

2nd Boom Prediction Workshop: Summary of Propagation Cases

Sriram K. Rallabhandi Alexandra Loubeau

NASA Langley Research Center

Motivation



- Commercial supersonic overland flight is currently prohibited
 - Supersonic overland flight is an enabler for entry into new vehicle market
- Replacing the prohibition with a certification standard requires an international effort to quantify the accuracy and reliability of prediction methods
- Deficiencies in existing methods should be noted to focus research on addressing weaknesses

Motivation



- The focus today was on atmospheric propagation
- Explore the issues
- Impartially compare:
 - Ground signatures at several azimuthal angles
 - Including lateral cut-offs
 - Under measured atmospheric conditions including winds
 - Loudness metrics
 - Primary boom carpets





Workshop Culture

- Adjectives such as good, bad, right, and wrong oversimplify issues and should be avoided
- Focus on describing observed differences and communicate why things are different

Cases



- LM1021 An optional cases from the 1st sonic boom prediction workshop
 - Ground signatures at -30°, 0° and 30° roll angles for atmospheric Profile1 (Required)
 - All other data (Optional)
- Axi-symmetric body A redesigned body of revolution that is close, in terms of the off-body pressure, to the C25F, a NASA low-Boom demonstration concept, for the near-field portion of this workshop
 - Ground signatures at -45°, 0° and 45° roll angles for atmospheric Profile3 (Required)
 - All other data (Optional)

Data Processing



- Thank You for all the submissions and participation!
- Received data via FTP or email
- Some had to be renamed, reformatted, zero padded, or sorted
- Plotted
- Contacted participants for clarification/update when
 - Significant or unexpected differences between submissions was observed in
 - Ground signatures
 - Loudness metrics etc.
 - Data missing

Summary of Perceived Level (PL)



- Metric for perceived level of loudness developed by Stevens
 - Developed to predict behavior of human auditory system in response to sound
- Adapted for use with sonic booms by Shepherd and Sullivan
- PL has been shown to correlate well with human perception of sonic booms heard outdoors
 - PL is used today to evaluate supersonic aircraft designs
- Uses signal spectrum in one-third-octave bands
- Uses a set of frequency weighting contours that vary with level
 - (By contrast, A-weighting contour does not vary with level)
 - Based on equal loudness contours for bands of noise
 - Extends down to 1 Hz, but this is an approximation
- Band of highest weighted level is the most important to overall level
- PL calculated and reported here

S. S. Stevens. Perceived level of noise by Mark VII and decibels (E). J. Acoust. Soc. Am., 51(2):575–601, 1972.

K. P. Shepherd and B. M. Sullivan. A loudness calculation procedure applied to shaped sonic booms. NASA Technical Report TP-3134, 1991.

Calculation Steps for Perceived Level (PL)

- 1. Calculate Sound Pressure Level of signal in 1/3-octave bands
- 2. Apply frequency weighting for loudness of individual bands
 - where loudness of 1 sone is referenced to 1/3-oct band of noise at 3150 Hz at 32 dB
- 3. Apply summation rule for total loudness

$$S_t = S_m + F(\Sigma S - S_m)$$

where

 S_t = total loudness

 S_m = loudness of loudest band ΣS = sum of loudnesses of all the bands

- F = fractional factor based on S_m
- 4. Convert to PL in dB

 $PL = 32 + 9 \log_2(S_t)$





Submissions





LM1021 profile1 Hydrostatic ASEL build-up at phi=0.0



LM1021 profile1 Hydrostatic Submitted Loudness Carpets



Perceived Level (dB)

LM1021 – Profile1, Hydrostatic, Phi = 0°







Sriram.Rallabhandi@nasa.gov

LM1021 – Profile1, Hydrostatic, Phi = 0°





LM1021 – Profile1, Linear, Phi = 0°





LM1021 – Profile1, Linear, Carpet PL





Sriram.Rallabhandi@nasa.gov

LM1021 – Profile1, Hydrostatic, Phi = -30°





Sriram.Rallabhandi@nasa.gov

LM1021 – Profile1, Hydrostatic, Phi = -30°





Sriram.Rallabhandi@nasa.gov

LM1021 – Profile1, Hydrostatic, Phi = -30°





LM1021 – Profile1, Linear, Phi = -30°





LM1021 – Profile1, Hydrostatic, Phi = 30°





Sriram.Rallabhandi@nasa.gov

LM1021 – Profile1, Hydrostatic, Phi = 30°





Sriram.Rallabhandi@nasa.gov

LM1021 – Profile1, Hydrostatic, Phi = 30°





LM1021 – Profile1, Linear, Phi = 30°





LM1021 – Profile1, Hydrostatic, Ranges - PL



PL vs. Ground Intersections



Sriram.Rallabhandi@nasa.gov

NASA

LM1021 – Profile1, PL Submitted Statistics







LM1021 – Std Profile, Hydrostatic, Phi = 0°





Sriram.Rallabhandi@nasa.gov

LM1021 – StdProfile, Hydrostatic, Phi = 0°





Sriram.Rallabhandi@nasa.gov

LM1021 – Std Profile, Hydrostatic, Carpet PL





LM1021 – Std Profile, Hydrostatic, Carpet PL





Sriram.Rallabhandi@nasa.gov

LM1021 – Std Profile, Hydrostatic, Phi = 0°



LM1021 stdprofile Hydrostatic Submitted and Computed PLs and ASELs at phi=0.0



Sriram.Rallabhandi@nasa.gov

LM1021 – Std Profile, Hydrostatic, Phi = 0°





LM1021 – Std Profile, Hydrostatic, Phi = -30°





Sriram.Rallabhandi@nasa.gov

LM1021 – Std Profile, Hydrostatic, Phi = -30°



_M1021 stdprofile Hydrostatic Submitted and Computed PLs and ASELs at phi=-30.0



Sriram.Rallabhandi@nasa.gov

LM1021 – Std Profile, Hydrostatic, Phi = -30°





LM1021 – Std Profile, Ranges-PL



PL vs. Ground Intersections



Sriram.Rallabhandi@nasa.gov
AXIBODY– Profile3, Hydrostatic, Phi = 0°





AXIBODY-Profile3, Mean and Std. Deviation





Sriram.Rallabhandi@nasa.gov

AXIBODY- Profile3, Hydrostatic, Carpet PL





AXIBODY– Profile3, Hydrostatic, Phi = 0°





Sriram.Rallabhandi@nasa.gov

AXIBODY– Profile3, Hydrostatic, Phi = 0°





AXIBODY– Profile3, Linear, Phi = 0°





AXIBODY– Profile3, Linear, Carpet PL





AXIBODY– Profile3, Linear, Phi = 0°





Sriram.Rallabhandi@nasa.gov

AXIBODY– Profile3, Hydrostatic, Phi = -45°





AXIBODY– Profile3, Hydrostatic, Phi = -45°





Sriram.Rallabhandi@nasa.gov

AXIBODY– Profile3, Hydrostatic, Phi = -45°





Sriram.Rallabhandi@nasa.gov

AXIBODY– Profile3, Linear, Phi = -45°





AXIBODY– Profile3, Hydrostatic, Phi = 45°





Sriram.Rallabhandi@nasa.gov

AXIBODY– Profile3, Linear, Phi = 45°





AXIBODY-Profile3, Hydrostatic, Ranges - PL







Sriram.Rallabhandi@nasa.gov





AXIBODY– StdProfile, Hydrostatic, Phi = 0°





AXIBODY- StdProfile, Hydrostatic, Carpet PL





AXIBODY- Carpet PLs, Std Vs. StdRH70





Sriram.Rallabhandi@nasa.gov

AXIBODY– StdProfile, Hydrostatic, Phi = 0°





AXIBODY– StdProfile, Linear, Phi = 0°





AXIBODY- StdProfile, Linear, Carpet PL





AXIBODY– StdProfile, Hydrostatic, Phi = -45°





Sriram.Rallabhandi@nasa.gov

AXIBODY– StdProfile, Linear, Phi = -45°





Sriram.Rallabhandi@nasa.gov

AXIBODY- StdProfile, Hydrostatic, Ranges - PL

NASA

PL vs. Ground Intersections



1/3-Octave-Band and Loudness Spectra



62

Spectra indicate the energy in different 1/3-octave frequency bands

Loudness spectra indicate the frequency bands which are most important to the calculation of PL (which approximates the sensitivity of human hearing)



Axi-symmetric, Standard Atm, Phi = -45°





Axi-symmetric, Standard Atm, Phi = 0°





Axi-symmetric, Standard Atm, Phi = $+45^{\circ}$





Axi-symmetric, Atm Profile 3, Phi = -45°





Axi-symmetric, Atm Profile 3, Phi = 0°





Axi-symmetric, Atm Profile 3, Phi = $+45^{\circ}$





LM1021, Standard Atm, Phi = -30°





LM1021, Standard Atm, Phi = 0°





LM1021, Standard Atm, Phi = $+30^{\circ}$
















Noise Metrics Analysis

- Several loudness metrics are available: A/B/C/D/E/Z weighting
- Each has different weighting at different frequencies







Noise Metrics Analysis

- Six noise metrics were calculated
 - PL
 - ASEL, BSEL, DSEL, ESEL
 - ISBAP = PL + 0.4201(CSEL-ASEL)
- These metrics have been found to correlate well with human annoyance (indoors and outdoors)
 - Based on meta-analysis of a variety of laboratory studies*
- Violin plots show distribution of data in addition to summary statistics



*A. Loubeau, Y. Naka, B. G. Cook, V. W. Sparrow, and J. M. Morgenstern. A new evaluation of noise metrics for sonic booms using existing data. 20th International Symposium on Nonlinear Acoustics, 2015.

Axi-symmetric Case, All Atmospheres





Axi-symmetric Case





LM1021 Case, All Atmospheres





LM1021 Case





Effect of Constant 70% Relative Humidity







- Most results match under-track in terms of ground signatures
- The discrepancy seems to increase for off-track roll angles, particularly near lateral cut-offs
- The PL calculation from some participants seems off
- Atmospheric pressure interpolation scheme has a significant impact on the propagated signatures
- There seems to be a discrepancy in the wind convention used by different participants need to make this consistent
- Realistic atmospheric profiles have a significant impact on the propagated signatures, carpet ranges and loudness metrics
- Higher sampling frequencies (>100 kHz) seem warranted for loudness convergence < 0.1 dB

Future Work



- Dig deeper into the statistics of different submissions
- Narrow band and 1/3 octave band spectral comparisons of all submissions
- Ranges
- Loudness build-ups and additional diagnostics
- •AVIATION 2017: Paper/presentation on extensive discussions of the submissions and additional comparisons, Sriram K. Rallabhandi, Alexandra Loubeau
- ASA, Boston 2017: Paper presentation on lessons learned, and progress made between the workshops and an informal propagation comparisons done in 2013

Acknowledgments



- NASA Commercial Supersonic Technology (CST) project
- Boom prediction workshop organizing committee and participants
- Mike Park, CASB, for sharing relevant data and information from previous workshops

Discussion



- Were the cases used in SBPW2 appropriate?
- What's the best dissemination methods for all participants



- Goals
- Cases
 - •Need input from other participants
- Potential additional investigations
 - Maneuvers/Trajectories
 - Focus and location of caustics
 - Over-the-top secondary booms
 - Turbulence
 - Irregular terrain
 - Ground impedance
 - Curved earth effects
 - Shadow zone calculations

SBPW3



- Potential additional information to gather
 - Frequency spectra
 - Execution time (wall clock?)
 - Propagation time to ground
 - Ray tube area
- Will specify wind convention and atmospheric condition interpolation method (or provide fine resolution)



EXTRAS

LM1021 – Std Profile 70, Hydrostatic, Phi = 0.0







LM1021 - Std Profile 70, Linear, Phi = 0.0



LM1021 – Std Profile 70, Hydrostatic, Phi = -30.0





LM1021 – Std Profile 70, Linear, Phi = -30.0



AXIBODY-Std70, Hydrostatic, Phi = 0.0



AXIBODY– Std70, Linear, Phi = 0.0



AXIBODY– Std70, Hydrostatic, Phi = -45.0



Sriram.Rallabhandi@nasa.gov

Sampling Freq. (kHz)

-0.5

Р#

P5 P8



AXIBODY-Std70, Linear, Phi = -45.0



AXIBODY– Std70, Hydrostatic, Phi = 45.0





AXIBODY- Std70, Linear, Phi = 45.0





AXIBODY-Profile4, Hydrostatic, Phi = 0.0





AXIBODY-Profile4, Linear, Phi = 0.0





AXIBODY– Profile4, Hydrostatic, Phi = -45.0





AXIBODY– Profile4, Linear, Phi = -45.0



AXIBODY– Profile4, Hydrostatic, Phi = 45.0







LM1021 – Profile2, Hydrostatic, Phi = 0.0





LM1021 – Profile2, Linear, Phi = 0.0



LM1021 – Profile2, Hydrostatic, Phi = -30.0





LM1021 – Profile2, Linear, Phi = -30.0




LM1021 – Profile2, Hydrostatic, Phi = 30.0



Sriram.Rallabhandi@nasa.gov



LM1021 – Profile2, Linear, Phi = 30.0



Sriram.Rallabhandi@nasa.gov

NASA

AXIBODY- StdProfile, Hydrostatic, Phi = 45.0





AXIBODY– StdProfile, Linear, Phi = 45.0







11 2 ¹¹³









11 5 ¹¹⁵

Axi-symmetric, Atm Profile 4, Phi = -45°





11 6 ¹¹⁶

Axi-symmetric, Atm Profile 4, Phi = 0°





11 7 ¹¹⁷

Axi-symmetric, Atm Profile 4, Phi = $+45^{\circ}$





11 8 ¹¹⁸





11 9 ¹¹⁹





12 0 ¹²⁰









12 2¹²²





12 2 ¹²³





12 1¹²⁴