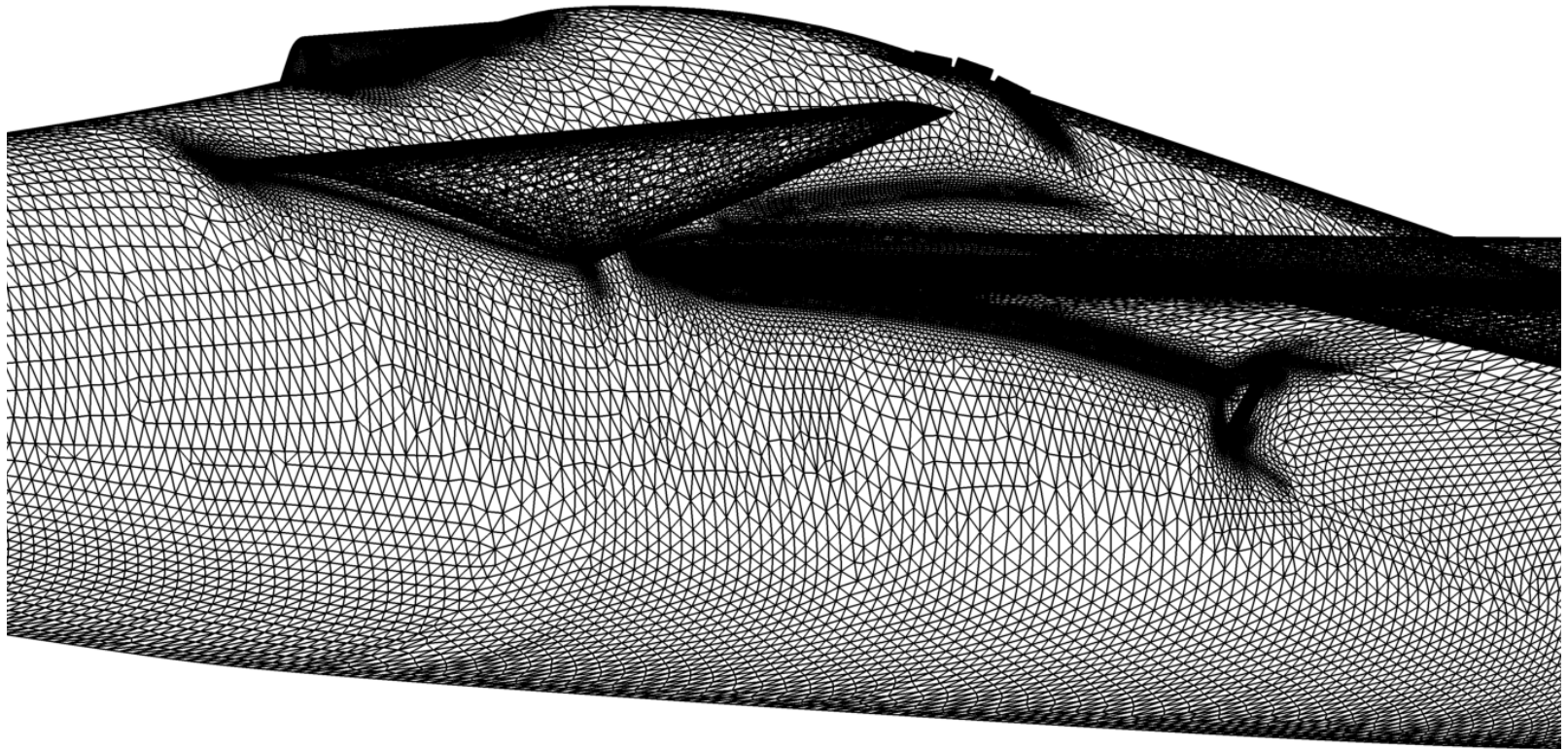
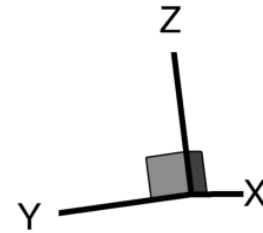
Mixed Element



# C608 SURFACE GRID

Grid 100

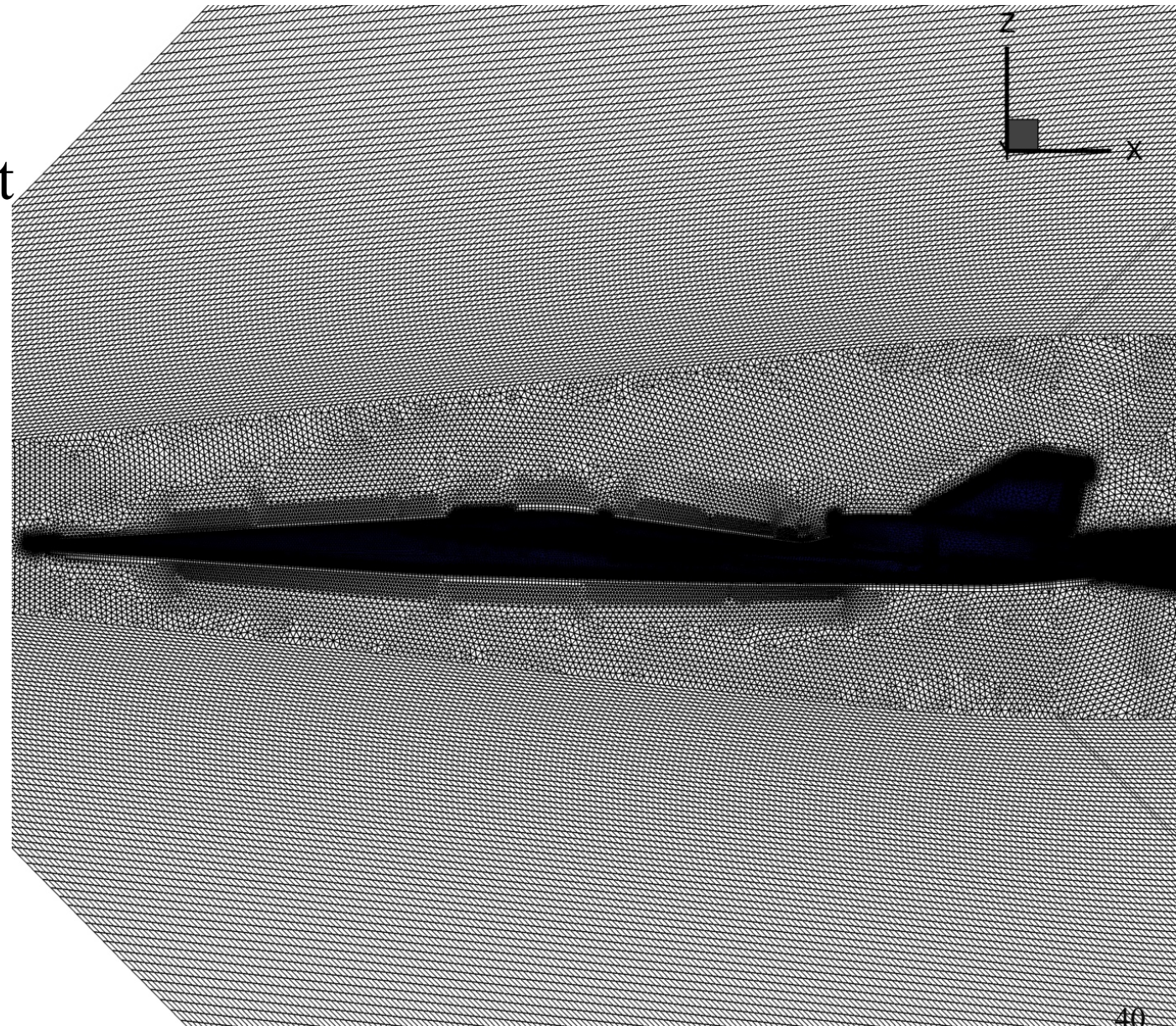
Mixed Element



# C608 SURFACE GRID

Grid 100

Mixed Element

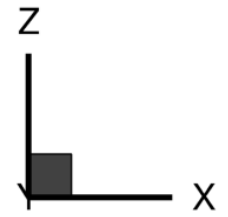
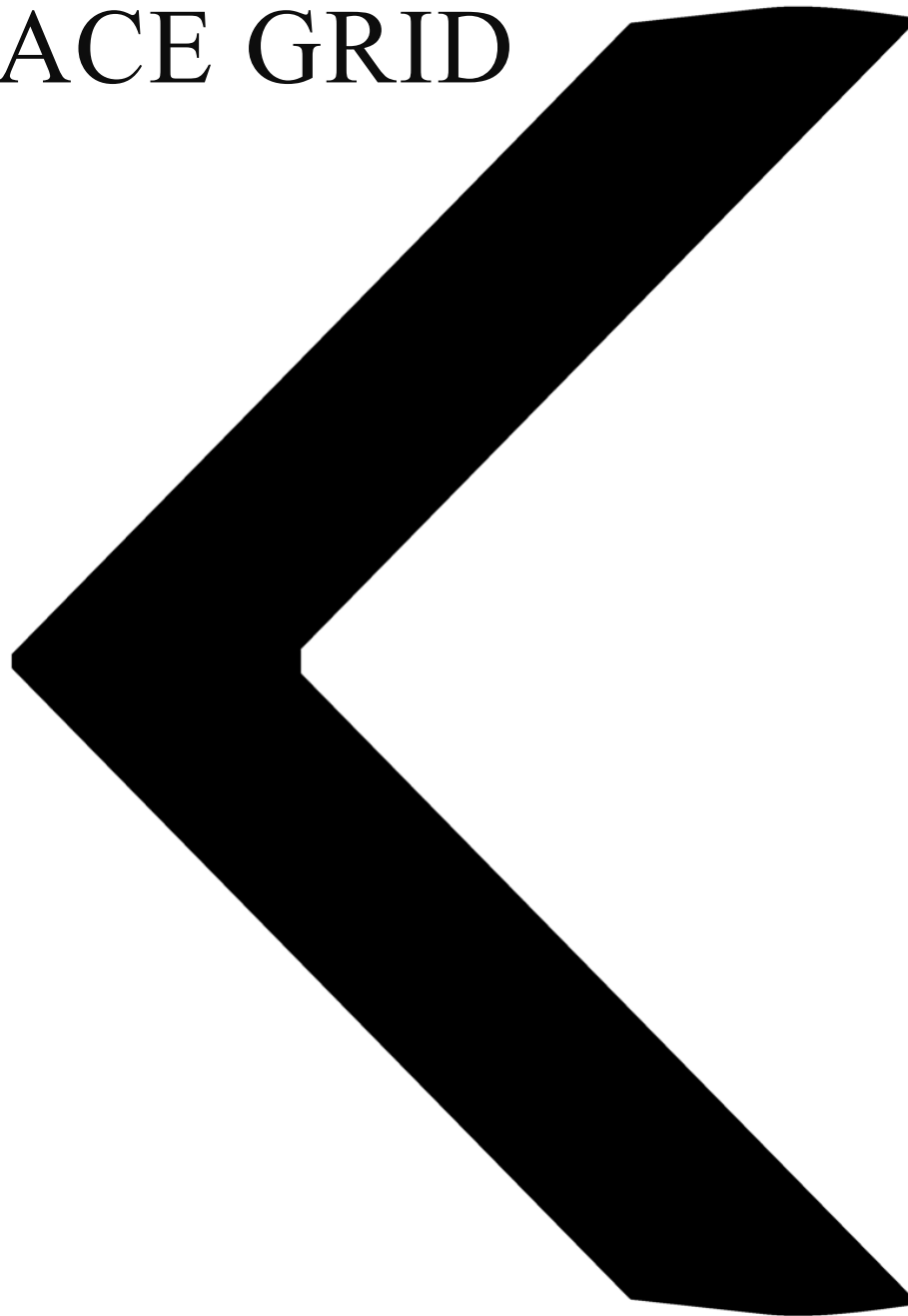




# C608 SURFACE GRID

Grid 100

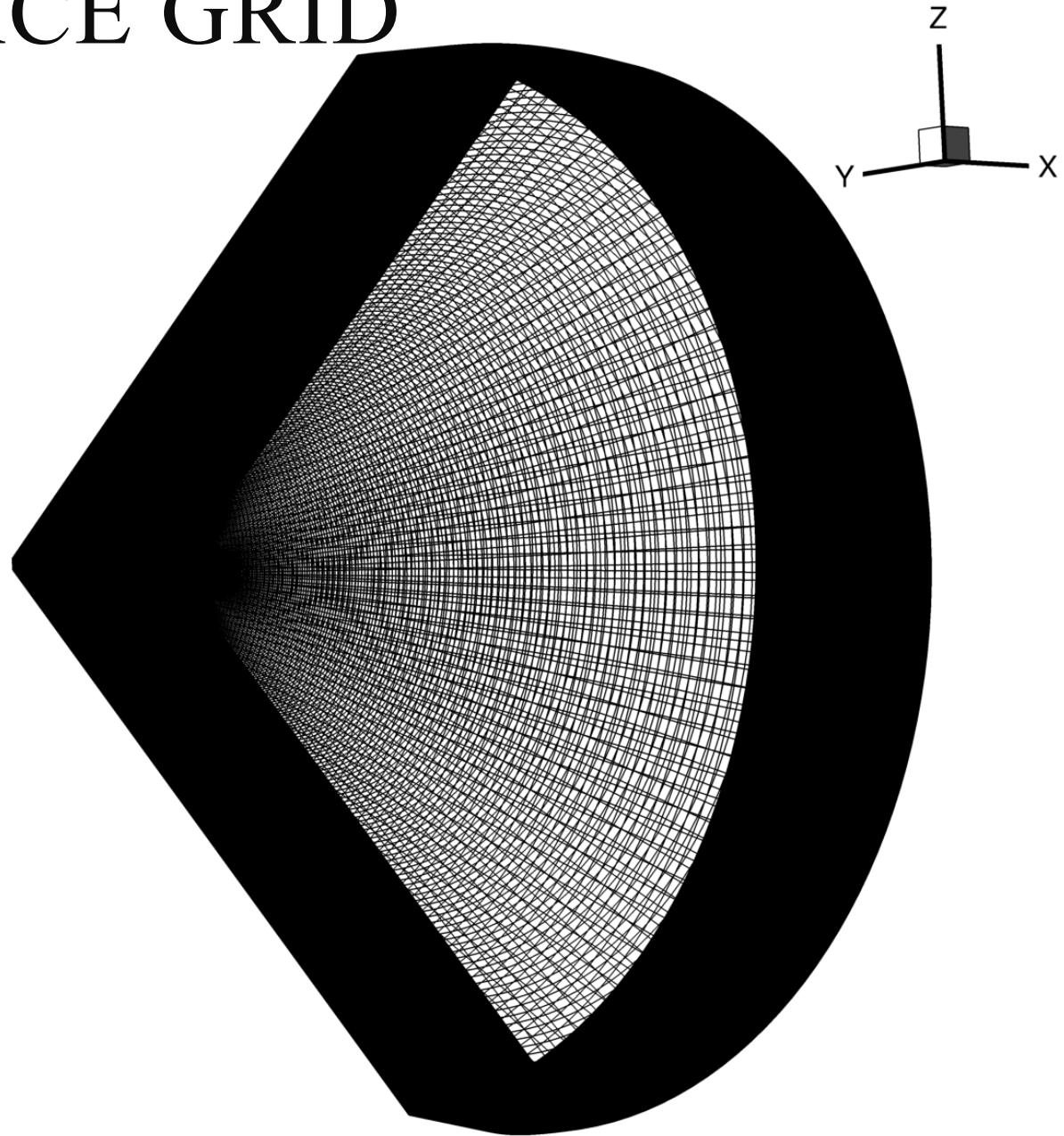
Mixed Element



# C608 SURFACE GRID

Grid 100

Mixed Element



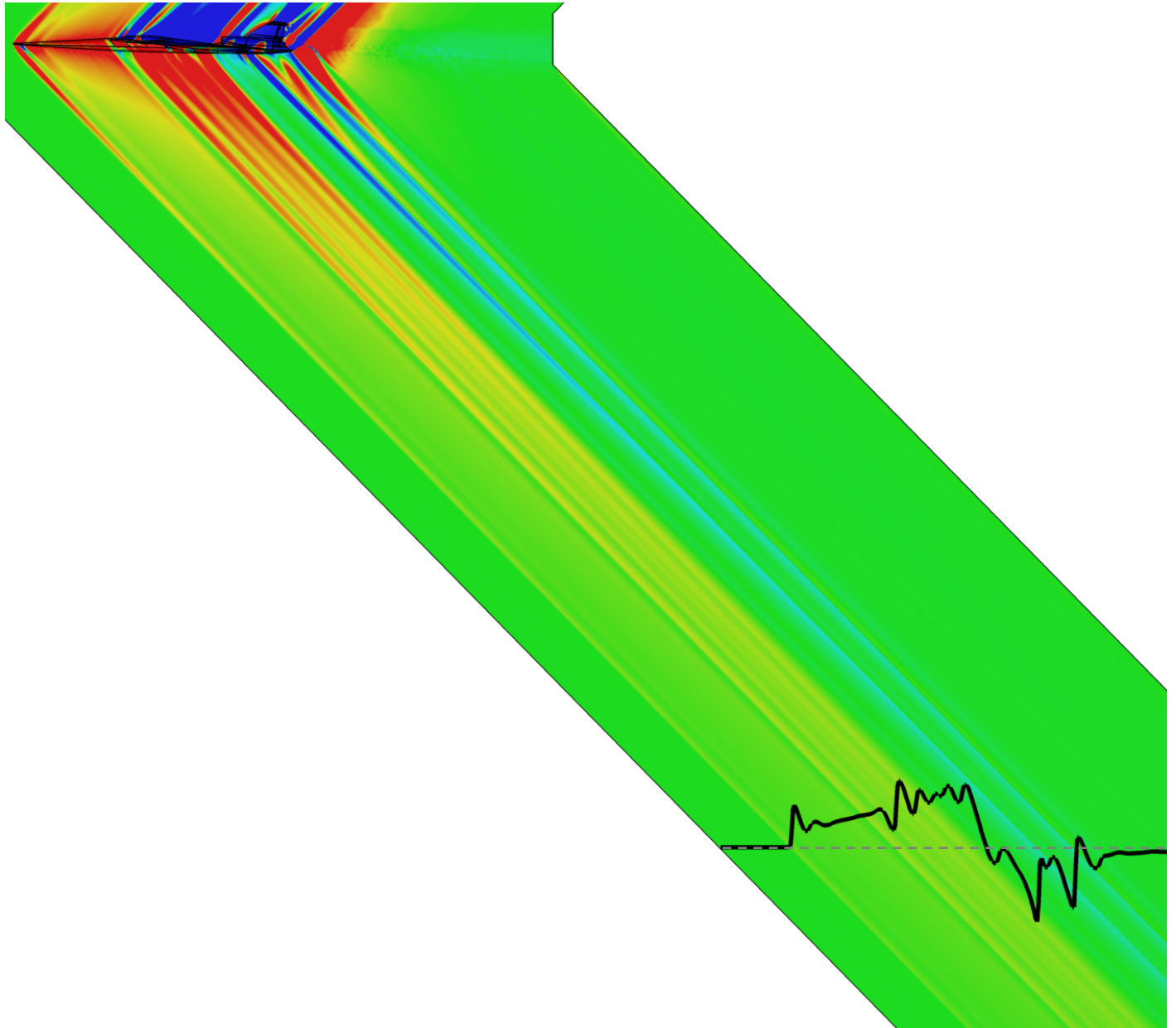
# C608 $dP/P_{INF}$

Grid 100

Tetrahedral

FUN3D

$dp/p_{\infty}$



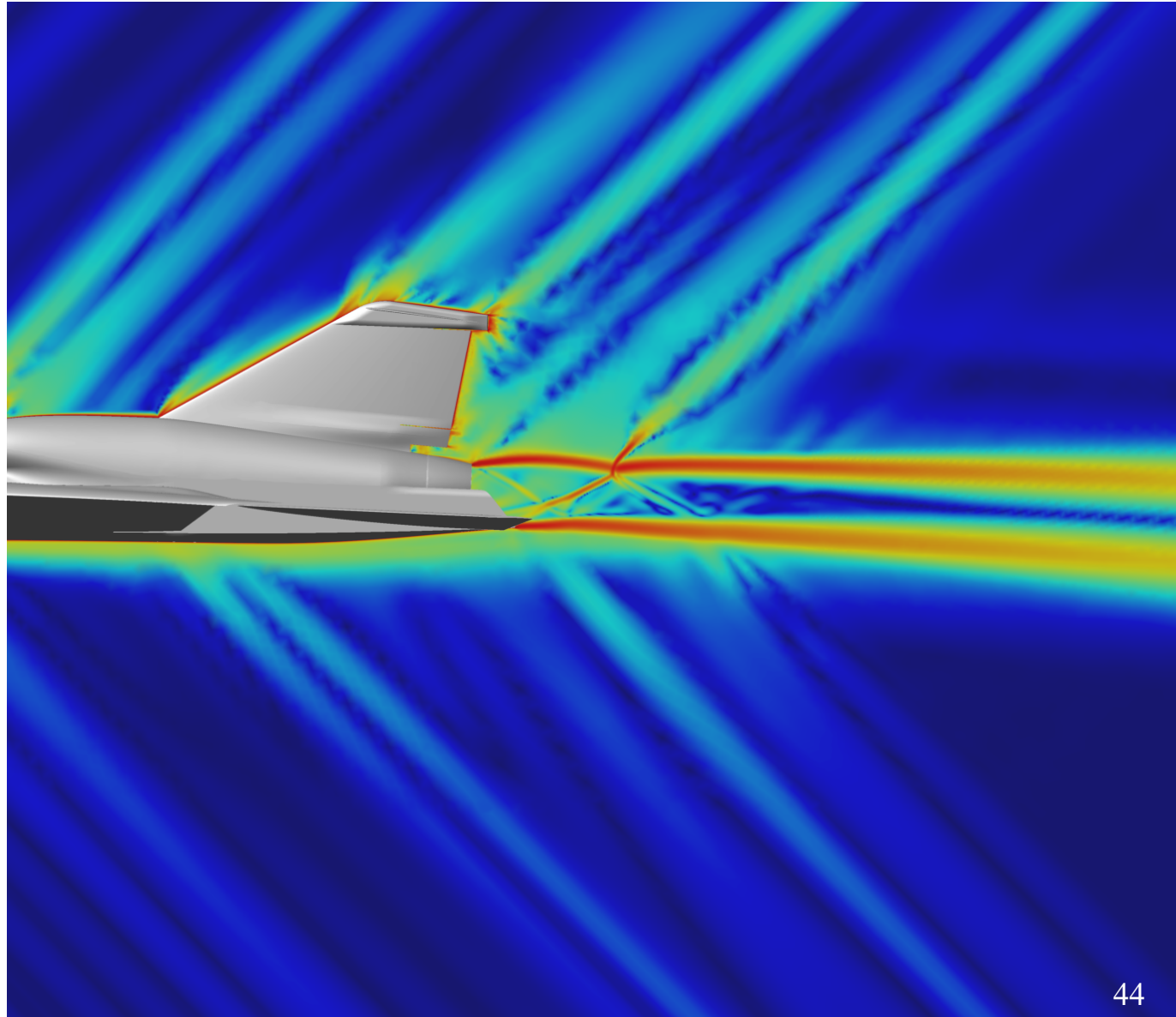
# C608 DENSITY GRADIENT

Grid 100

Tetrahedral

FUN3D

Density  
gradient  
(numerical  
schlieren)



# SUBMISSIONS AND ANALYSIS

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# EXTRACT SIGNATURES FROM VOLUME

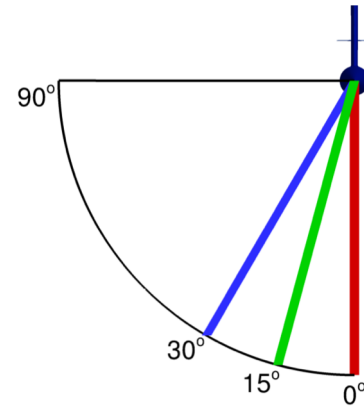
Tecplot macro was provided

## Biconvex

- Data taken to match experiment
- 3 cuts, at roughly 15-inch radius at different off-track angles (Phi)
  - $Z = -15.108$  inches at  $\text{Phi} = 0.26^\circ$
  - $Z = -14.496$  inches at  $\text{Phi} = 15.12^\circ$
  - $Z = -13.070$  inches at  $\text{Phi} = 30.15^\circ$

## C608

- 3 body lengths,  $L = 3,240$  inches
- $0^\circ - 180^\circ$  in  $2^\circ$  increments to obtain off-track angles



# DATA PROCESSING

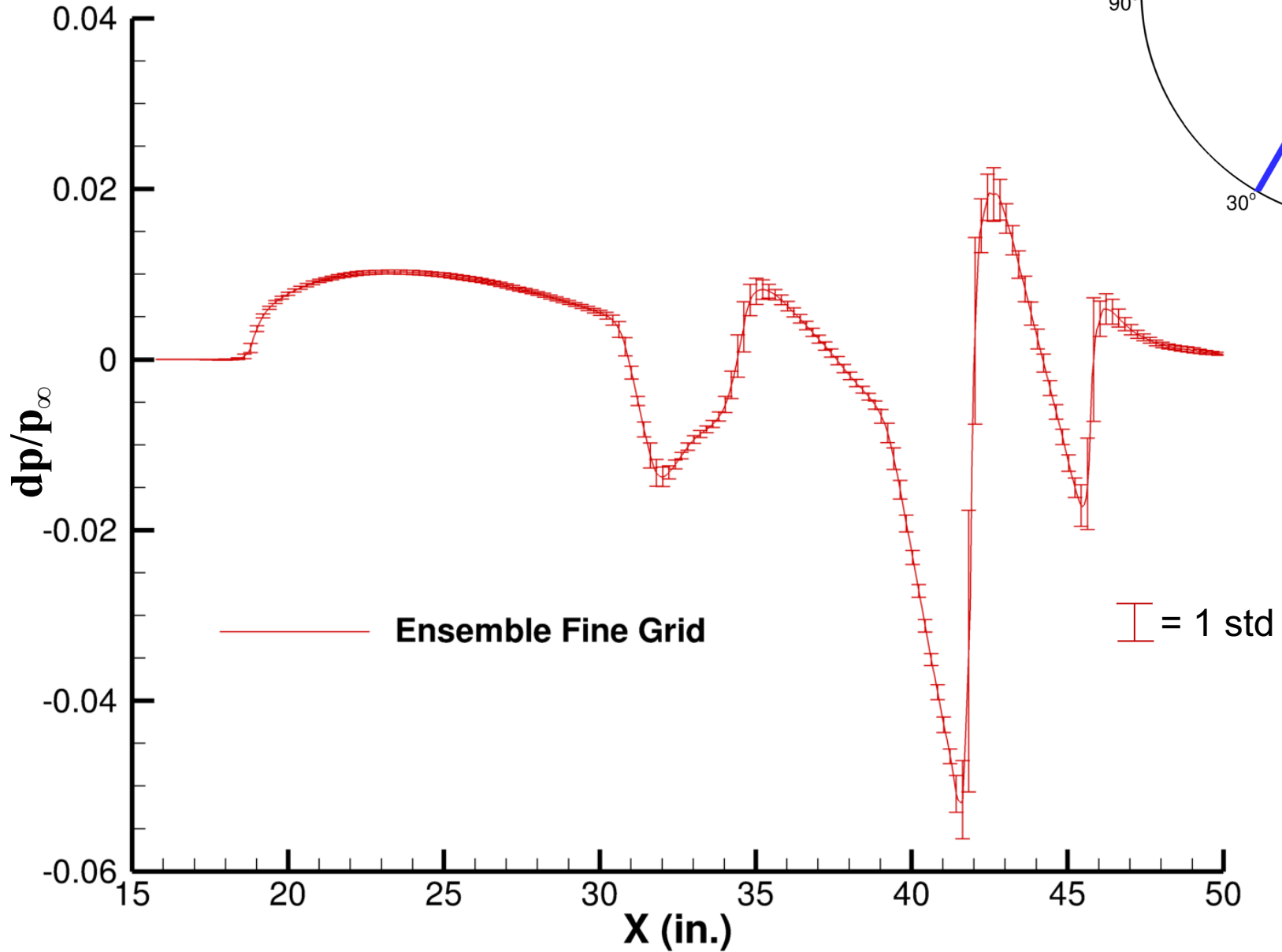
- Thank You! Consistency improved from second and first workshops
- Received signatures via SFTP or email
- Some were reformatted, zero padded, or sorted
- Data plotted
- Contacted participants for clarification/update when
  - Incorrect location or incomplete signature
  - Significant differences between submissions of same participant (iterative convergence)
  - Reference or boundary conditions suspect

# NEAR FIELD AND GROUND SIGNATURE STATISTICS

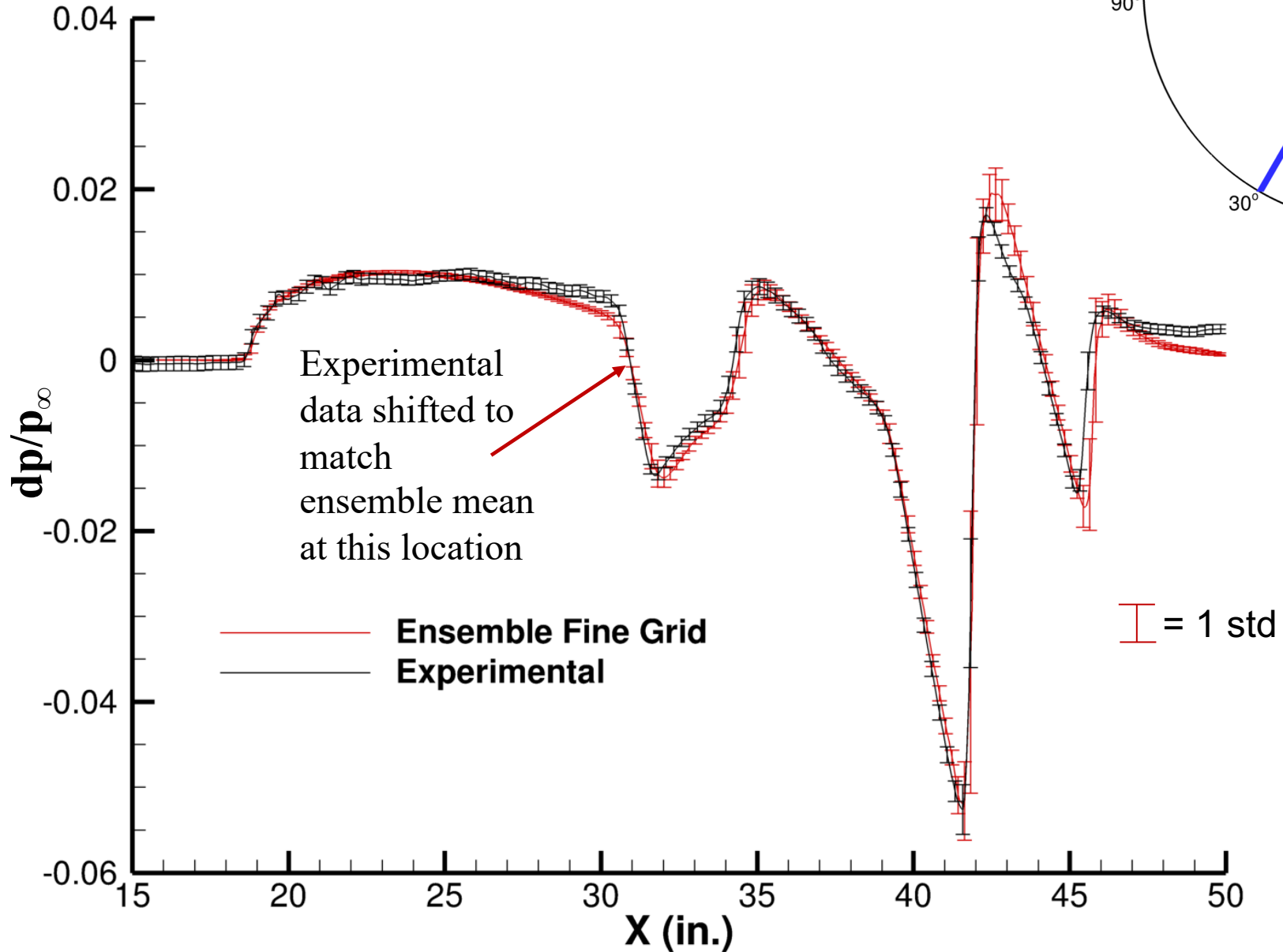
- Population mean and standard deviation of interpolated near field signature every 0.05 inch (Biconvex) or 0.5 inch (C608)
- Analogous to wind tunnel spatial averaging
- Indication of high variation areas to watch for in participant talks



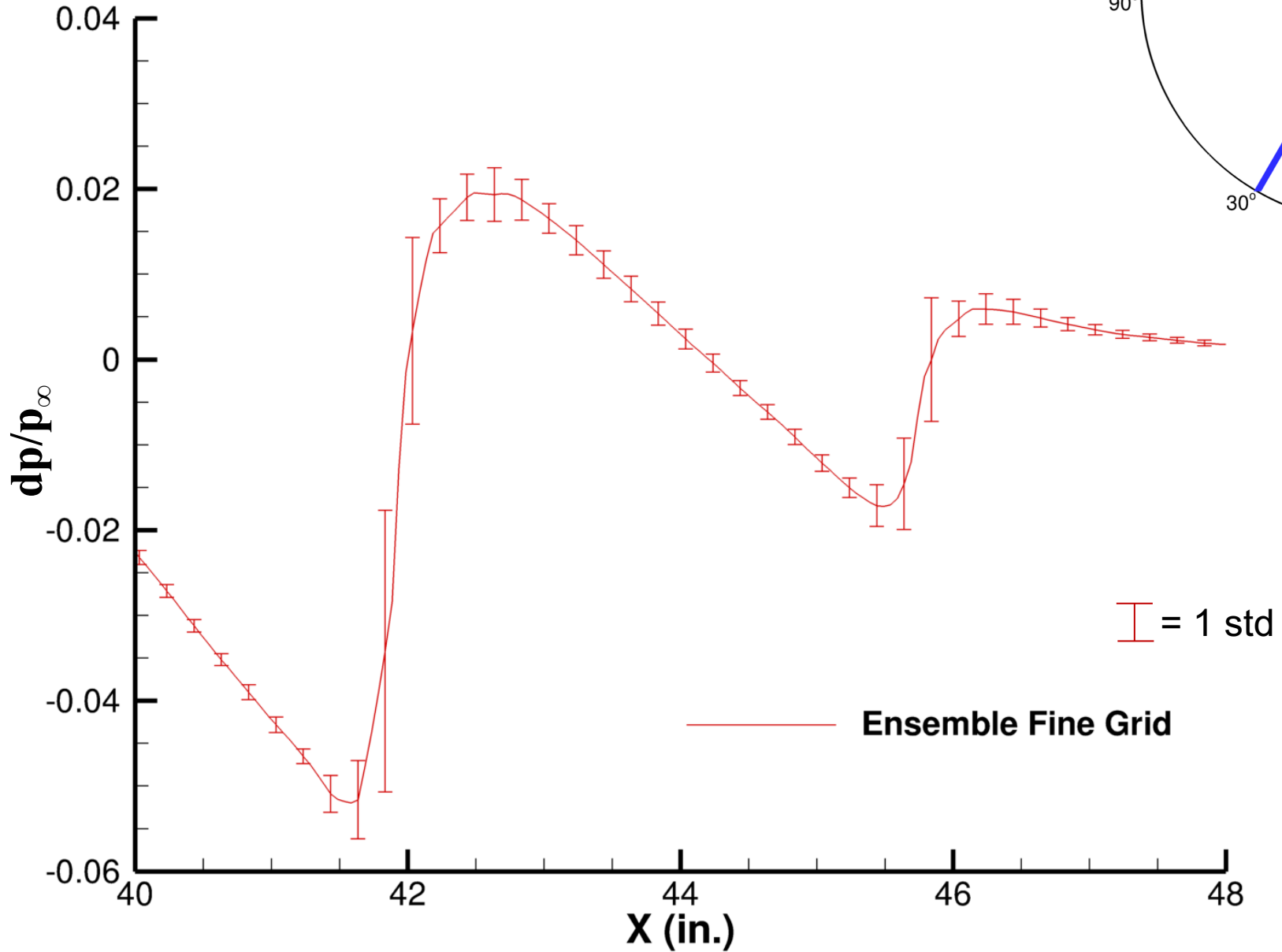
# BICONVEX FINE-GRID ENSEMBLE



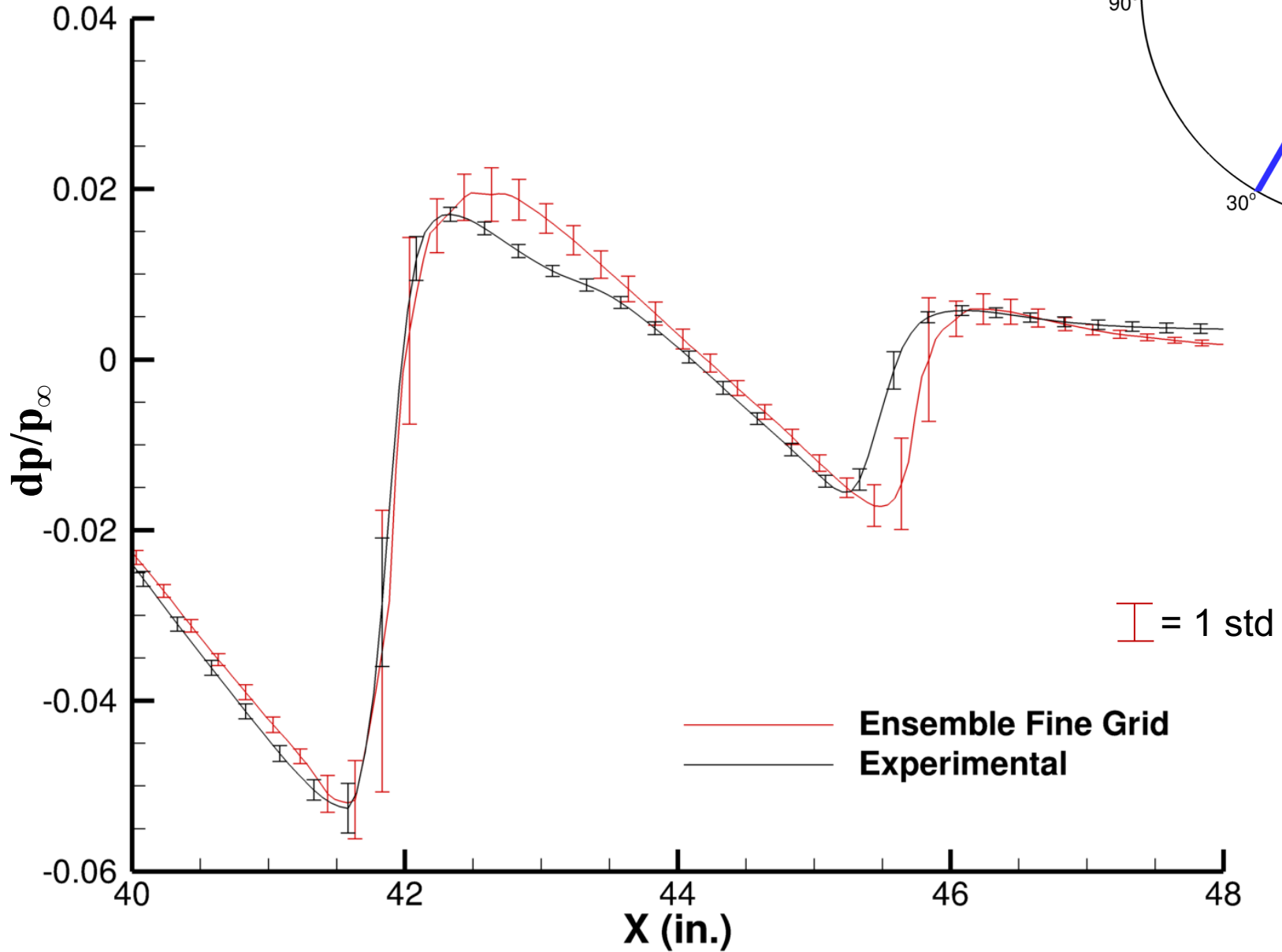
# BICONVEX FINE-GRID ENSEMBLE



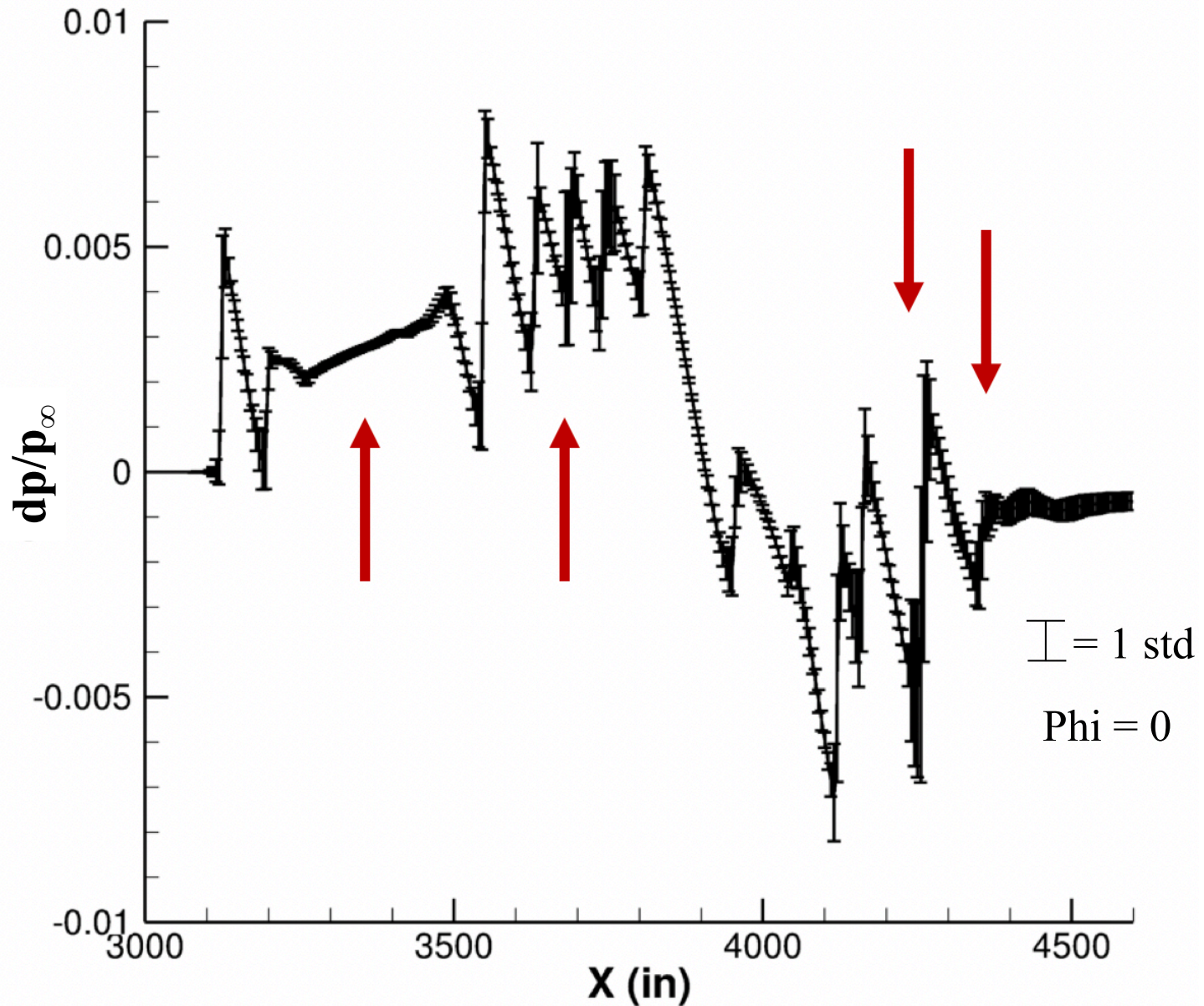
# BICONVEX FINE-GRID ENSEMBLE



# BICONVEX FINE-GRID ENSEMBLE



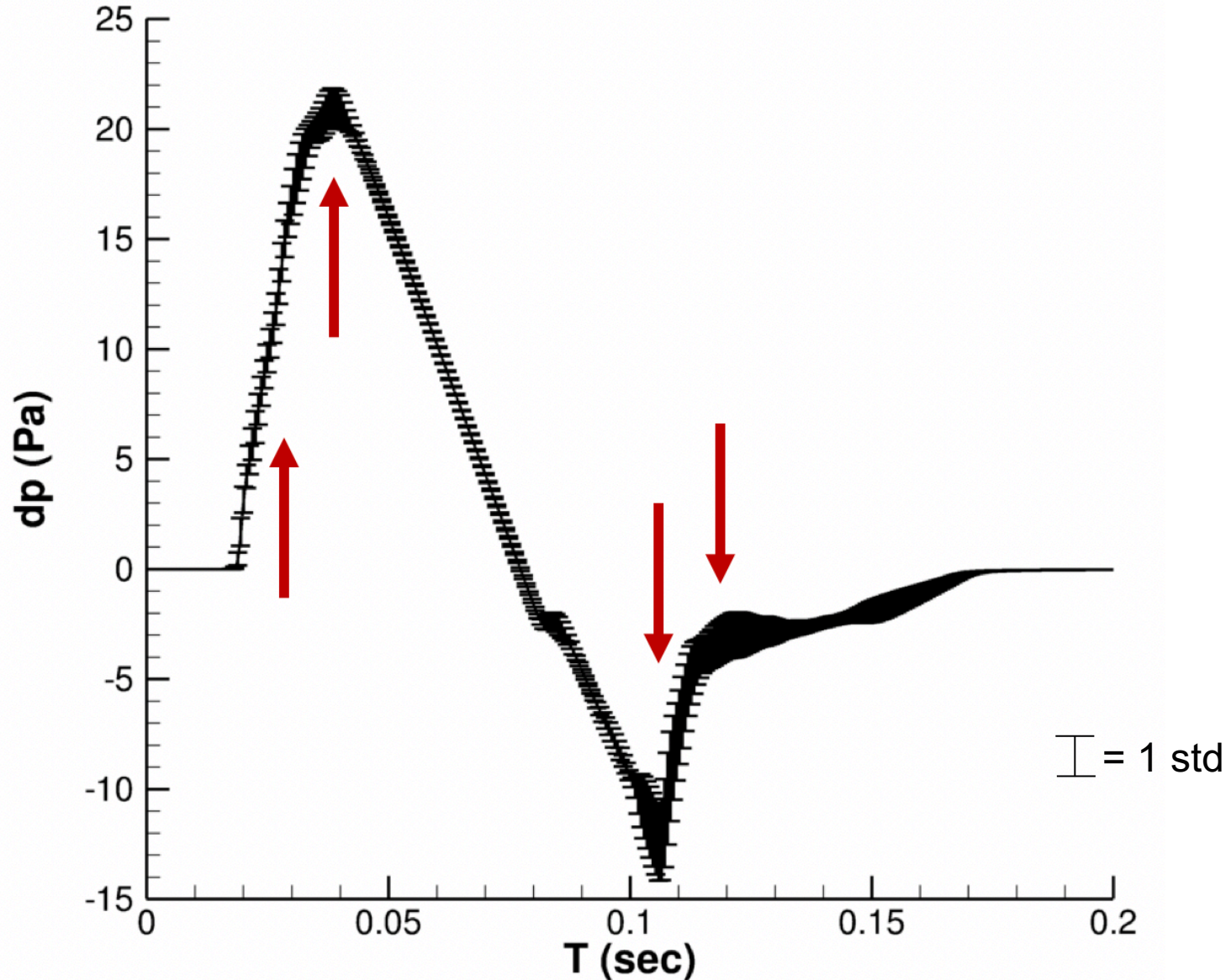
# C608 FINE-GRID ENSEMBLE



# GROUND PROPAGATION

- Geometry and grids provided in “full-scale”
- US Standard atmosphere and ANSI S1.26 Annex C relative humidity from 53200 ft. altitude
- sBOOM version 2.82 (Rallabhandi)
  - Burgers’ equation with molecular relaxation
- Submissions are windowed with fore and aft ramps

# C608 FINE-GRID ENSEMBLE PROPAGATED TO GROUND



# ACKNOWLEDGMENTS

- All participants
- Norma Farr, Scott Brynildsen, and Michael Wiese at Geolab for geometry preparation
- Alex Kleb for notice of intent assessment, C608 workshop grids, and C608 geometry assessment
- Jochen Kirz and Todd Michal for grid evaluation and feedback
- Joe Derlaga for statistical tools
- Mark Gammon and Nigel Taylor for geometry assessment
- NASA Commercial Supersonic Technology Project



# SUMMARY

More to follow after the participant talks

- Examination of outliers
- Propagation
- Loudness measures