

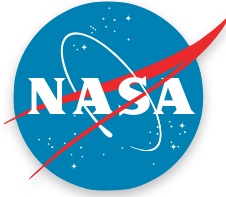
# Cart3D Simulations for the First AIAA Sonic Boom Prediction Workshop

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**Marian Nemec**

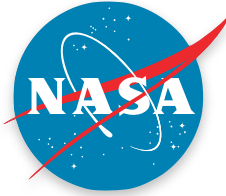
Science and Technology Corp.  
Applied Modeling & Simulations Branch  
Moffett Field, CA 94035  
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## Note:

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- Full paper available on-line AIAA 2014-0558
- Presentation is Tuesday Jan 14 @ 3:30 in Applied CFD



# Introduction – Cart3D

## Meshing:

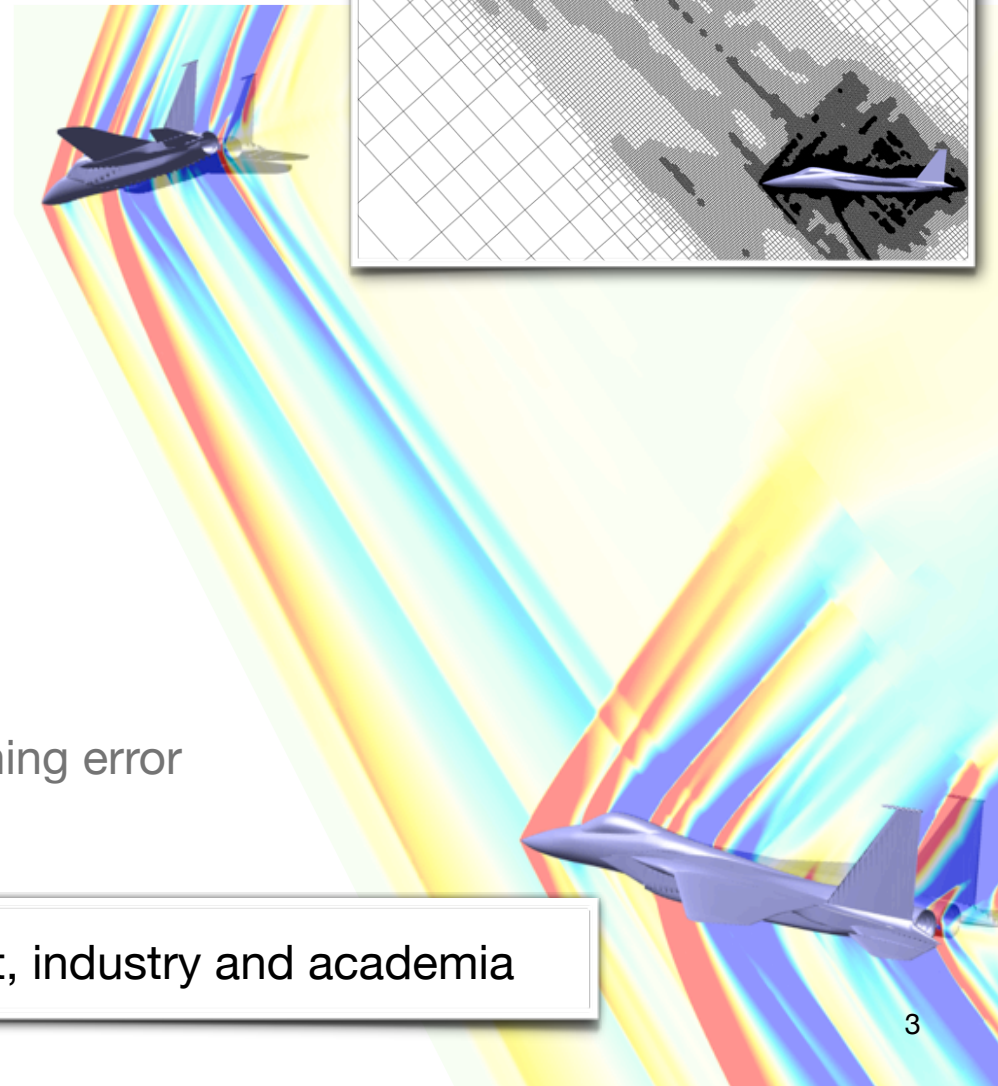
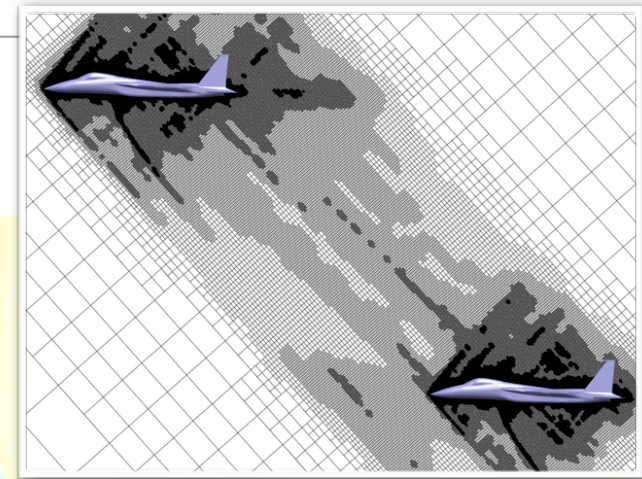
- Multi-level Cartesian mesh with embedded boundaries
- Insensitive to geometric complexity
- Adjoint-based mesh adaptation

## Inviscid flow solver

- Monotone second-order upwind method
- Tensor slope limiters preserve k-exactness
- Runge-Kutta with multigrid acceleration
- Domain decomposition for scalability

## Output-based mesh adaptation

- Duality-preserving discrete adjoint
- Provides output correction & error estimate
- Adjoint-based mesh refinement using remaining error



Broad use throughout NASA, US Government, industry and academia



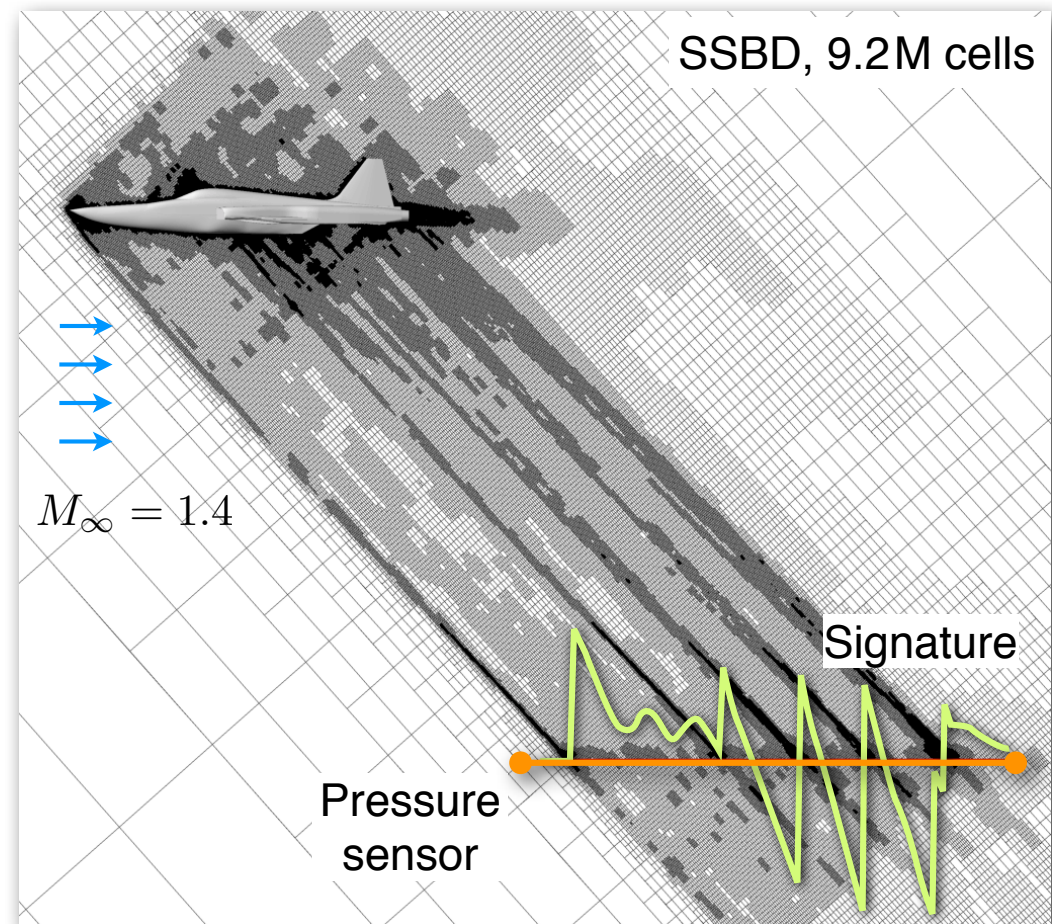
# Boom problems with Cartesian Mesh Methods

Goal: Accurate prediction of near/mid-field pressure signatures

- Mesh adaptation to pressure sensor output

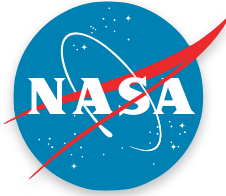
$$\mathcal{J}_{\text{sensor}} = \int_0^L \frac{(p - p_\infty)^2}{p_\infty} dl$$

- Mesh rotation to  $\sim$ Mach angle
- Mesh stretching along dominant direction of wave propagation
- See: *AIAA 2008-0725*, 6593 & *AIAA 2013-0649*



*AIAA 2008-6593, Wintzer et al.*





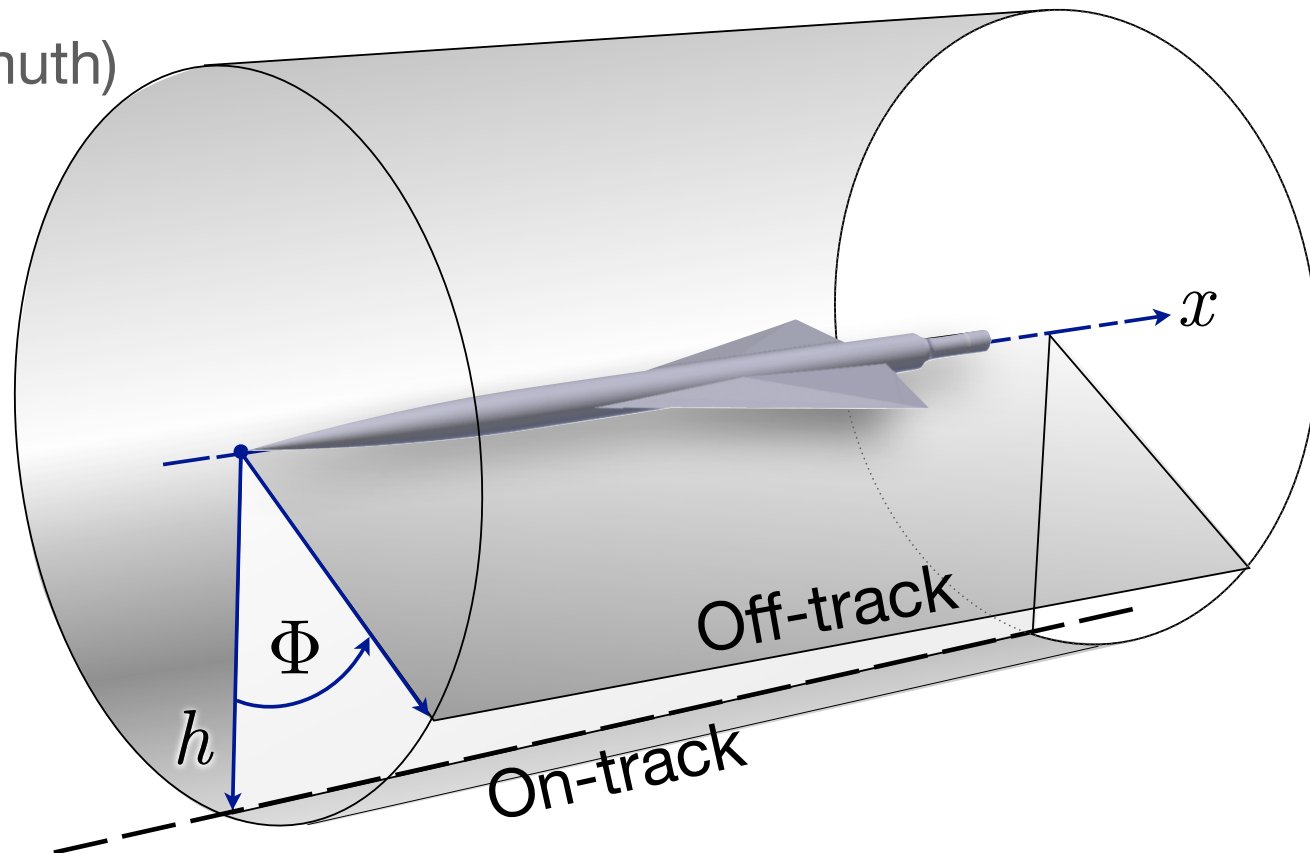
# Nomenclature

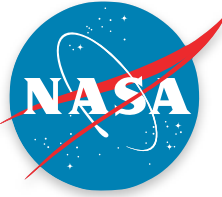
Cylindrical coordinates used for sonic boom

$x$  : Distance along sensor (axial distance)

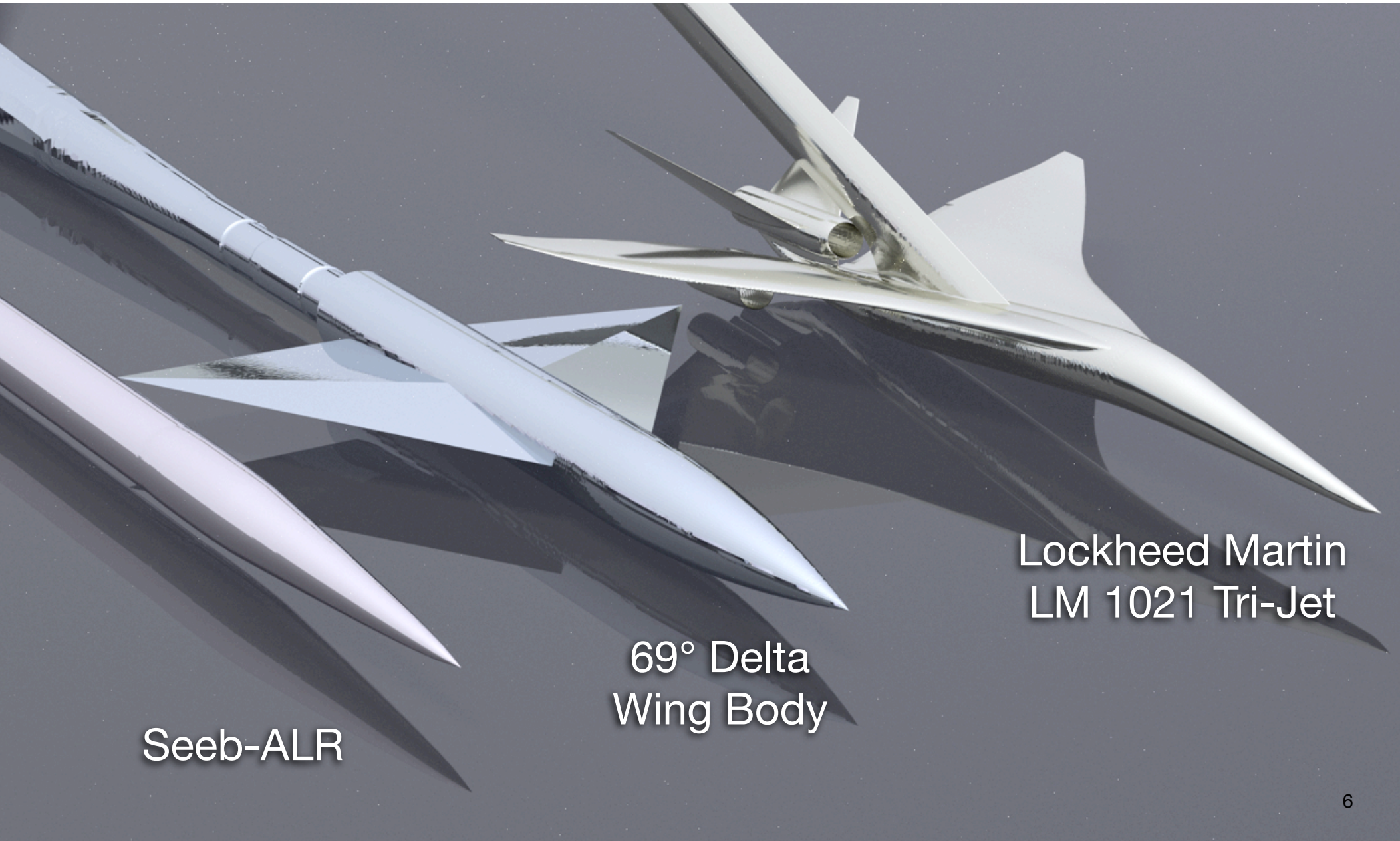
$h$  : Distance from axis (radius)

$\Phi$  : Off-track angle (azimuth)





# Results and Investigations

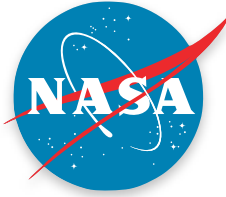


Seeb-ALR

69° Delta  
Wing Body

Lockheed Martin  
LM 1021 Tri-Jet

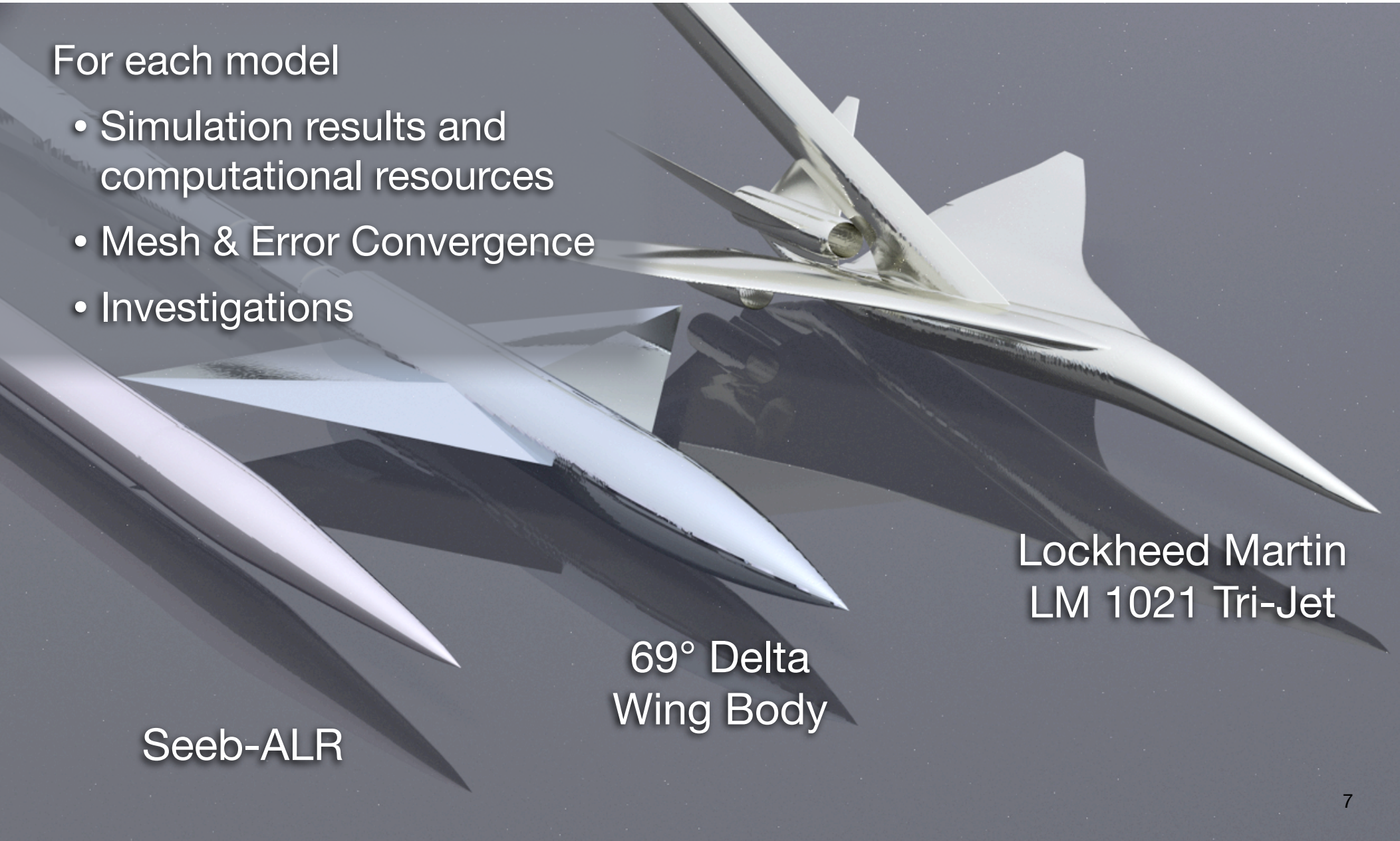




# Results and Investigations

For each model

- Simulation results and computational resources
- Mesh & Error Convergence
- Investigations

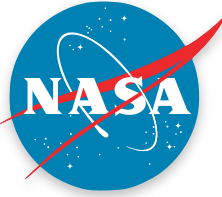


Seeb-ALR

69° Delta  
Wing Body

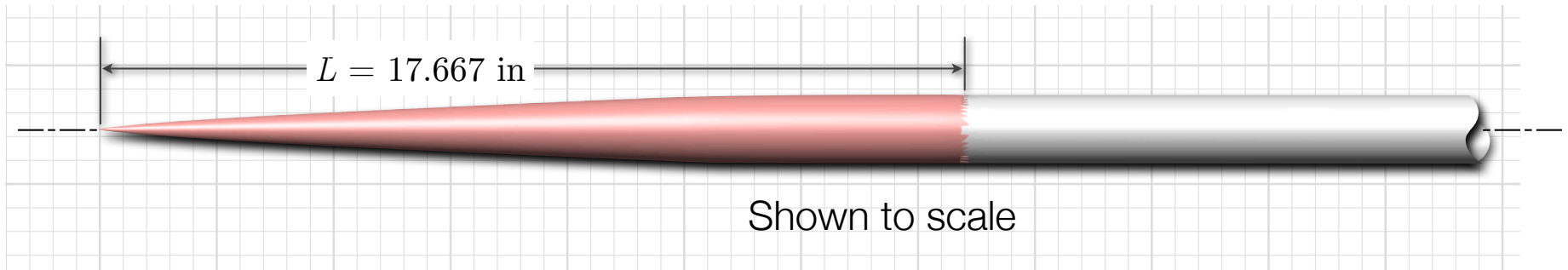
Lockheed Martin  
LM 1021 Tri-Jet





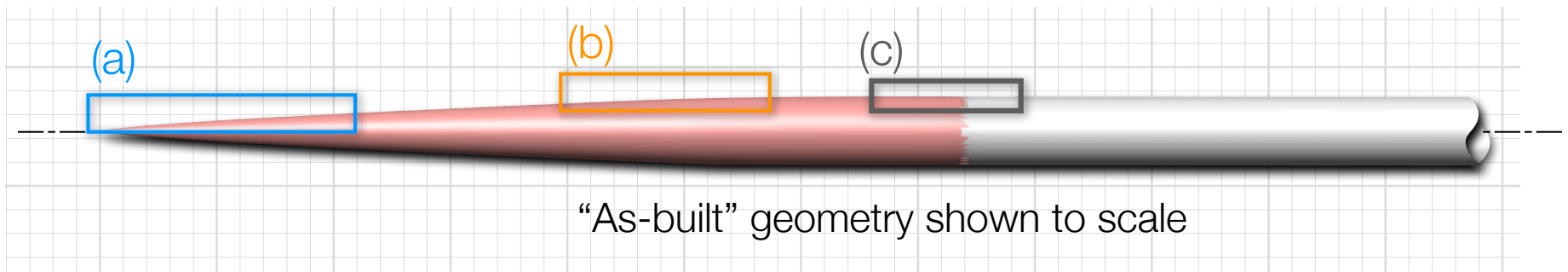
# Case 1 – Seeb-ALR

$$M_{\infty} = 1.6, \alpha = 0^{\circ}$$



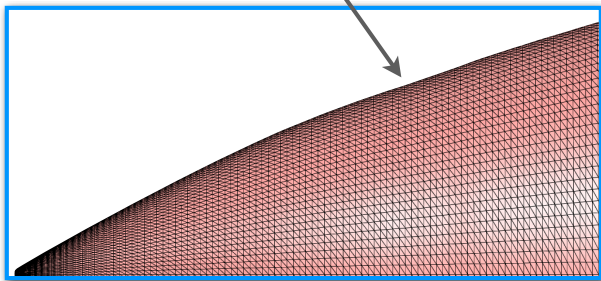
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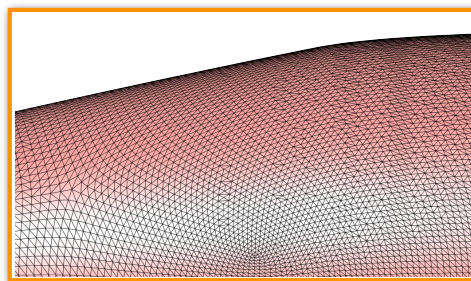


Detail with axial scale compressed 5x

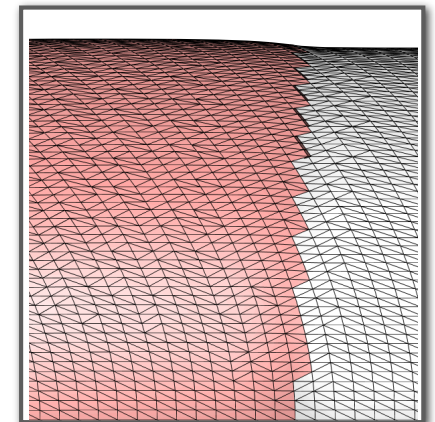
(a) Slight inflection (concavity)

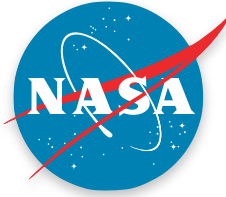


(b) Surface mesh at shoulder



(c) Aft cylindrical juncture

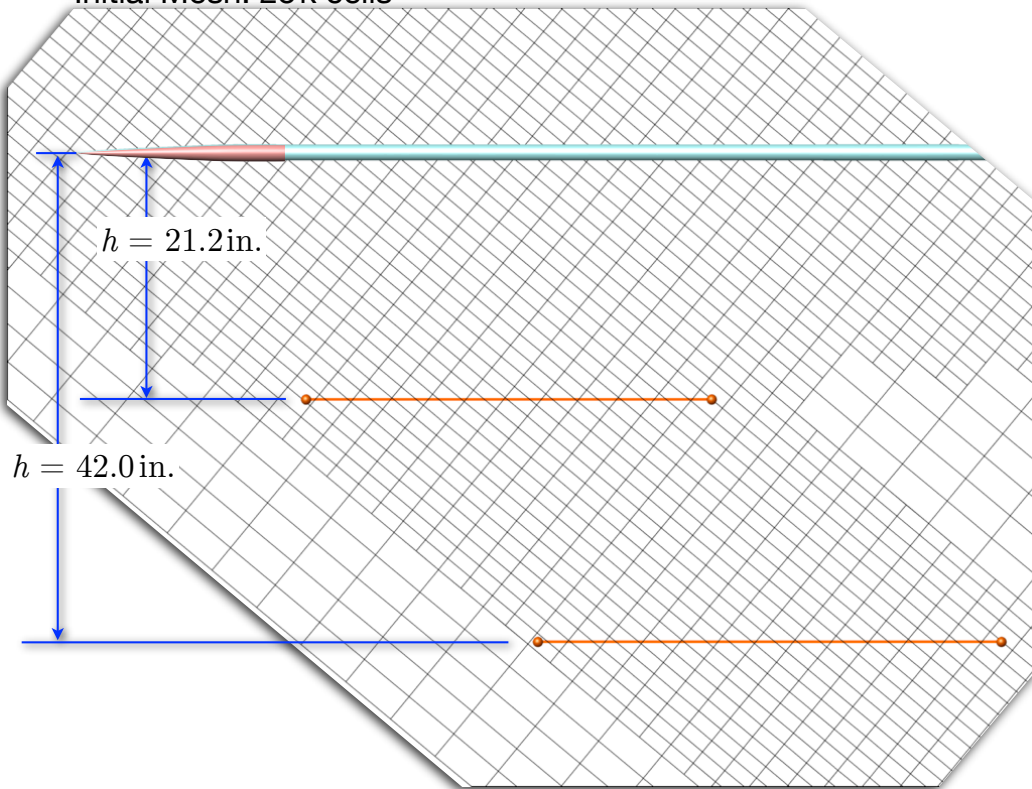




# Seeb-ALR: Meshing

$M_\infty = 1.6$ ,  $\alpha = 0^\circ$ , On-track @  $h = 21.2$  in. & 42 in.

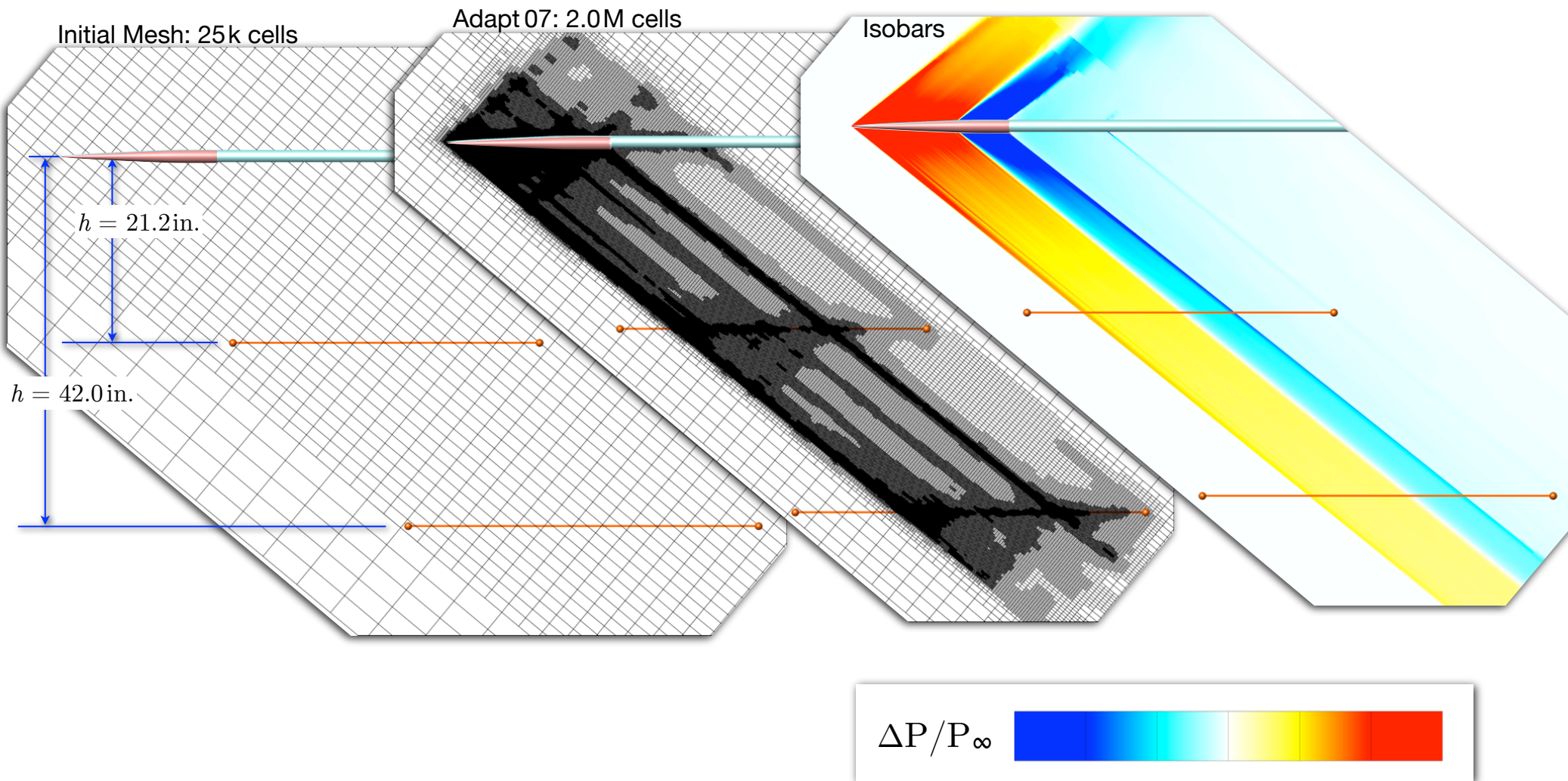
Initial Mesh: 25k cells

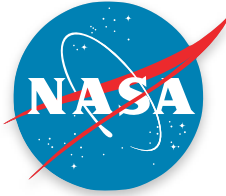




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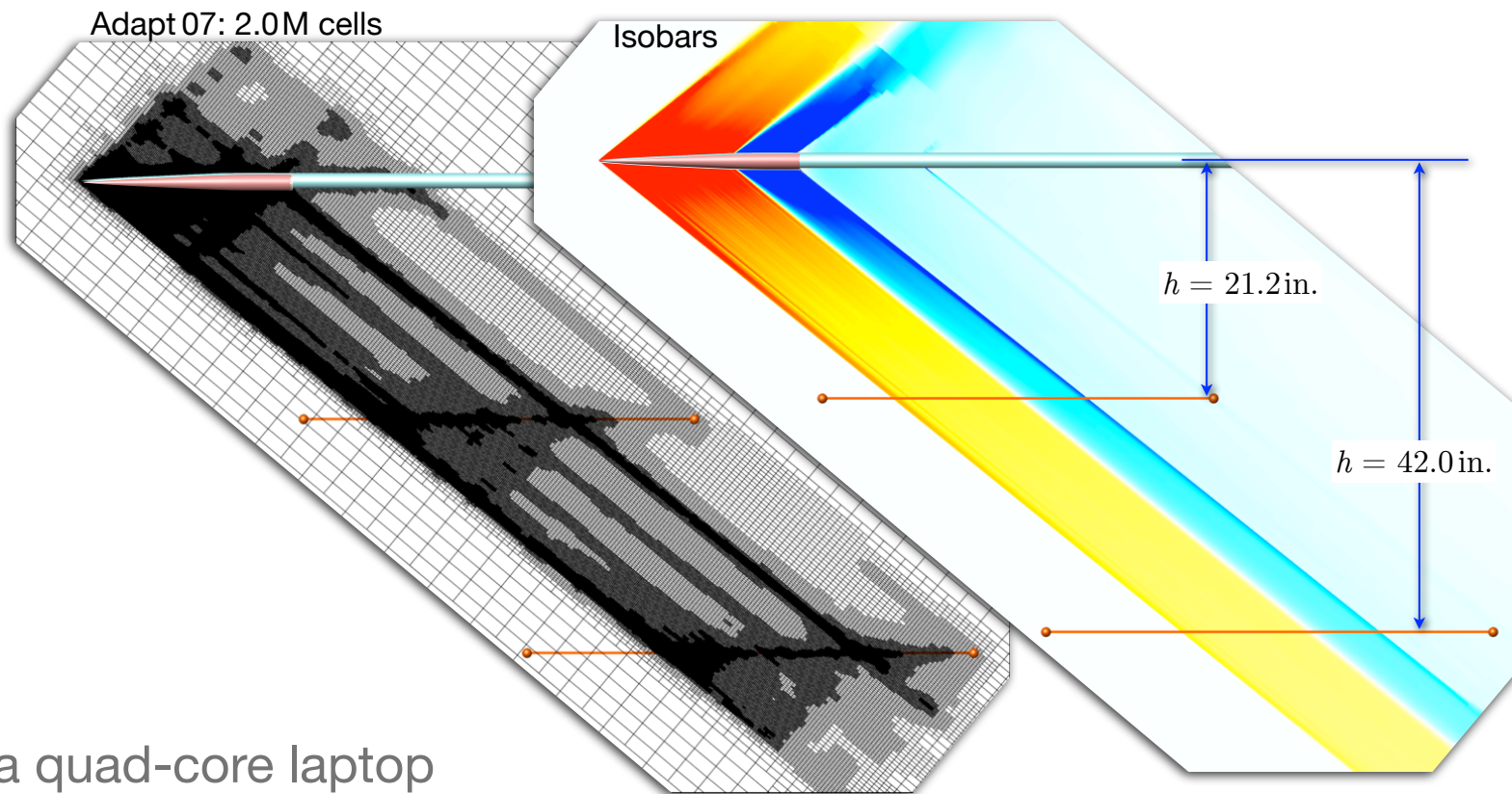
$M_\infty = 1.6$ ,  $\alpha = 0^\circ$ , On-track @  $h = 21.2$  in. & 42 in.





# Seeb-ALR: Computational Work

$M_\infty = 1.6$ ,  $\alpha = 0^\circ$ , On-track @  $h = 21.2$  in. & 42 in.

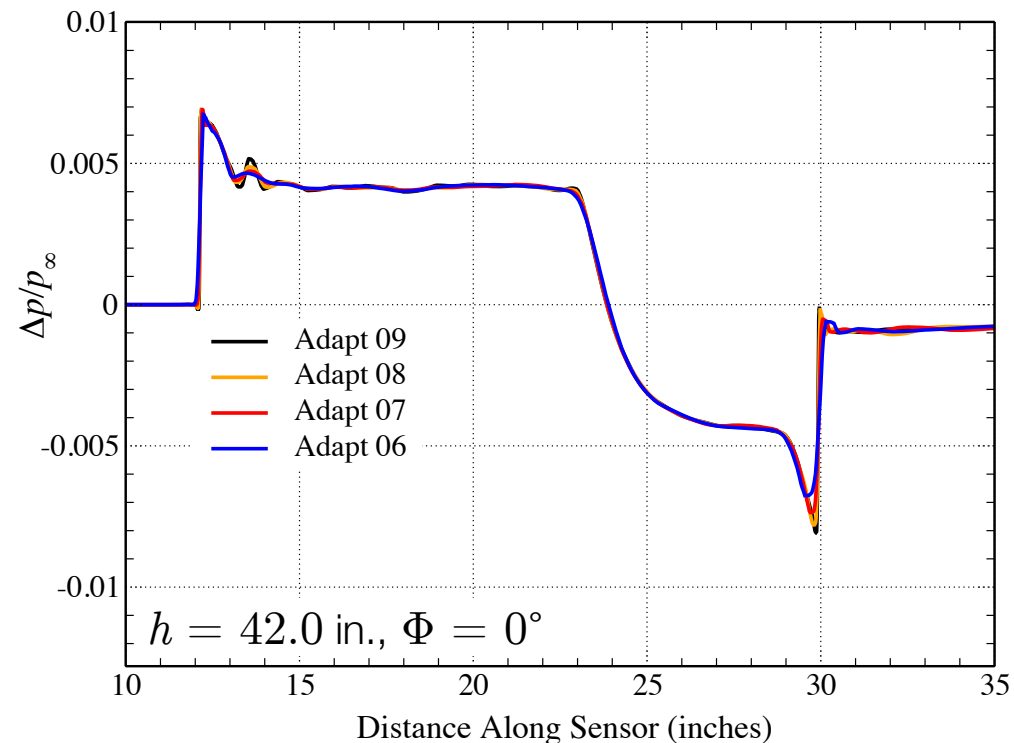
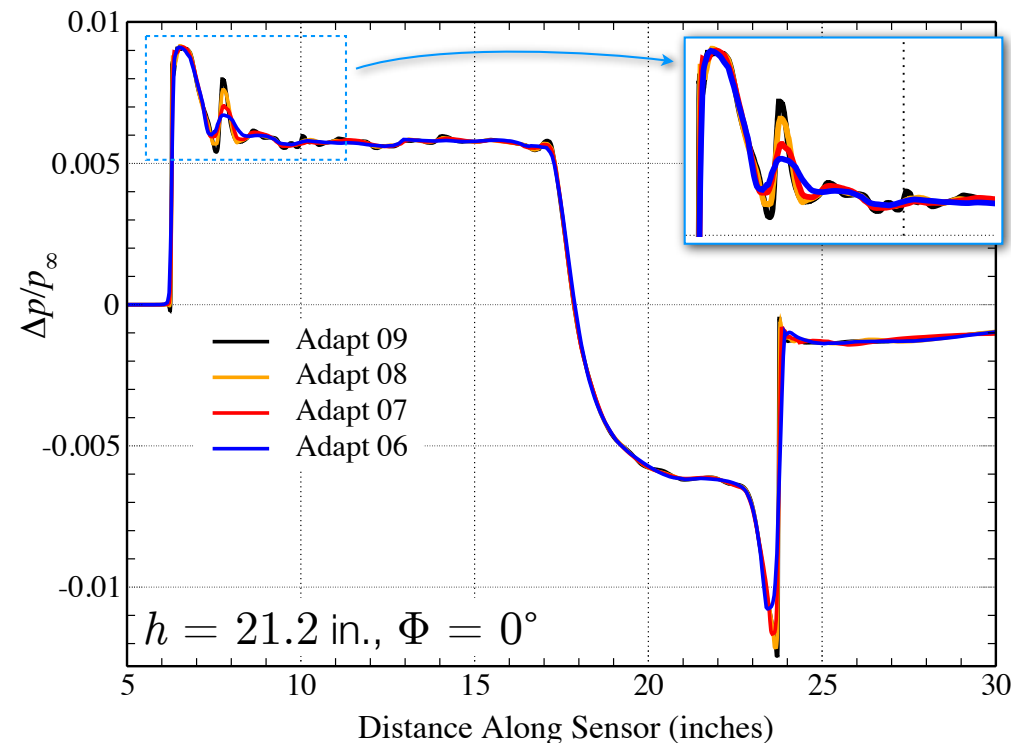


## Resources

- Run on 2011-era quad-core laptop
- ~1 hr runtime (61mins)
- 3.6 GB of memory (max)

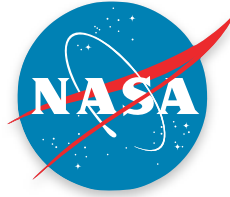
# Seeb-ALR: Mesh Convergence

Convergence of pressure signature,  $M_\infty = 1.6$ ,  $\alpha = 0^\circ$



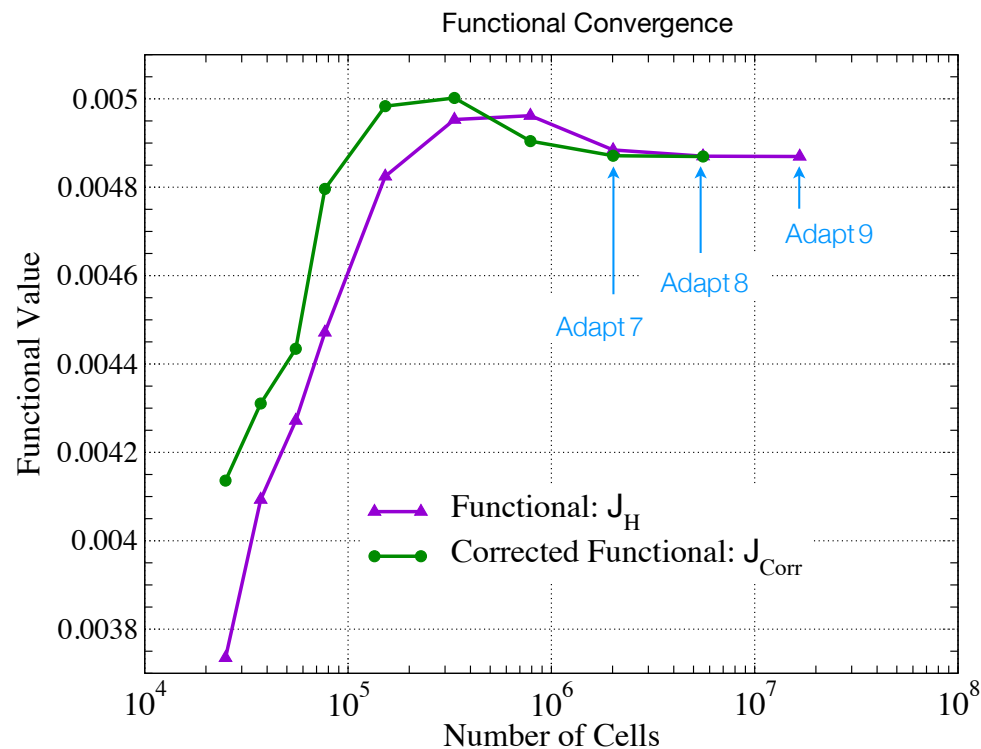
- Pressure signatures largely converged by 6th adapt cycle. - even at 42 in.
- Additional mesh resolution only sharpening shocks



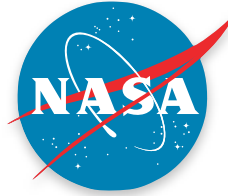


# Seeb-ALR: Mesh Convergence

- Results at 7<sup>th</sup> adaptation submitted to workshop
- Perform 2 more adaptations to assess degree of mesh convergence

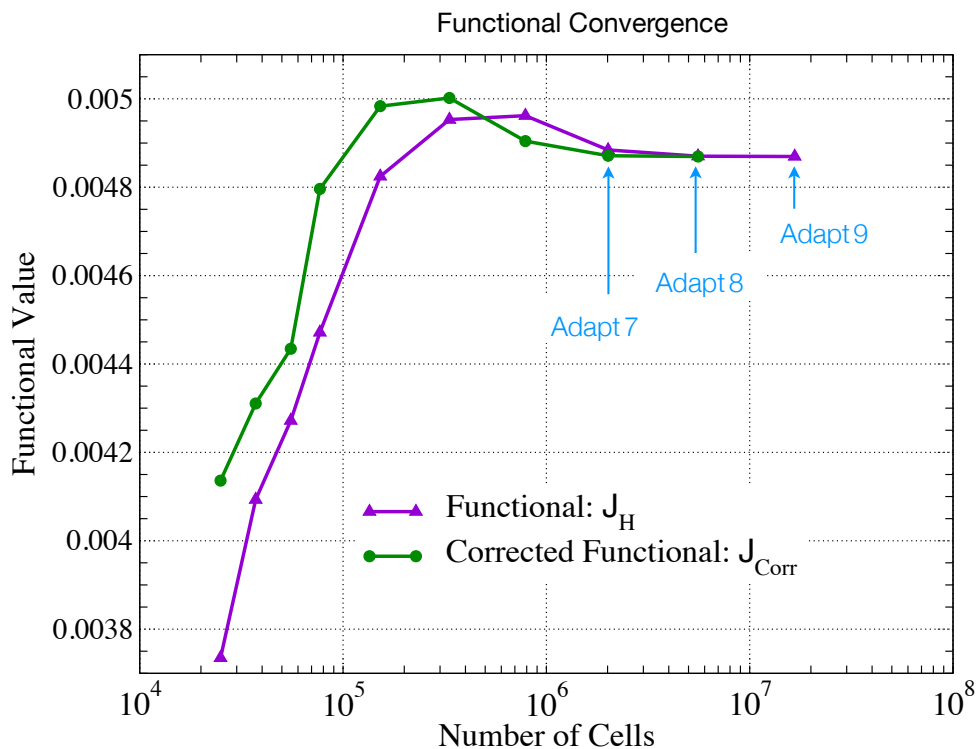


- Functional converges
- Correction *leads* functional
- Adjoint Correction vanishes

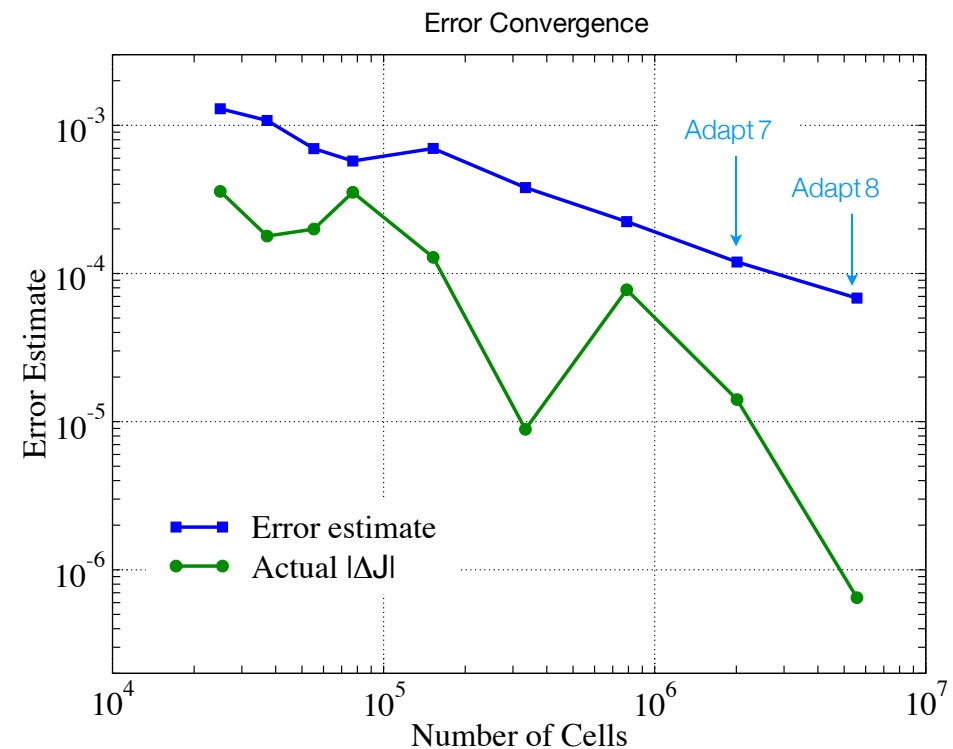


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- Perform 2 more adaptations to assess degree of mesh convergence



- Functional converges
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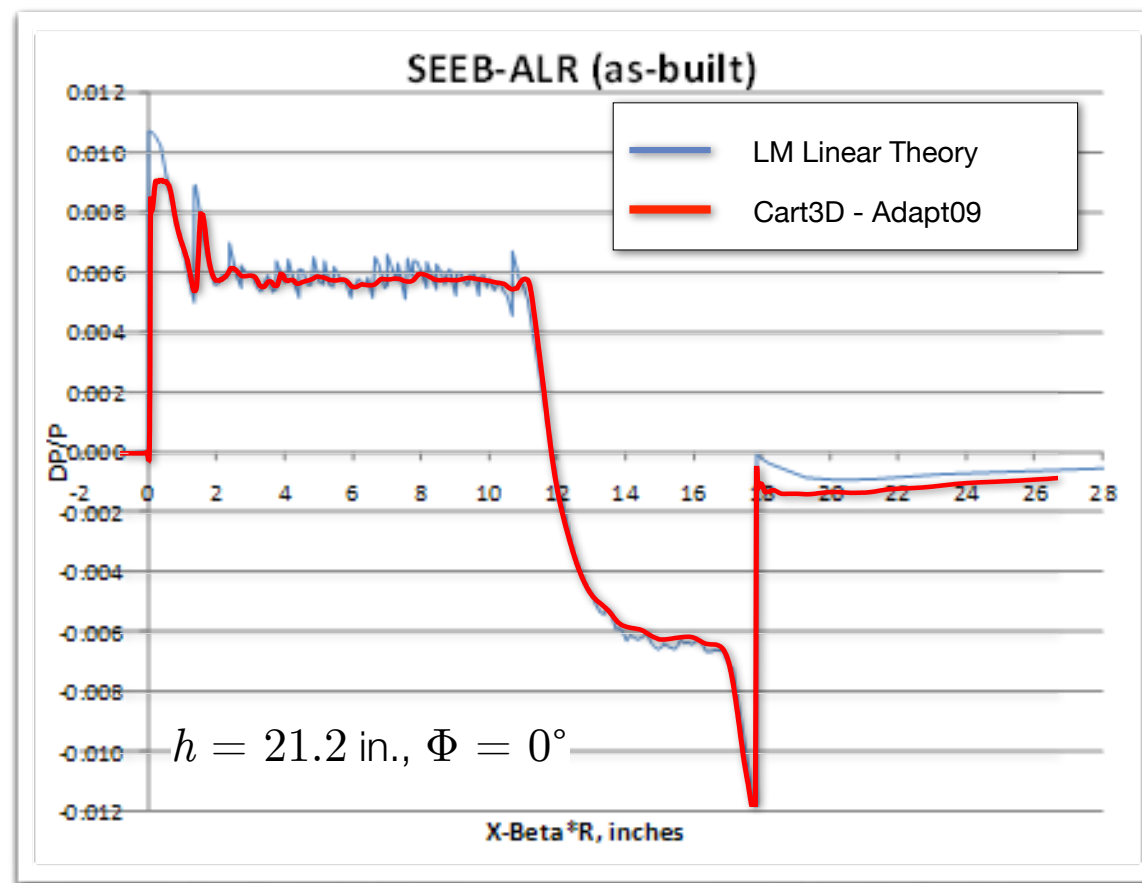


- Error-estimate bounds update  $|\Delta J|$
- Remaining error converges asymptotically
- “Textbook” convergence

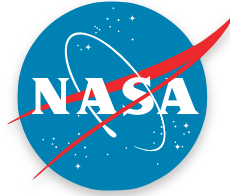
# Seeb-ALR: Data Comparison

Comparison with linear theory,  $M_\infty = 1.6$ ,  $\alpha = 0^\circ$

- Code-to-Code comparison used before exp. data was available



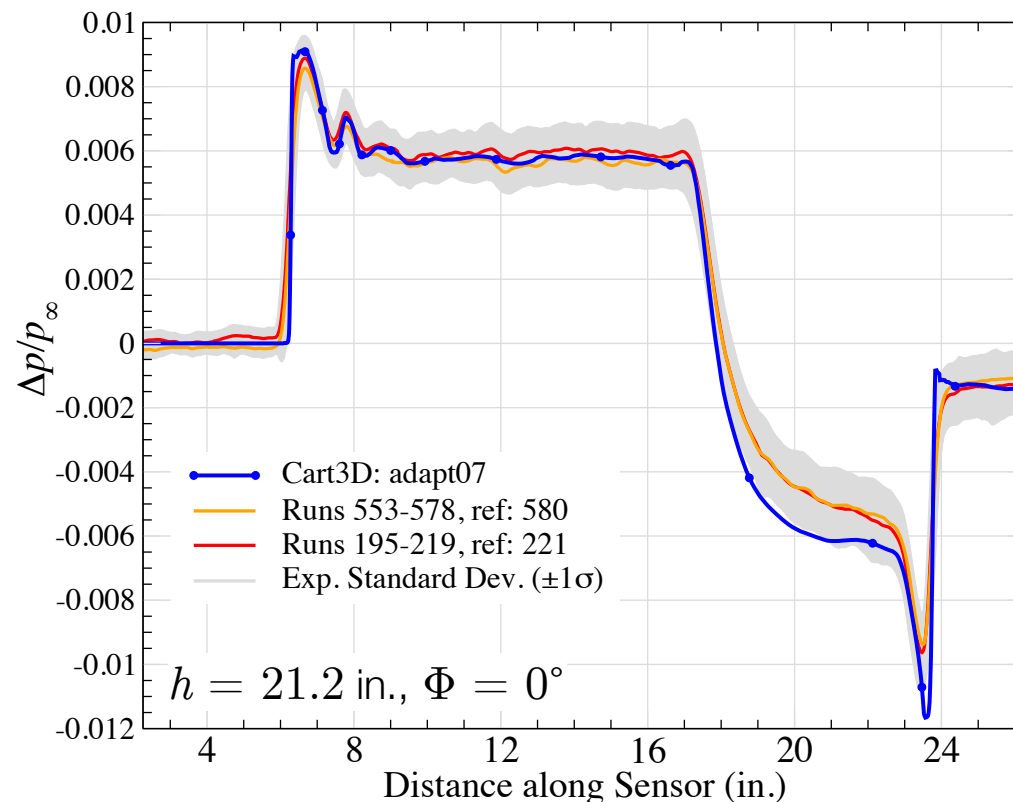




# Seeb-ALR: Data Comparison

Comparison with experimental data,  $M_\infty = 1.6$ ,  $\alpha = 0^\circ$

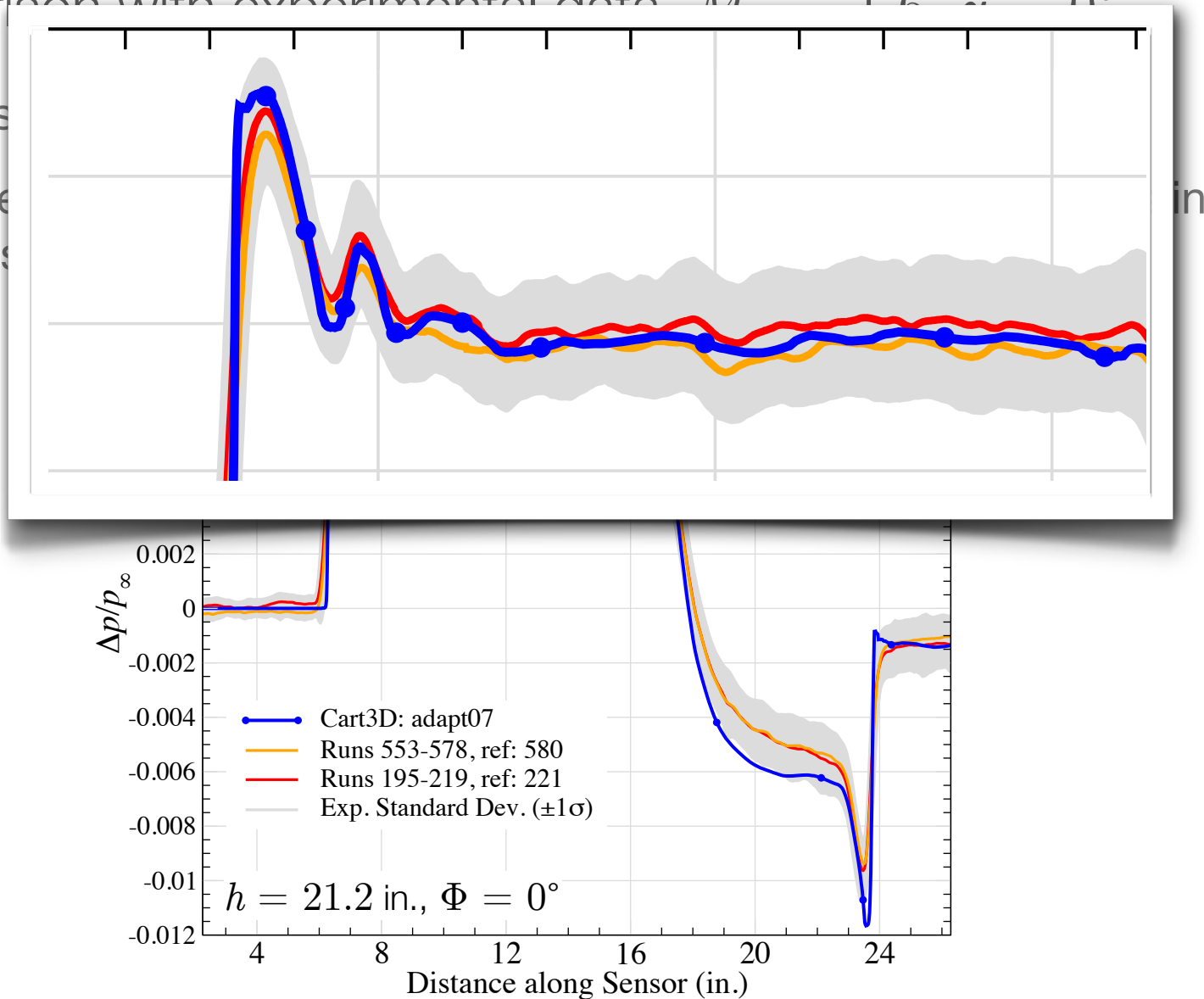
- Closest data at  $h \approx 20.6$  in.,  $\alpha = -0.3^\circ$ ,  $\beta = -0.3^\circ$
- Excellent agreement in peaks and on flat-top, some differences in expansion

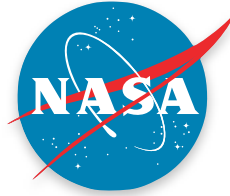


# Seeb-ALR: Data Comparison

Comparison with experimental data  $M = 1.6$ ,  $\alpha = 0^\circ$

- Closes
- Excellent expansion

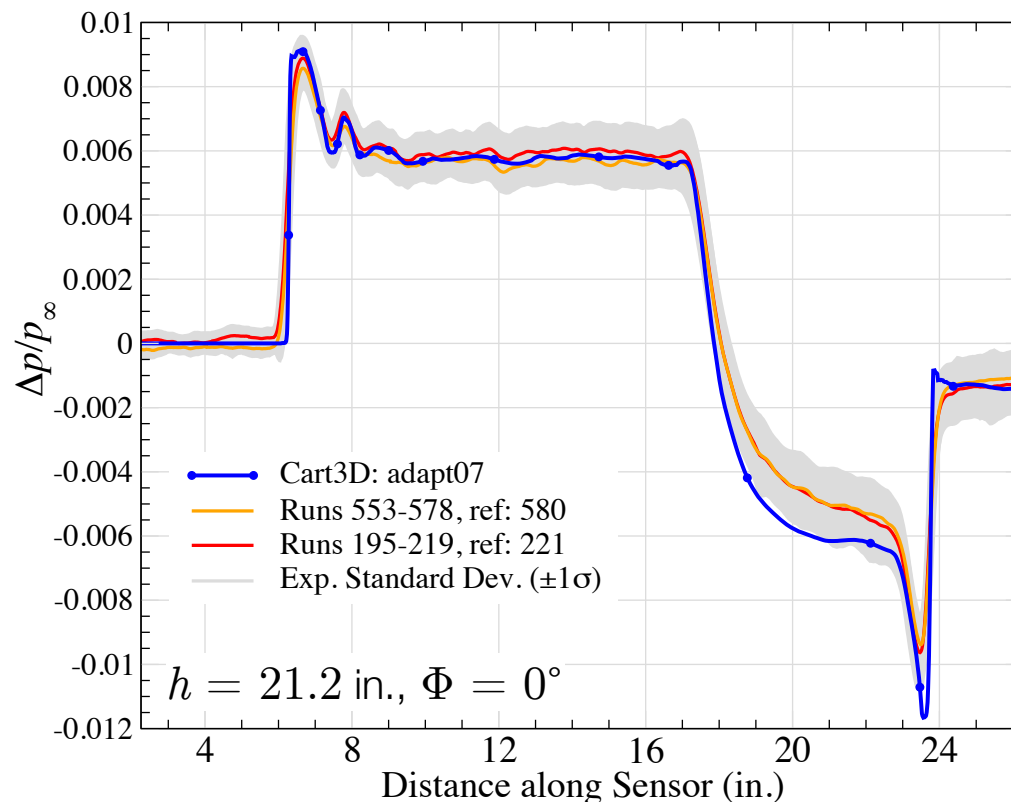


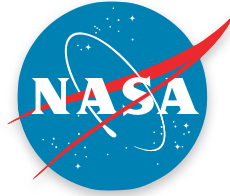


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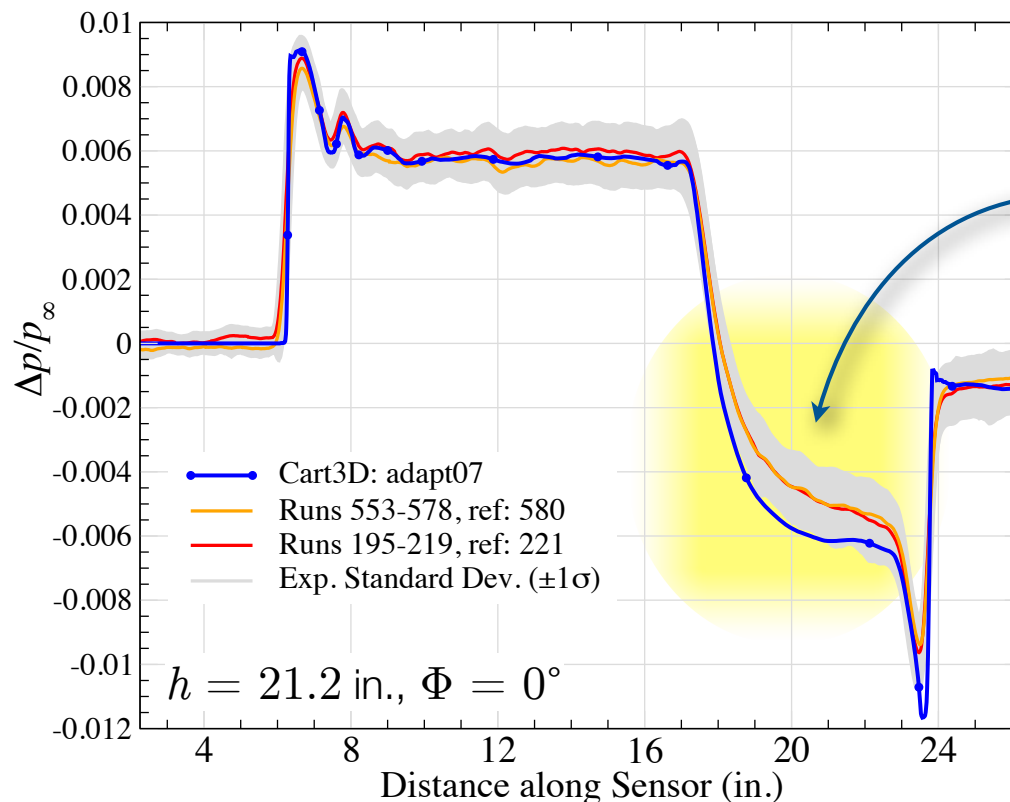




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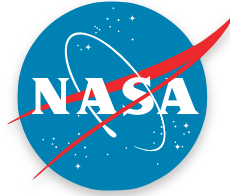
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Differences in expansion were troubling since we have high confidence in solution

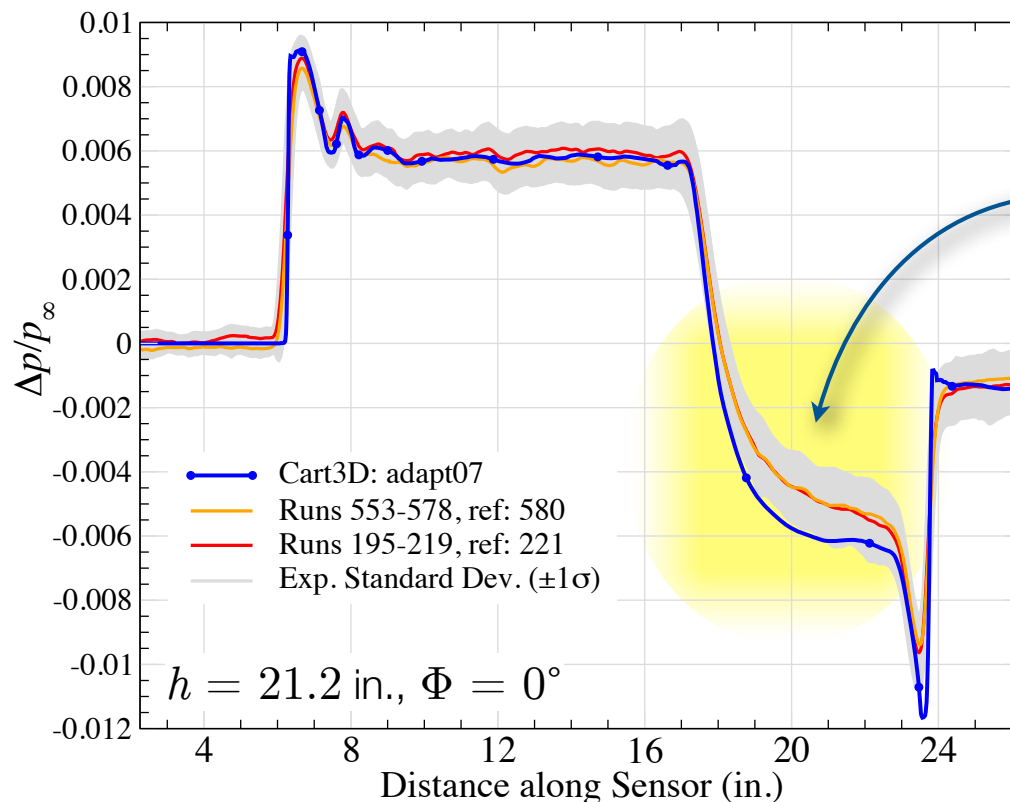




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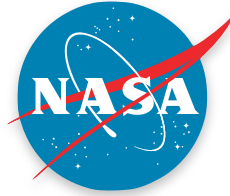
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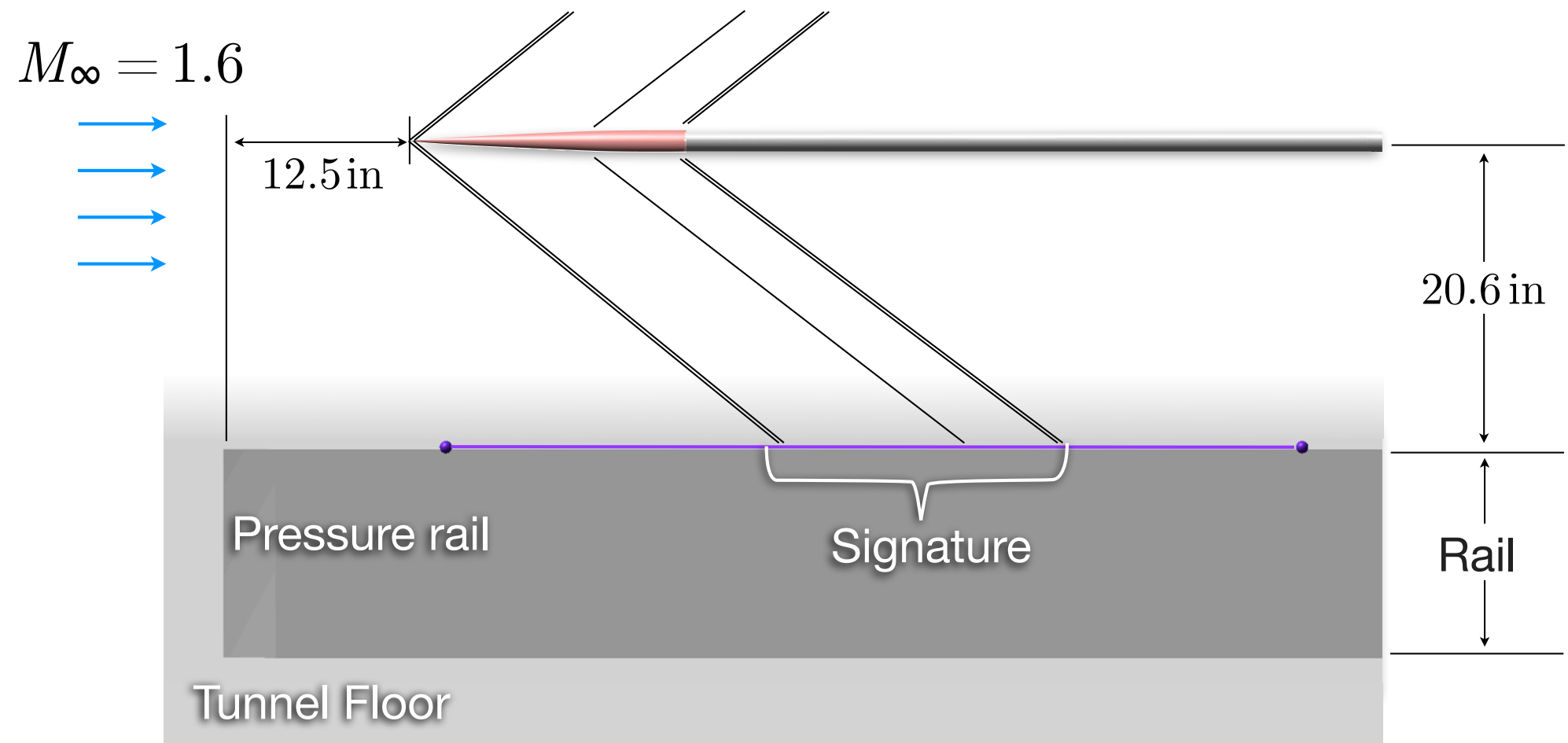
1. Re-measured model
2. Ran case with Seeb-ALR + pressure rail + tunnel wall



# Seeb-ALR: Data Comparison

Simulation with Seeb-ALR + pressure rail + tunnel floor

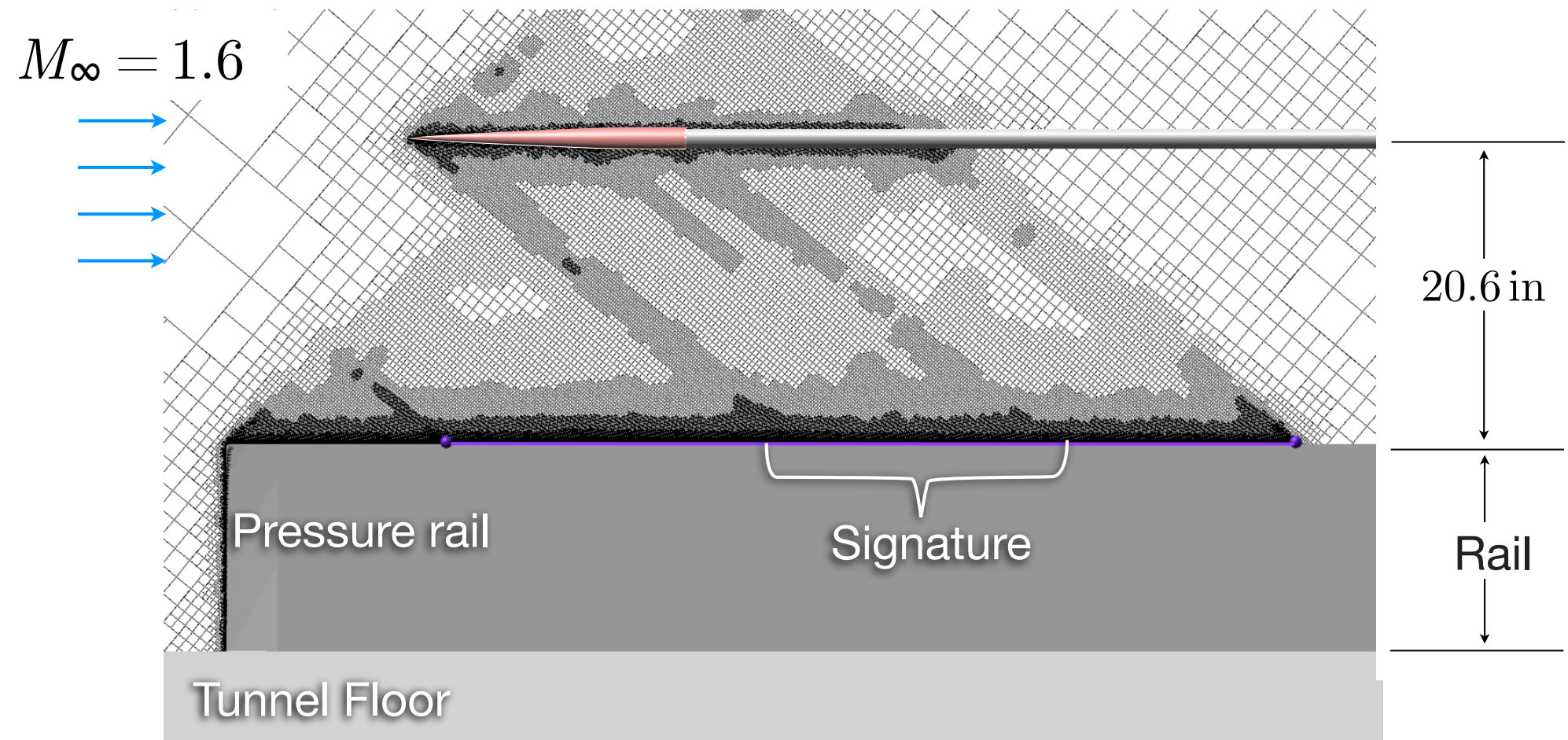
Mid-traverse location for data @  $h = 20.6$  in.



# Seeb-ALR: Data Comparison

Simulation with Seeb-ALR + pressure rail + tunnel floor

Mid-traverse location for data @  $h = 20.6$  in.

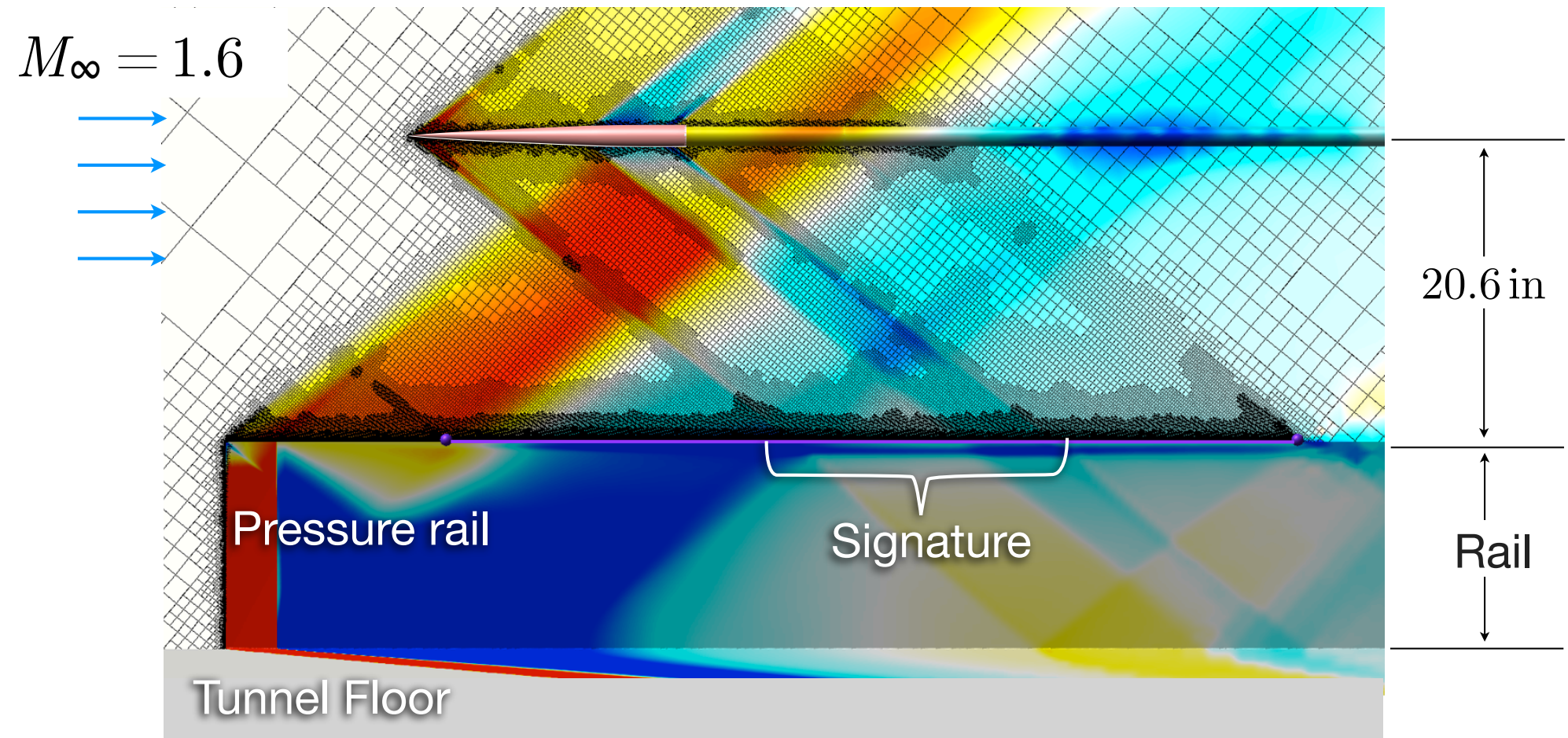




# Seeb-ALR: Data Comparison

Simulation with Seeb-ALR + pressure rail + tunnel floor

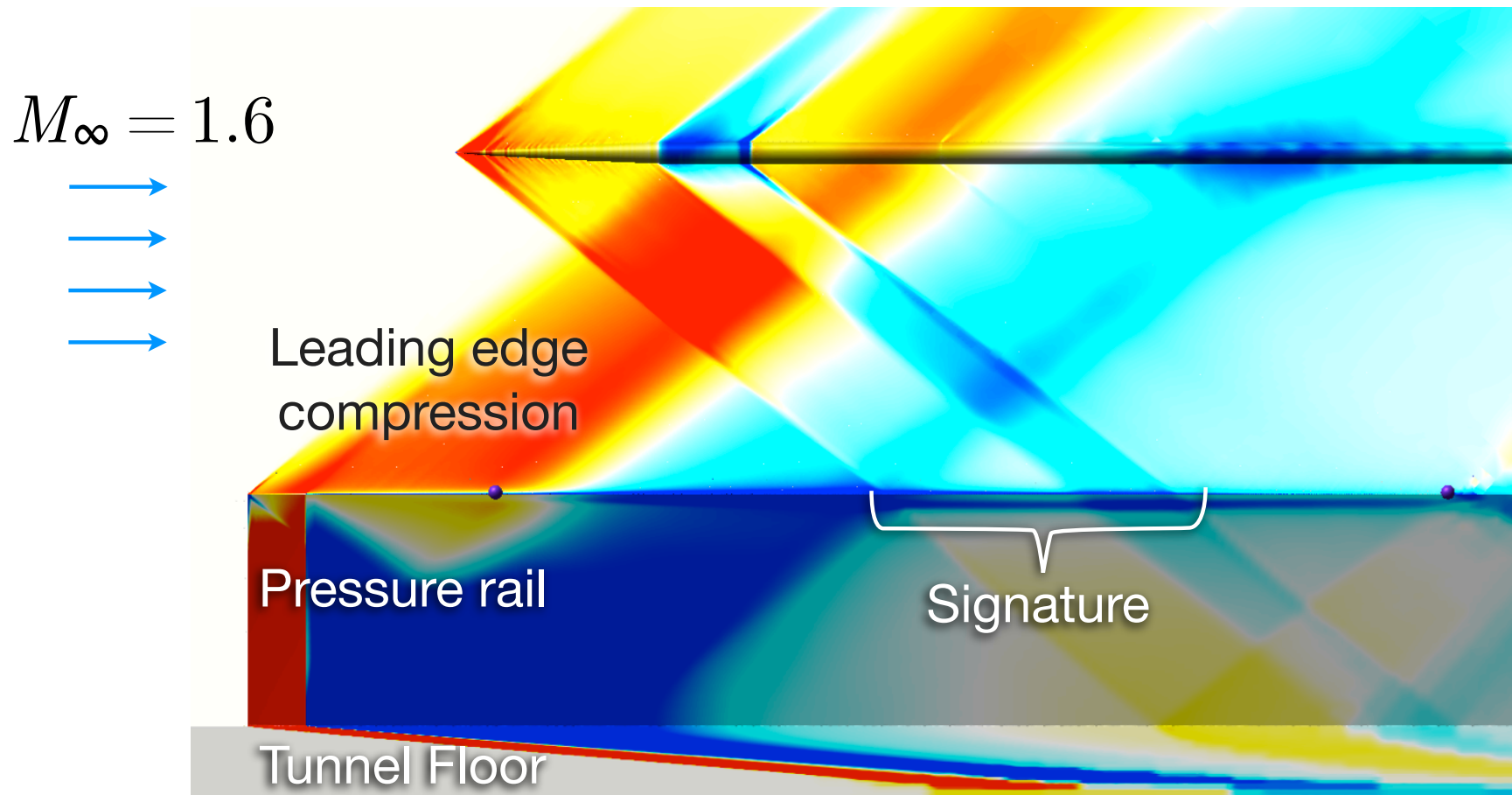
Mid-traverse location for data @  $h = 20.6$  in.



# Seeb-ALR: Data Comparison

Simulation with Seeb-ALR + pressure rail + tunnel floor

Mid-traverse location for data @  $h = 20.6$  in.



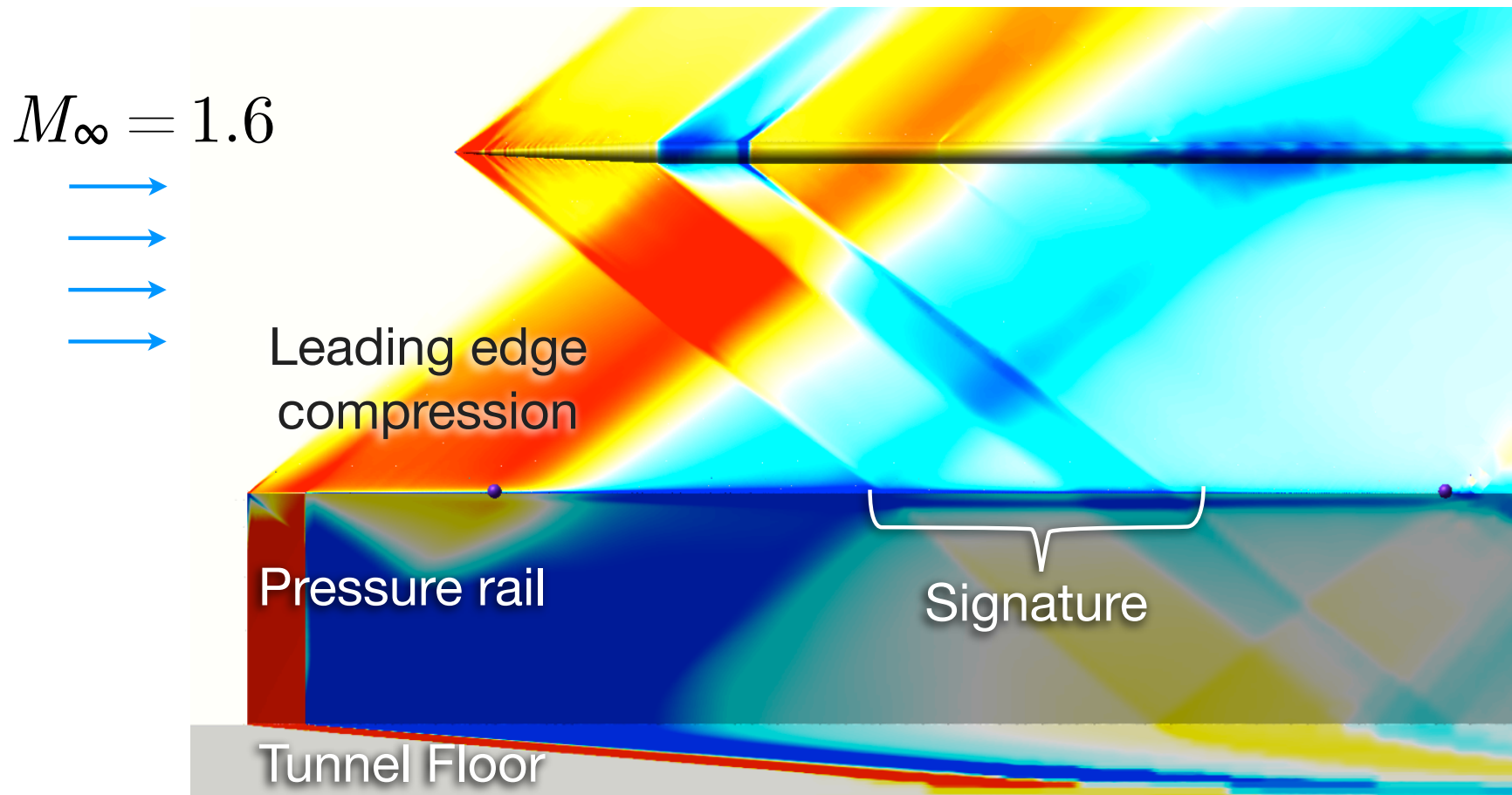
- Model positioned in middle of range of experimental traverse
- Leading edge compression interacts with model, relieving suction



# Seeb-ALR: Data Comparison

Simulation with Seeb-ALR + pressure rail + tunnel floor

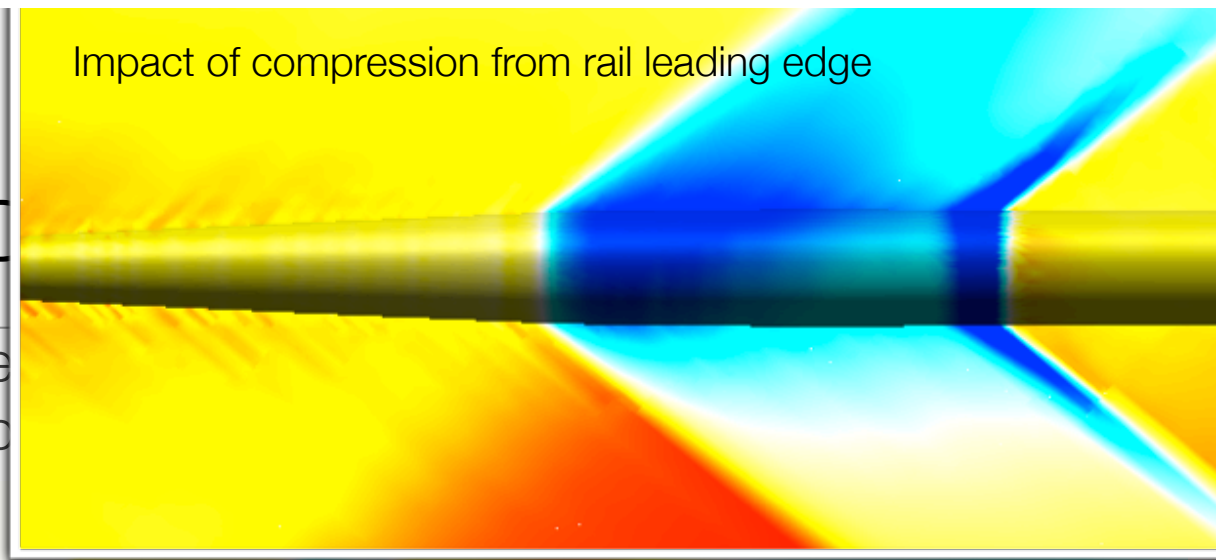
Mid-traverse location for data @  $h = 20.6$  in.



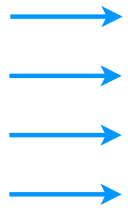
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# Seeb-ALR: D

Simulation with Seeb  
Mid-traverse location



$$M_{\infty} = 1.6$$



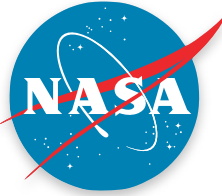
Leading edge  
compression

Pressure rail

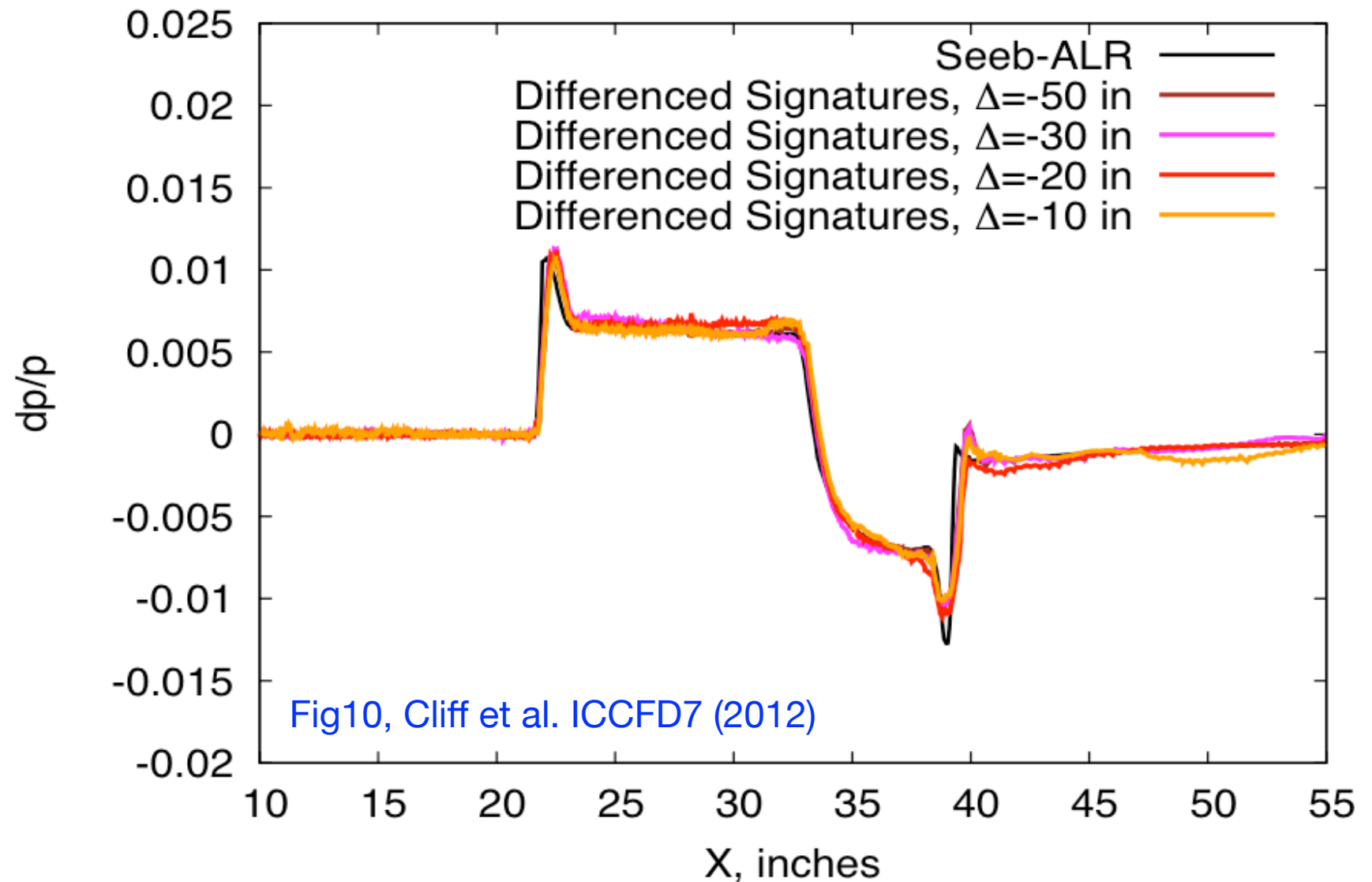
Signature

Tunnel Floor

- Model positioned in middle of range of experimental traverse
- Leading edge compression interacts with model, relieving suction



# Seeb-ALR: Data Comparison





Seeb-

n

$dn/n$

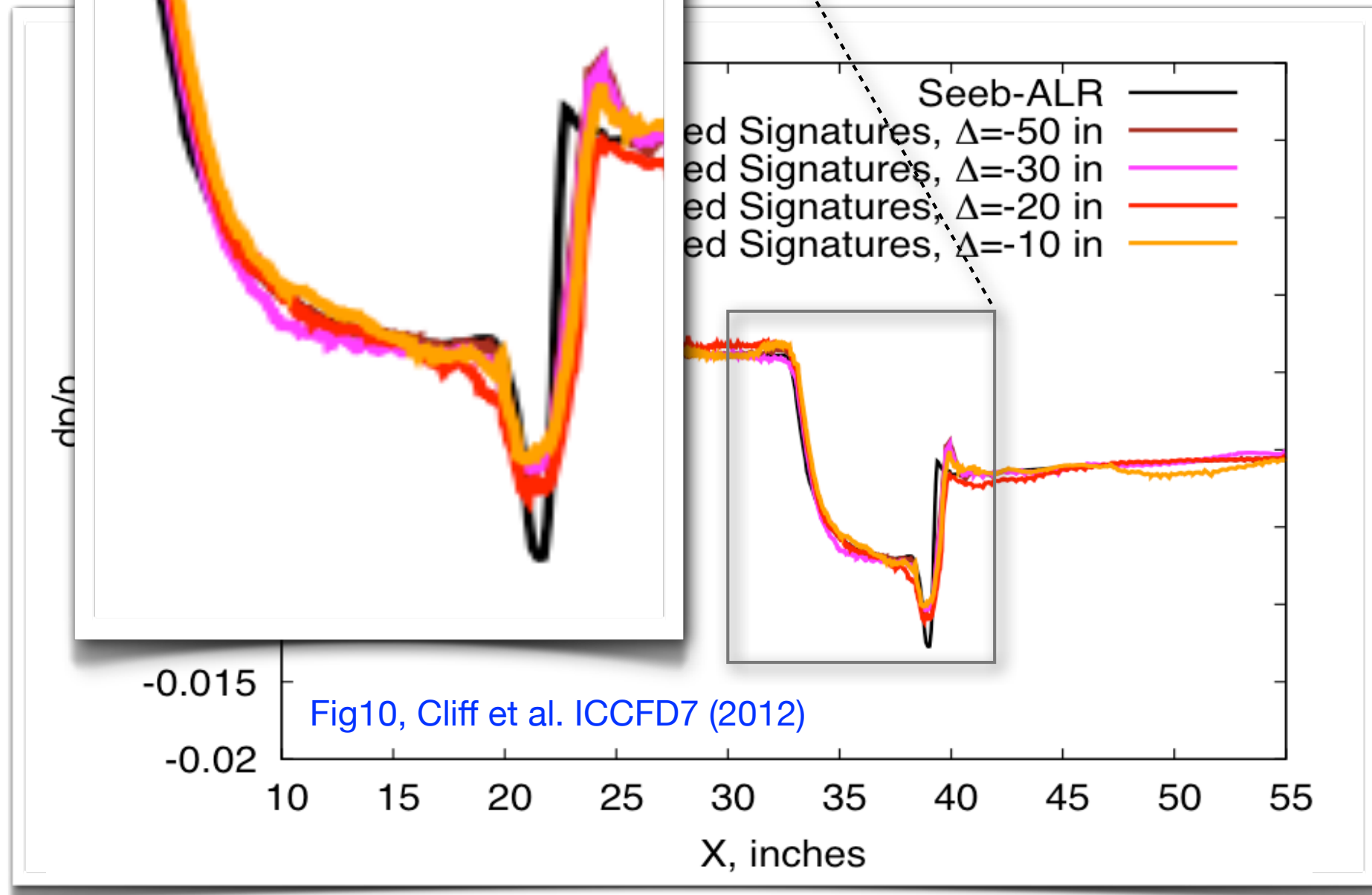
-0.015  
-0.02

Fig10, Cliff et al. ICCFD7 (2012)

10 15 20 25 30 35 40 45 50 55

X, inches

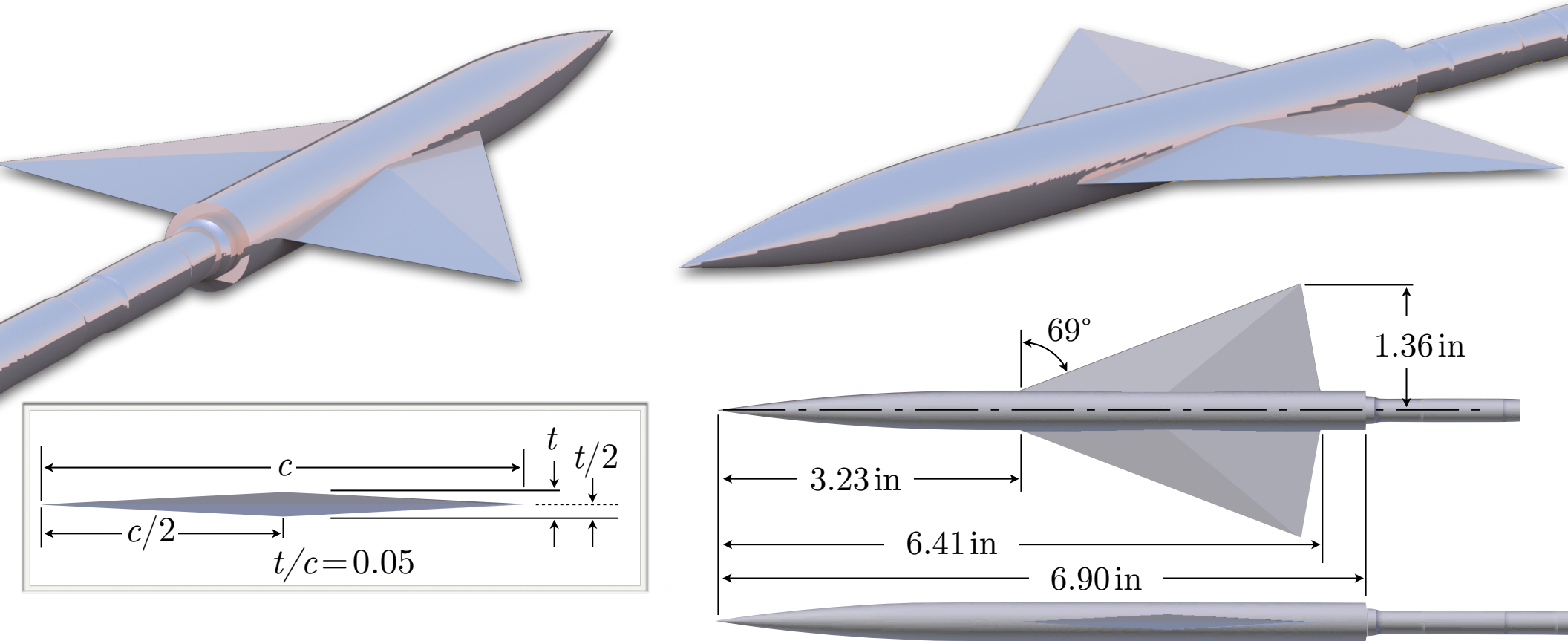
Seeb-ALR  
ed Signatures,  $\Delta=-50$  in  
ed Signatures,  $\Delta=-30$  in  
ed Signatures,  $\Delta=-20$  in  
ed Signatures,  $\Delta=-10$  in





# 69° Delta Wing Body

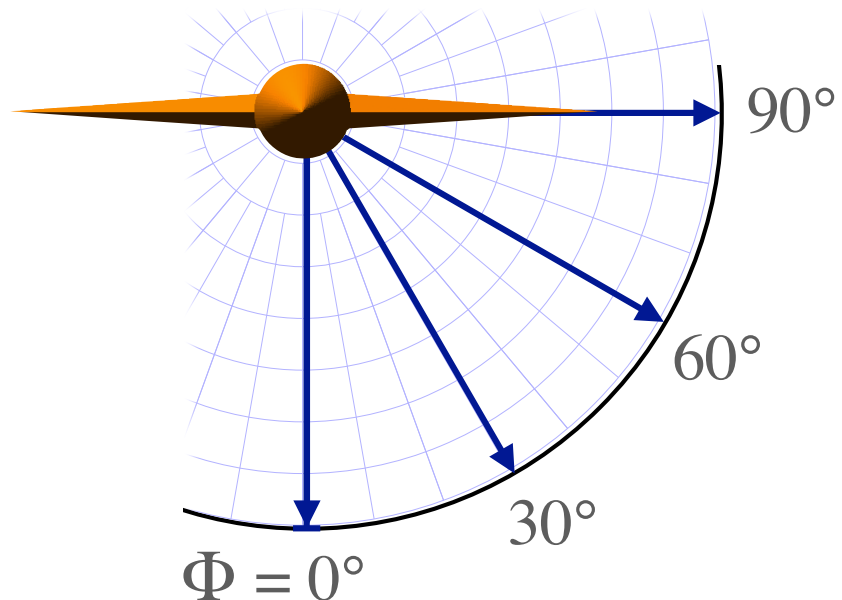
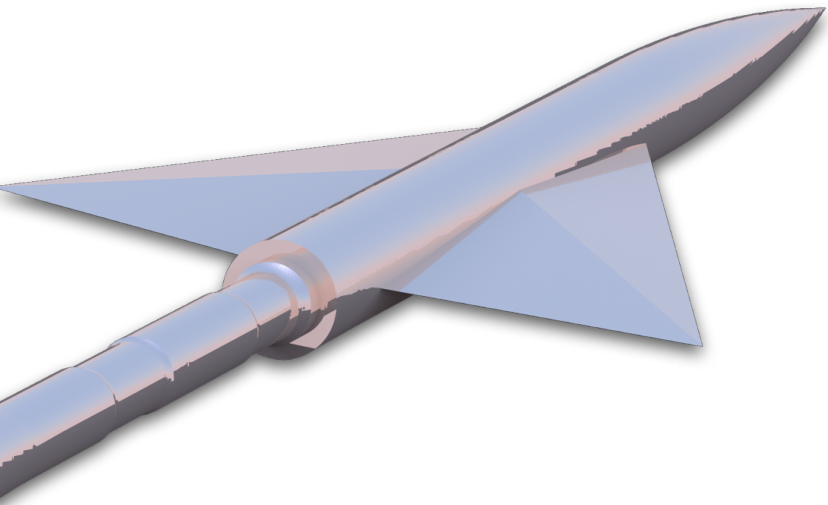
$$M_{\infty} = 1.7, \alpha = 0^{\circ}$$



- Tangent-ogive-cylinder fuselage
- Delta wing with 5% thick diamond airfoil
- New sting fitted to original (1973) model from Hunton et al.

# 69° Delta Wing Body

$$M_{\infty} = 1.7, \alpha = 0^{\circ}$$



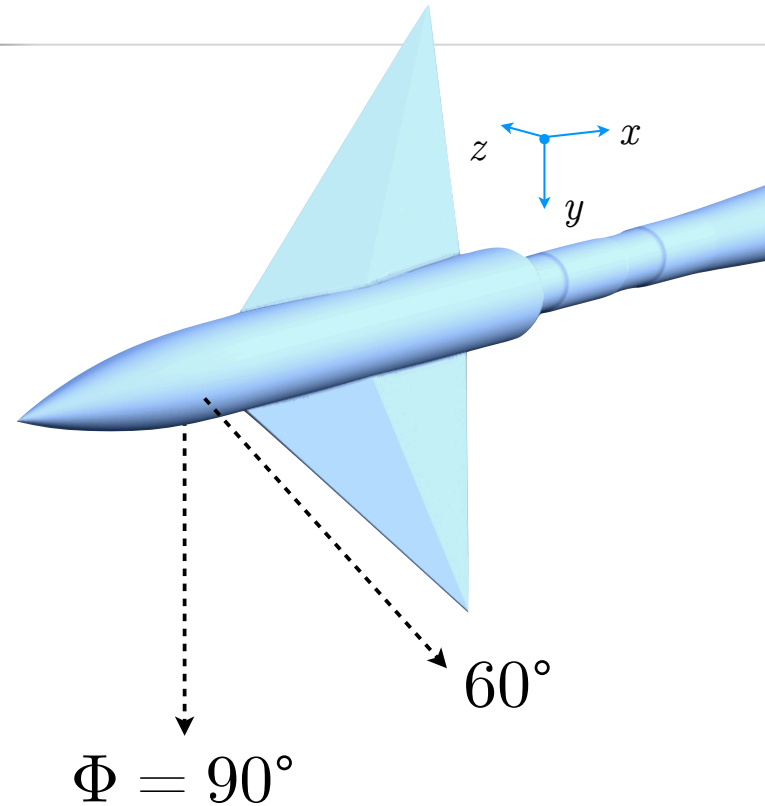
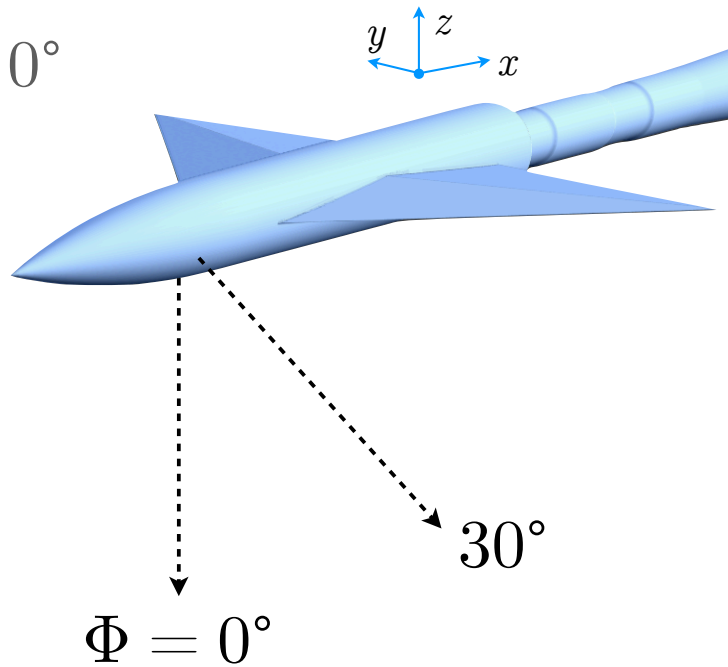
## Required Pressure Signatures

- $\Phi = \{0^{\circ}, 30^{\circ}, 60^{\circ}, 90^{\circ}\}$
- $h = \{0.5, 21.2, 24.8, 31.8\}$  in.
- 10 sensors and extreme off-track angles

# 69° Delta Wing Body

$$M_{\infty} = 1.7$$

$$\alpha = 0^{\circ}$$



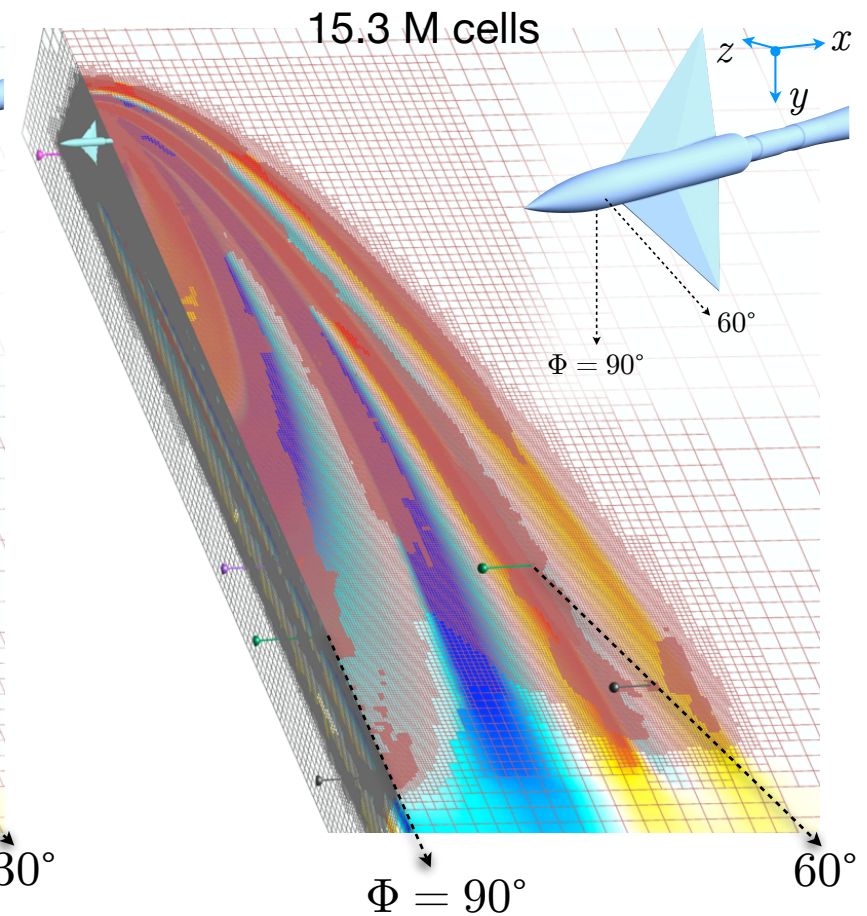
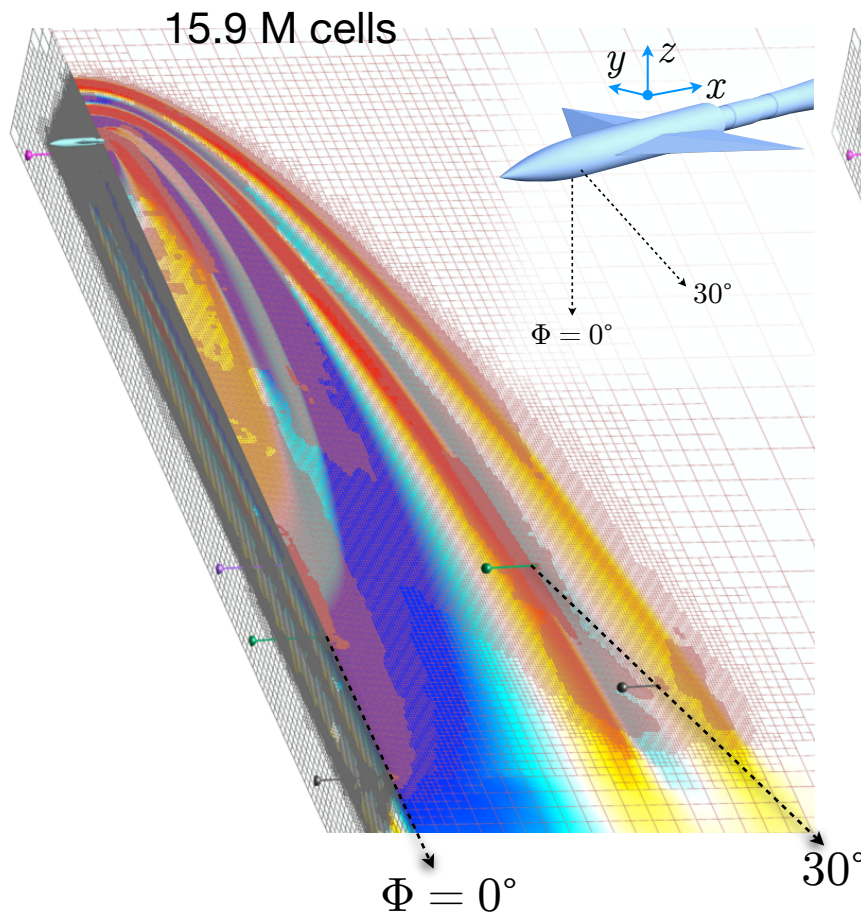
## Setup as 2 cases

1.  $\Phi = \{0^{\circ}, 30^{\circ}\}$  – Mesh rotated in pitch plane
2.  $\Phi = \{60^{\circ}, 90^{\circ}\}$  – Mesh rotated in yaw plane

# Case 2 – 69° Delta Wing Body

$$M_{\infty} = 1.7$$

$$\alpha = 0^{\circ}$$



Setup as 2 cases

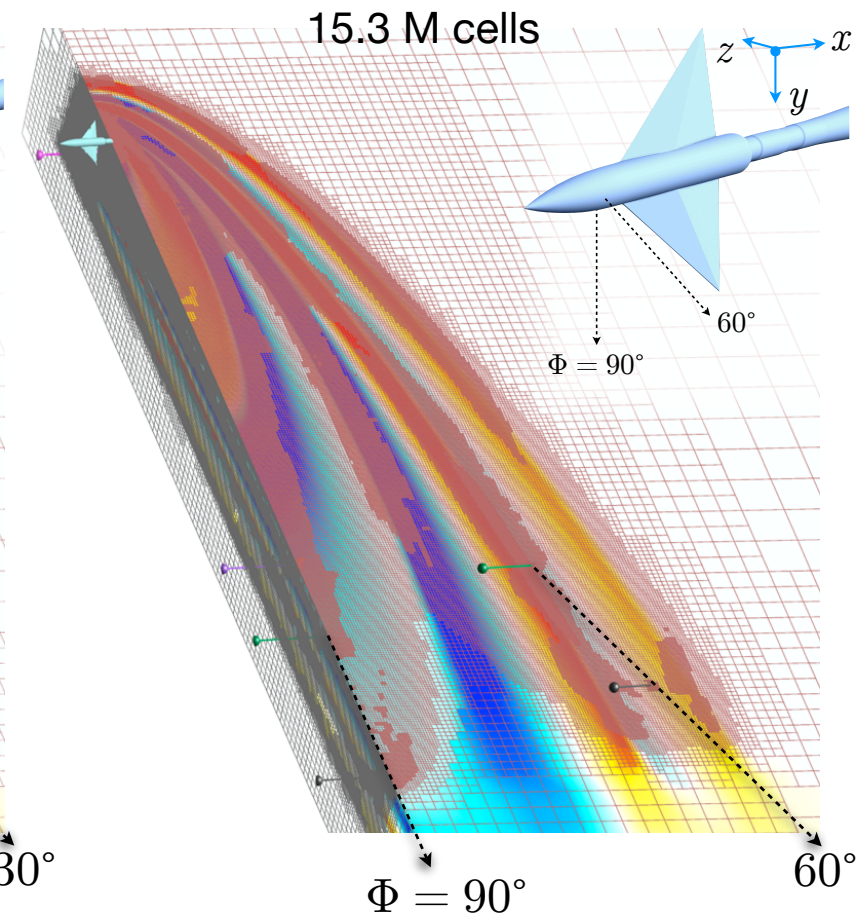
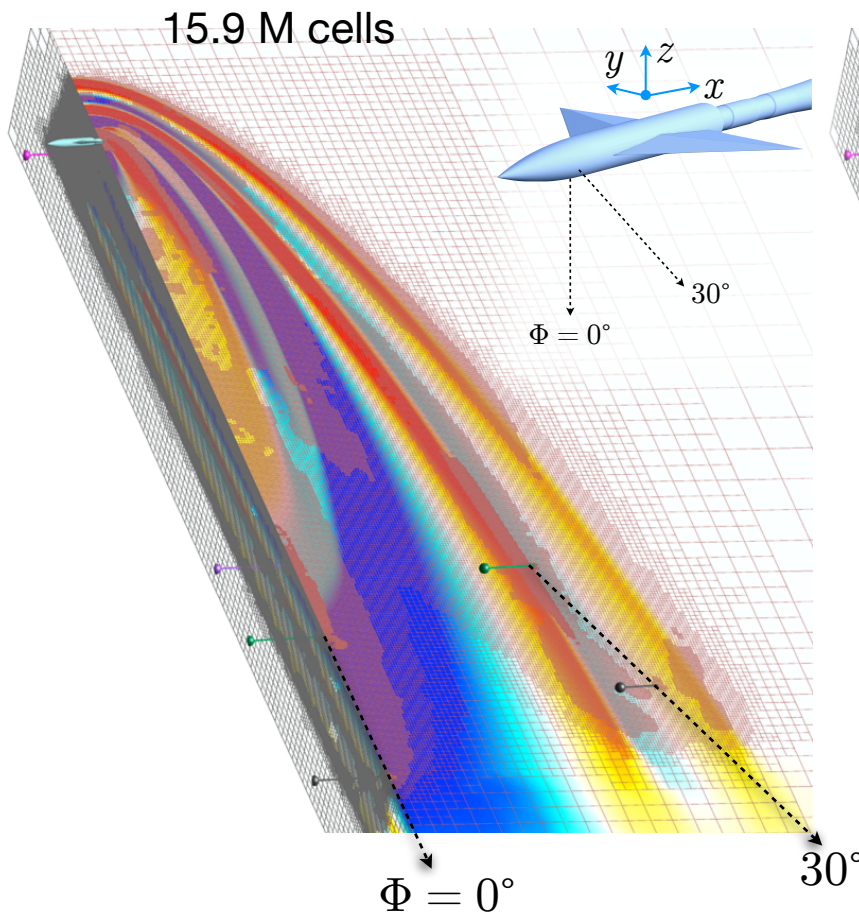
1.  $\Phi = \{0^{\circ}, 30^{\circ}\}$  – Mesh rotated in pitch plane
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## Case 2 – 69° Delta Wing Body

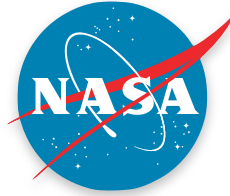
$$M_{\infty} = 1.7$$

$$\alpha = 0^{\circ}$$



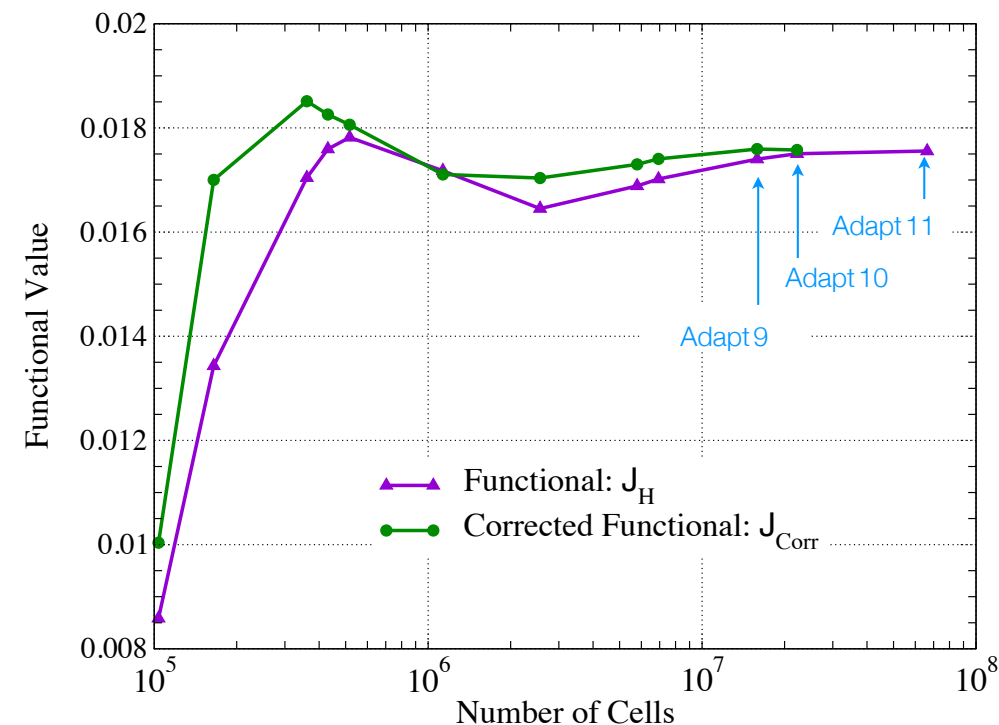
### Resources

- Run on dual socket system w/ 20 cores
- (1 hr runtime) x 2
- 36 GB of memory (max)

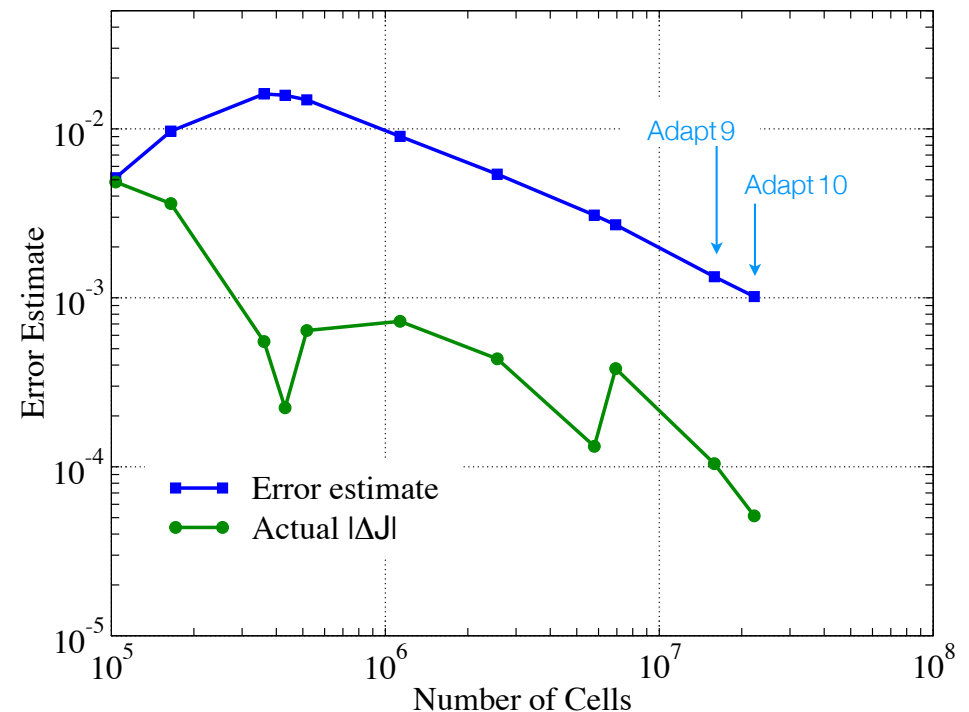


# 69° Delta Wing Body: Mesh Convergence

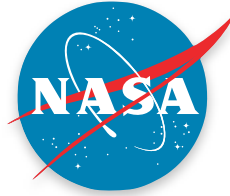
- Results at 9<sup>th</sup> adaptation submitted to workshop
- Perform 2 more adaptations to assess degree of mesh convergence



- Functional converges
- Correction *leads* functional
- Adjoint Correction vanishes

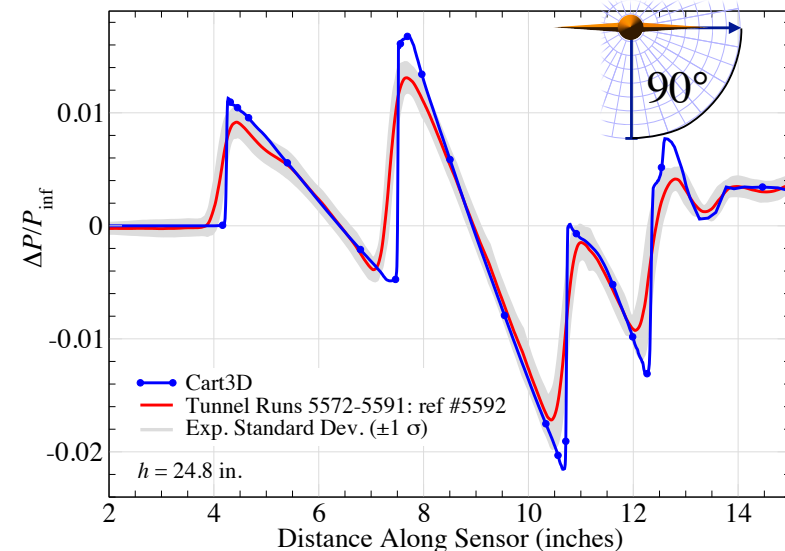
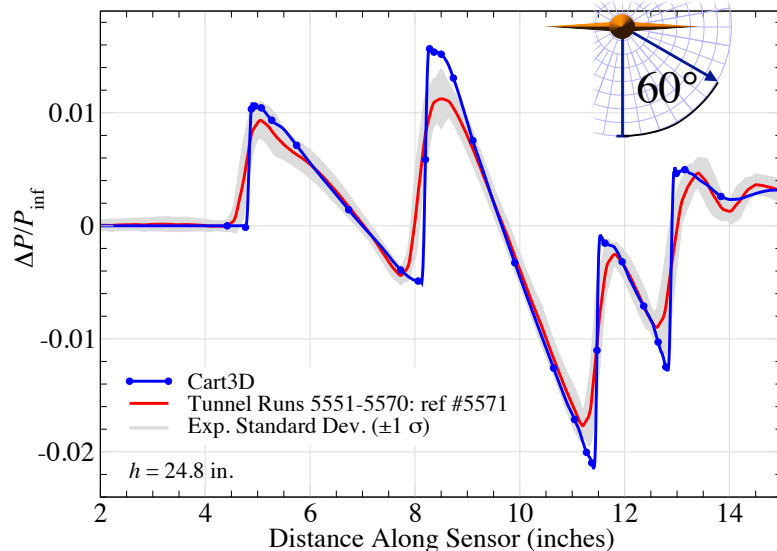
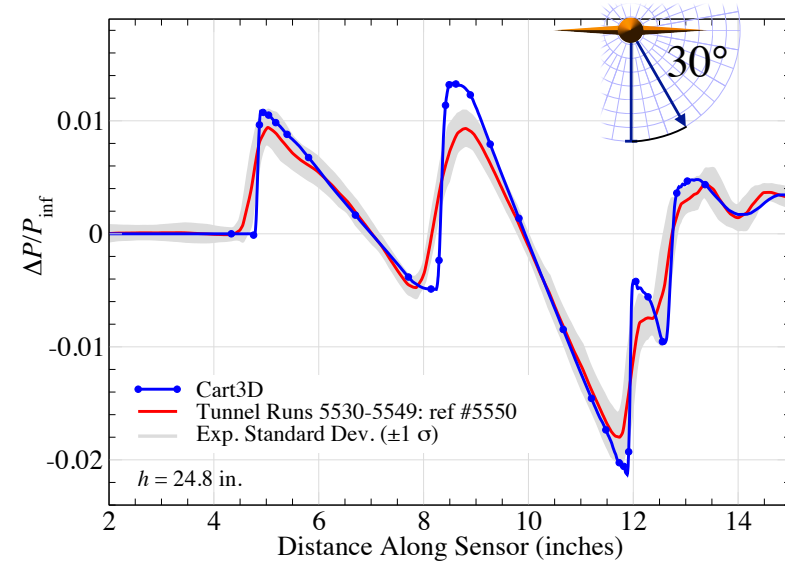
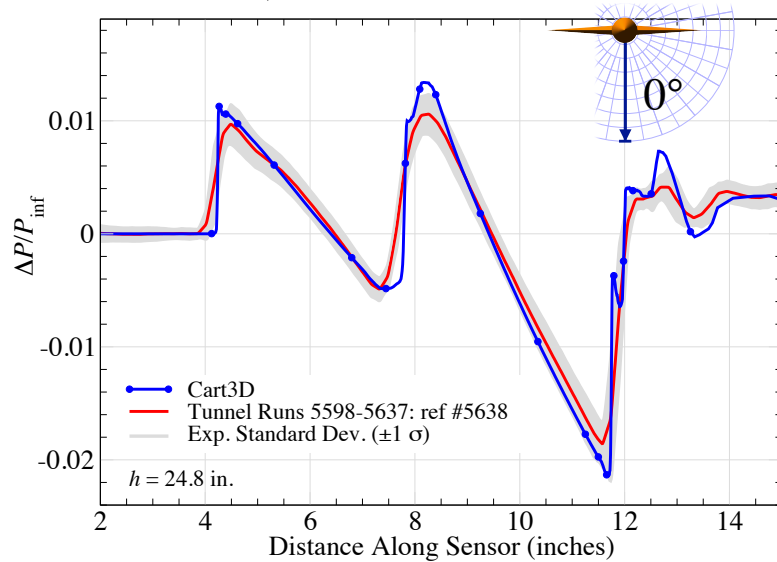


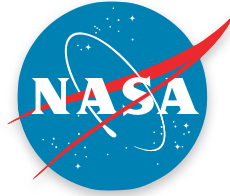
- Error-estimate bounds update  $|\Delta J|$
- Remaining error converges asymptotically
- Very good convergence



# 69° Delta Wing Body: Signatures @ 24.8 in

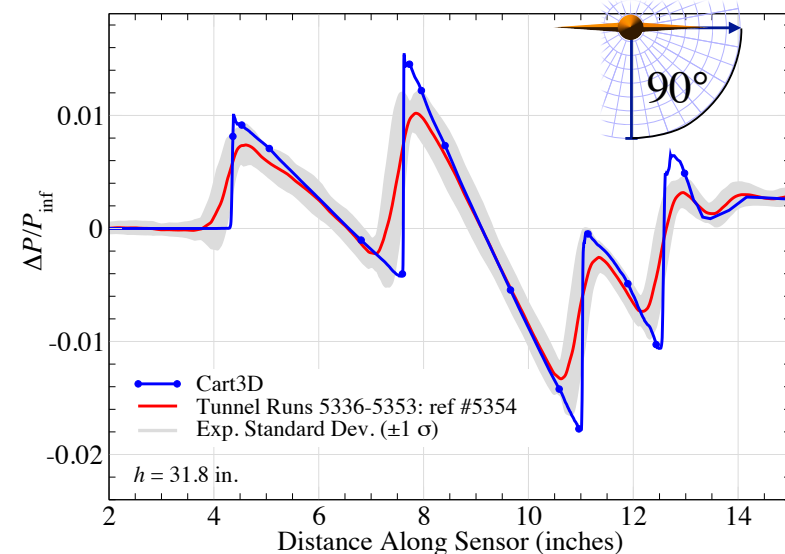
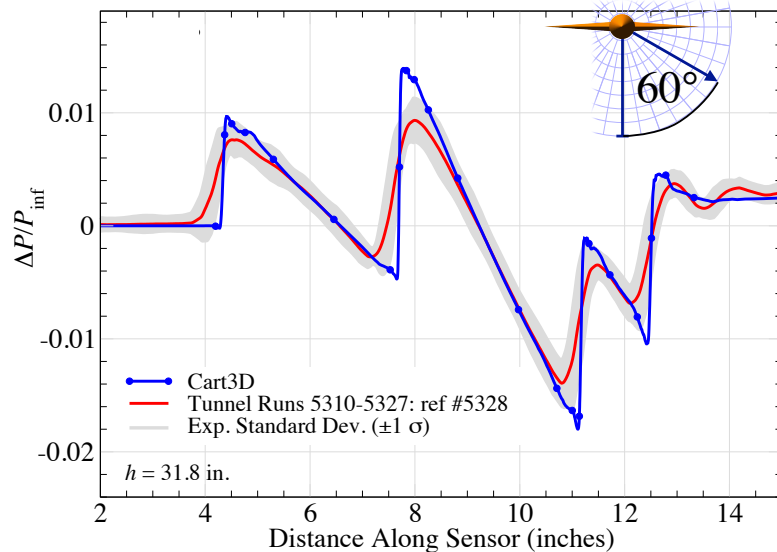
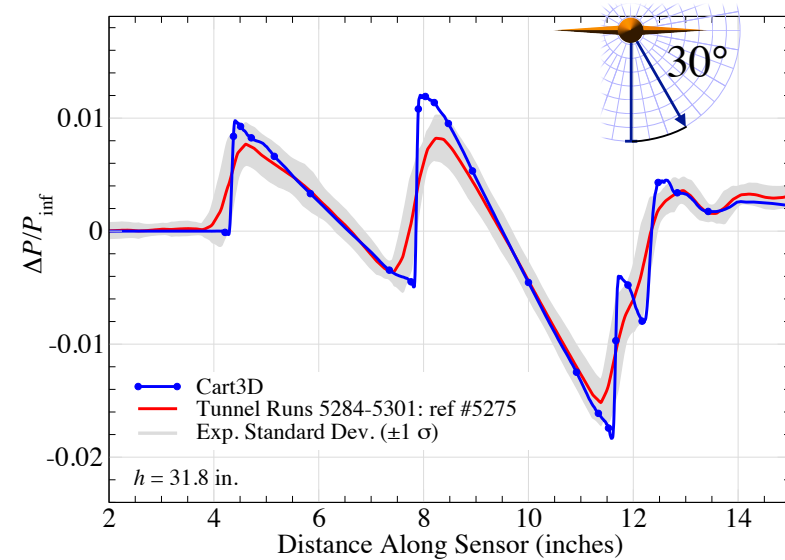
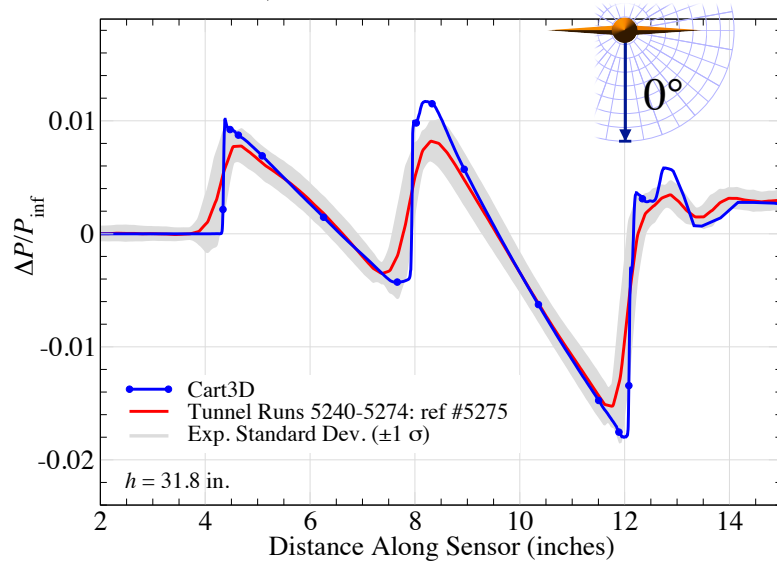
$$M_\infty = 1.7, \alpha = 0^\circ$$



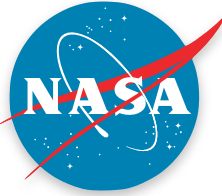


# 69° Delta Wing Body: Signatures @ 31.8 in

$$M_\infty = 1.7, \alpha = 0^\circ$$







# Lockheed Martin LM 1021

$$M_{\infty} = 1.6, \alpha = 2.1^{\circ}$$

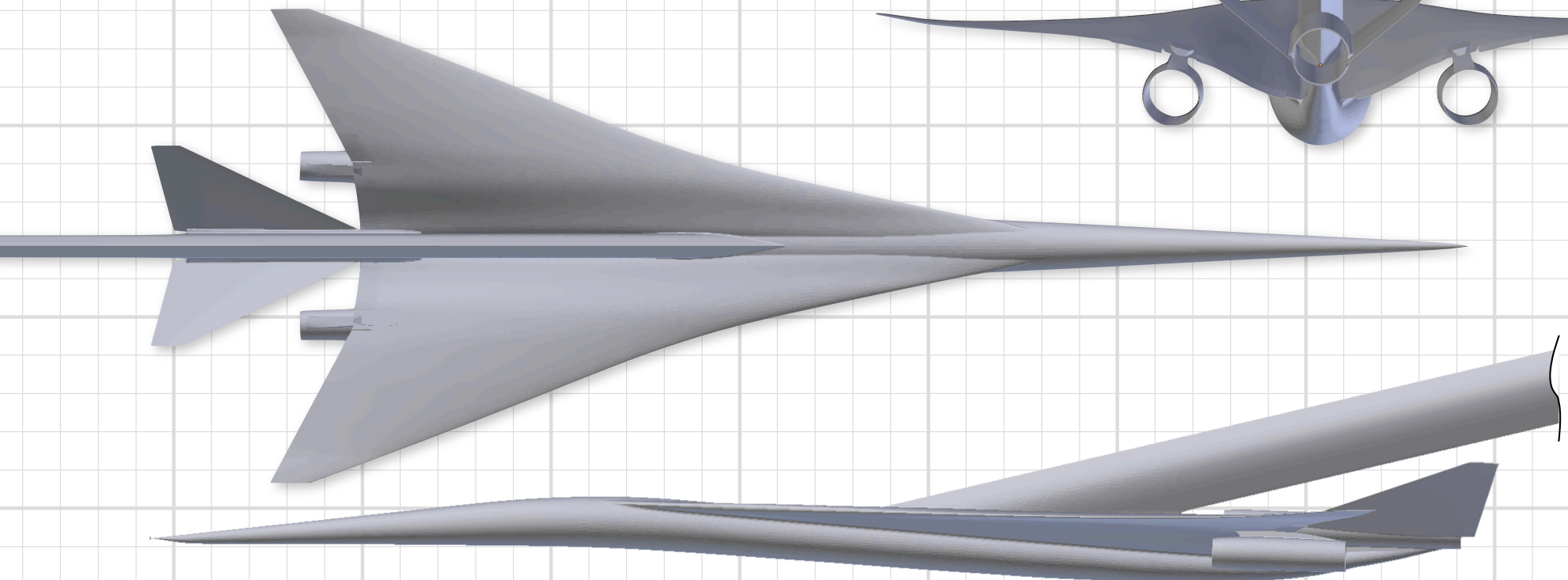
$$L_{\text{ref}} = 22.40 \text{ in}$$

$$S_{\text{ref}} = 33.18 \text{ in}^2$$

$$M_{\infty} = 1.6$$

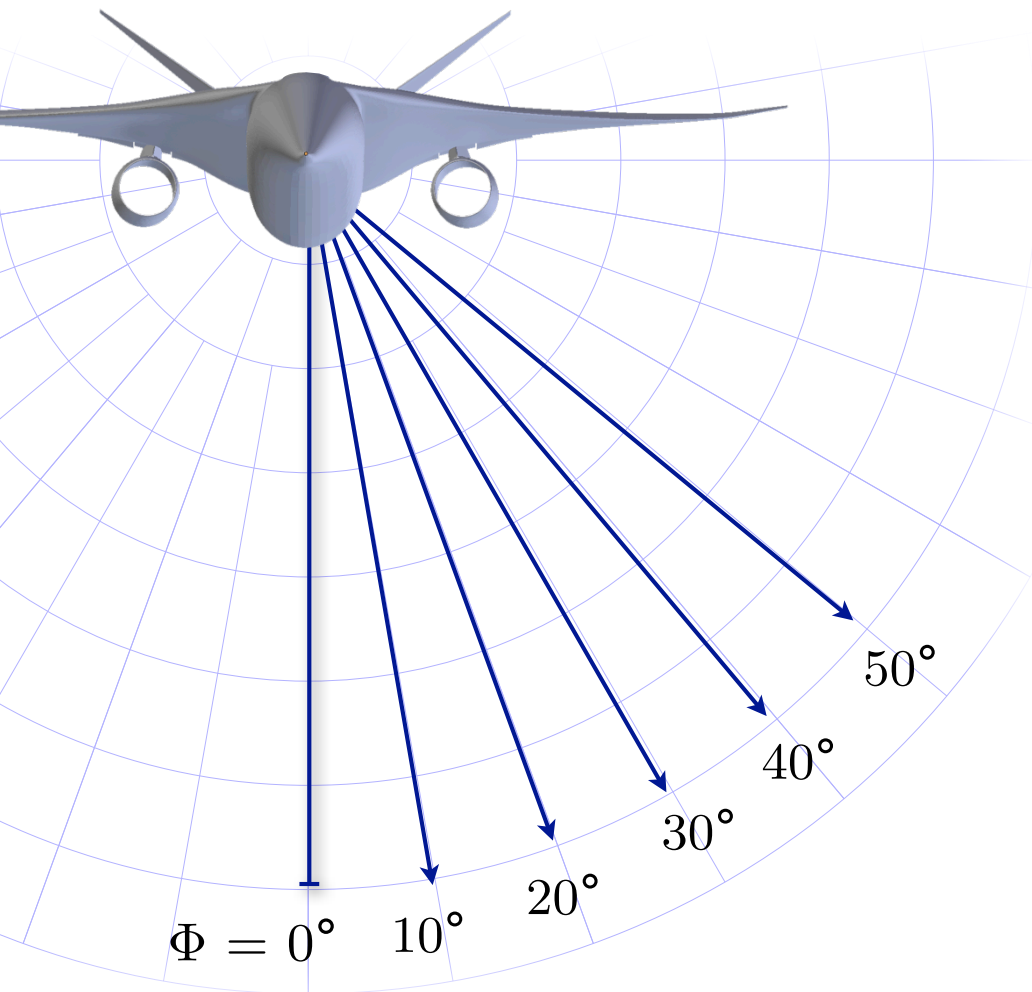
$$\alpha_{\text{cruise}} = 2.3^{\circ}$$

$$C_{L \text{ cruise}} = 0.142$$



# LM 1021: Conditions

$$M_\infty = 1.6, \alpha = 2.1^\circ$$



Extracted signatures at 30 locations

- $h = \{1.64, 2.65, 3.50, 5.83, 8.39\}$  ft
- $\Phi = \{0^\circ, 10^\circ, 20^\circ, 30^\circ, 40^\circ, 50^\circ\}$
- Single simulation for all 30 signatures
- Net functional is combination of 30 sensors

$$\mathcal{J} = \sum_{i=1}^M w_i \mathcal{J}_i \quad \text{with}$$

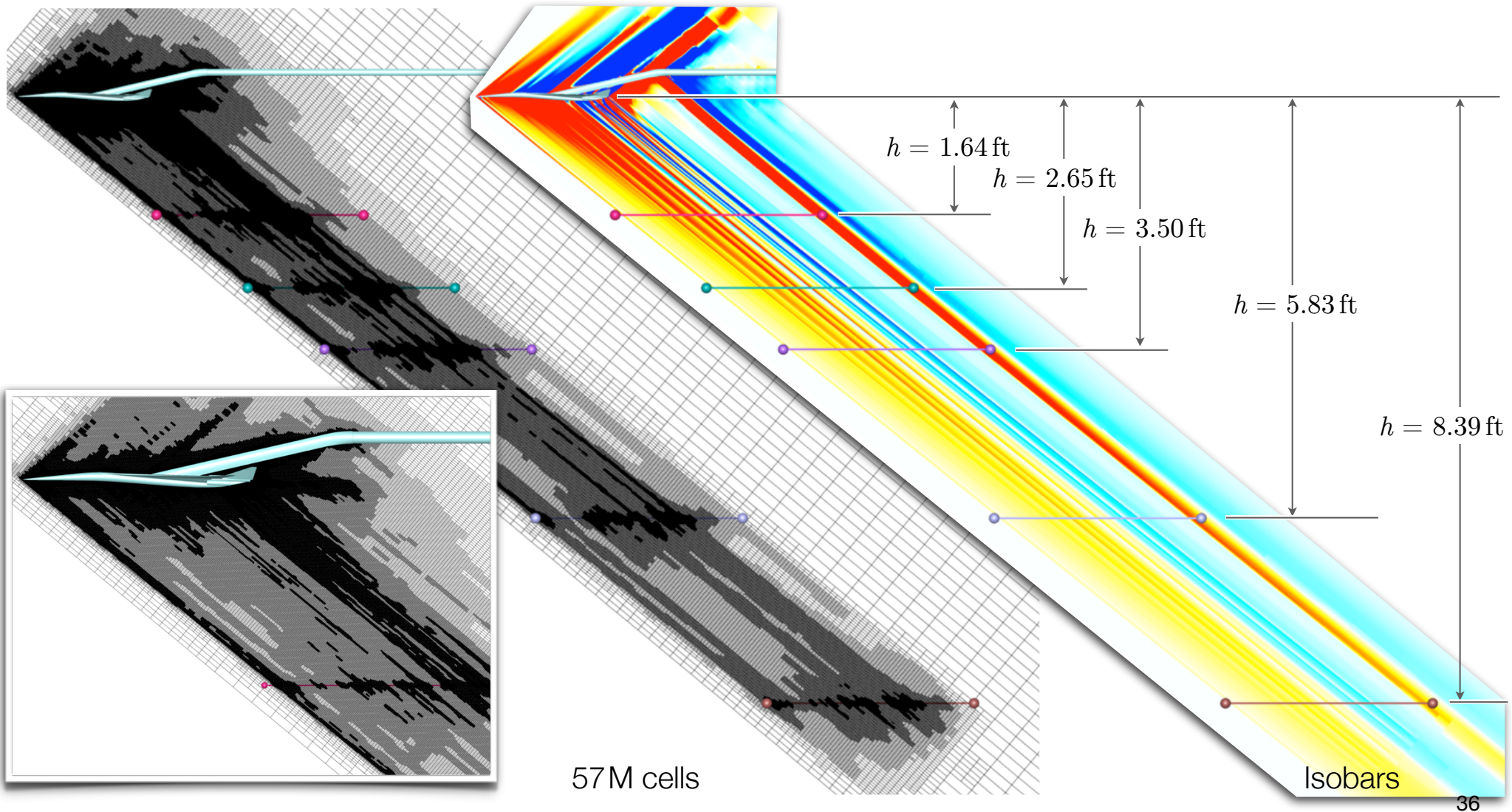
$$w_i = \frac{h_i}{L_{\text{ref}}} \left( 1 + \frac{4}{\sqrt{2}} \sin \Phi_i \right)$$

Weighting accounts for

- Decrease in signal strength w/ increasing  $h$
- Increase in resolution requirements with increasing  $\Phi$

# LM 1021: Meshing

$$M_{\infty} = 1.6, \alpha = 2.1^{\circ}$$

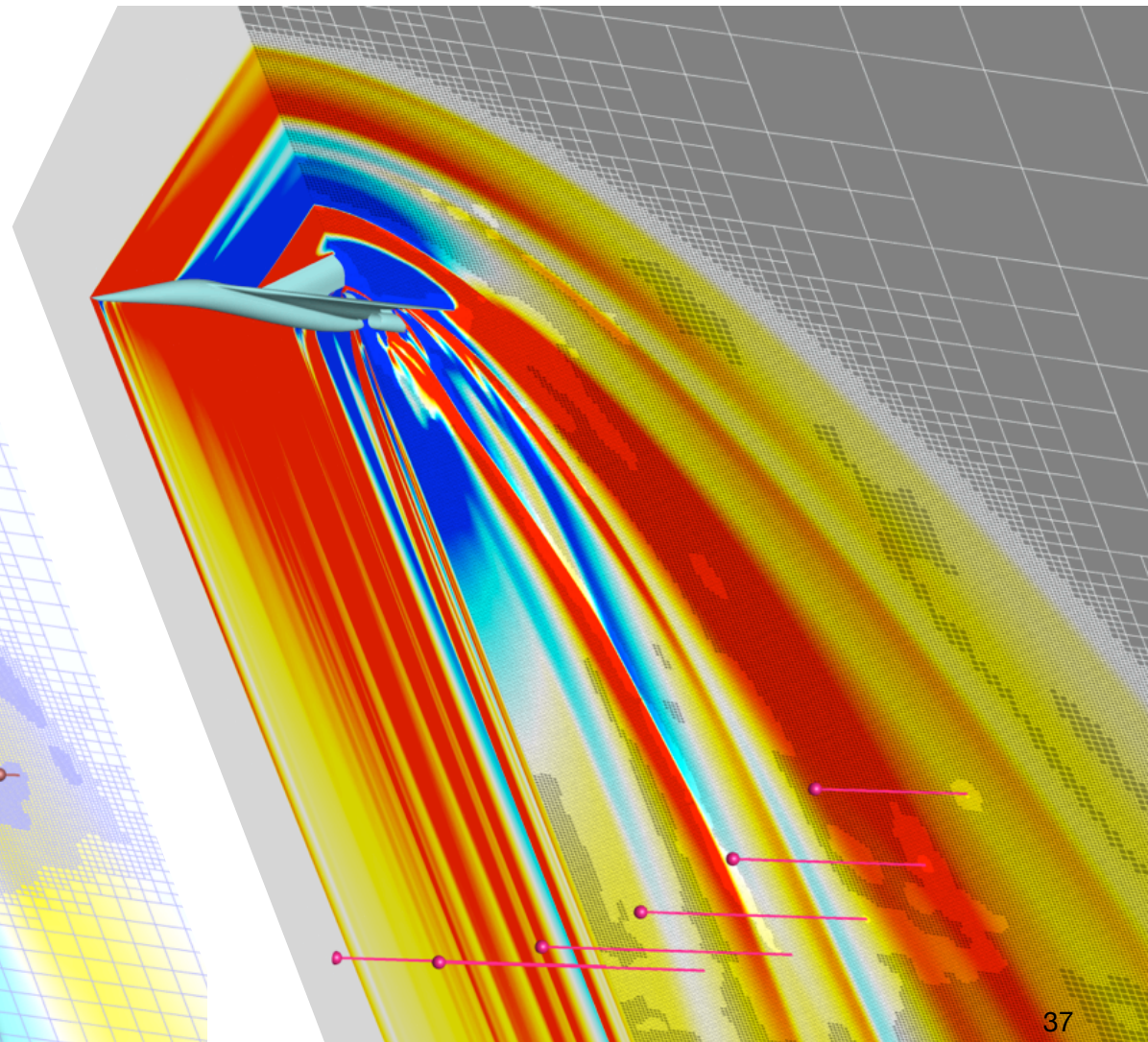
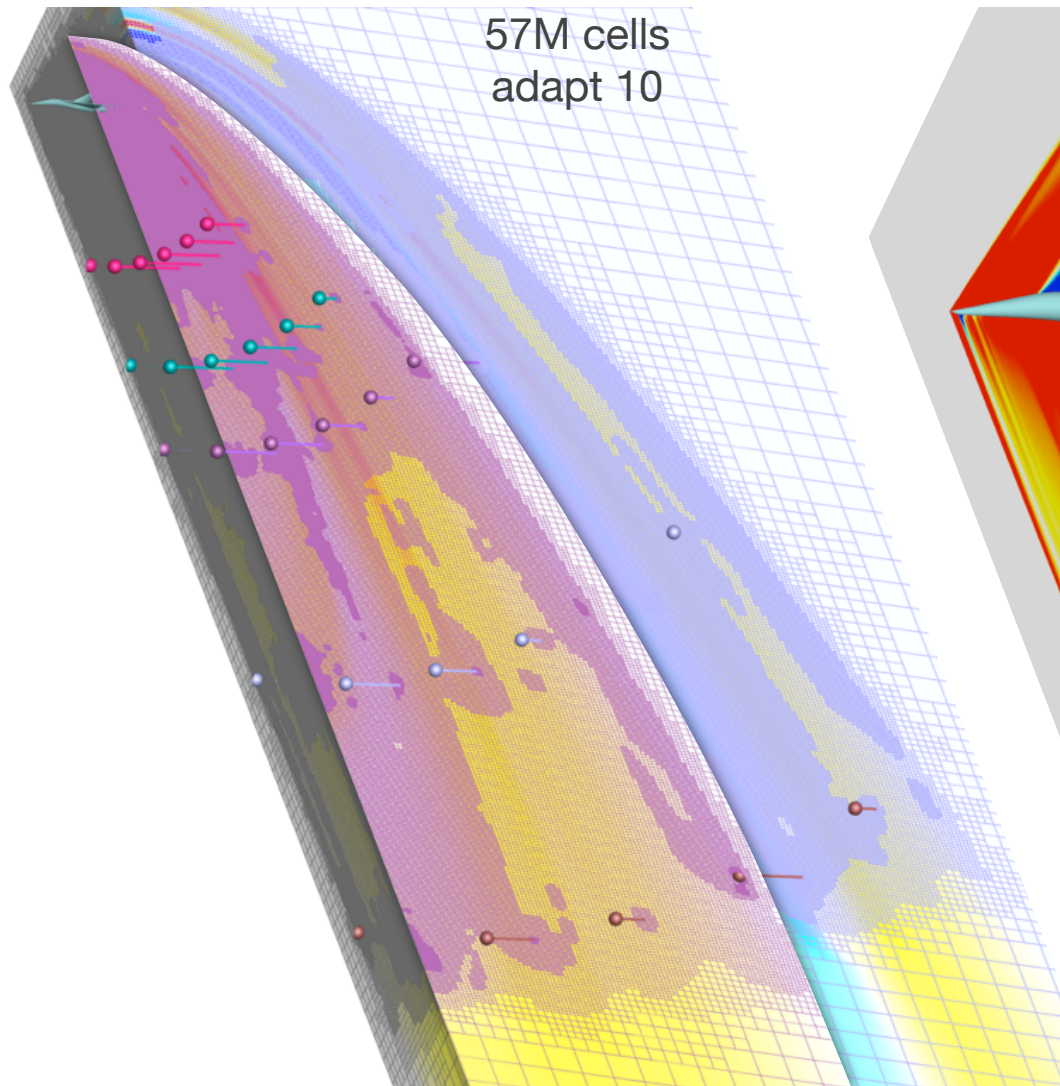




# LM 1021: Meshing

$$M_{\infty} = 1.6, \alpha = 2.1^{\circ}$$

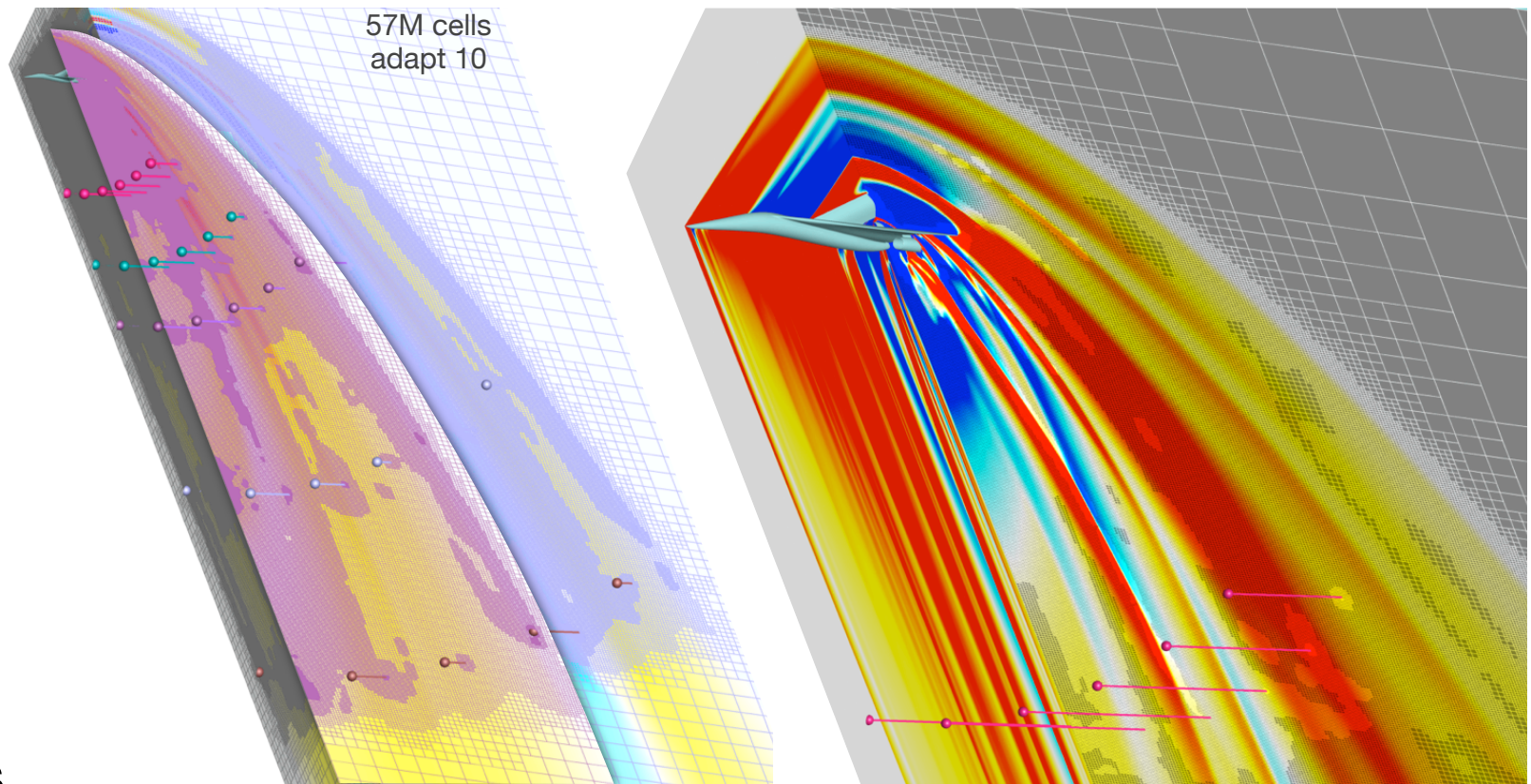
Isobars and mesh near body





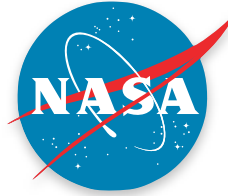
# LM 1021: Resources

$$M_{\infty} = 1.6, \alpha = 2.1^{\circ}$$



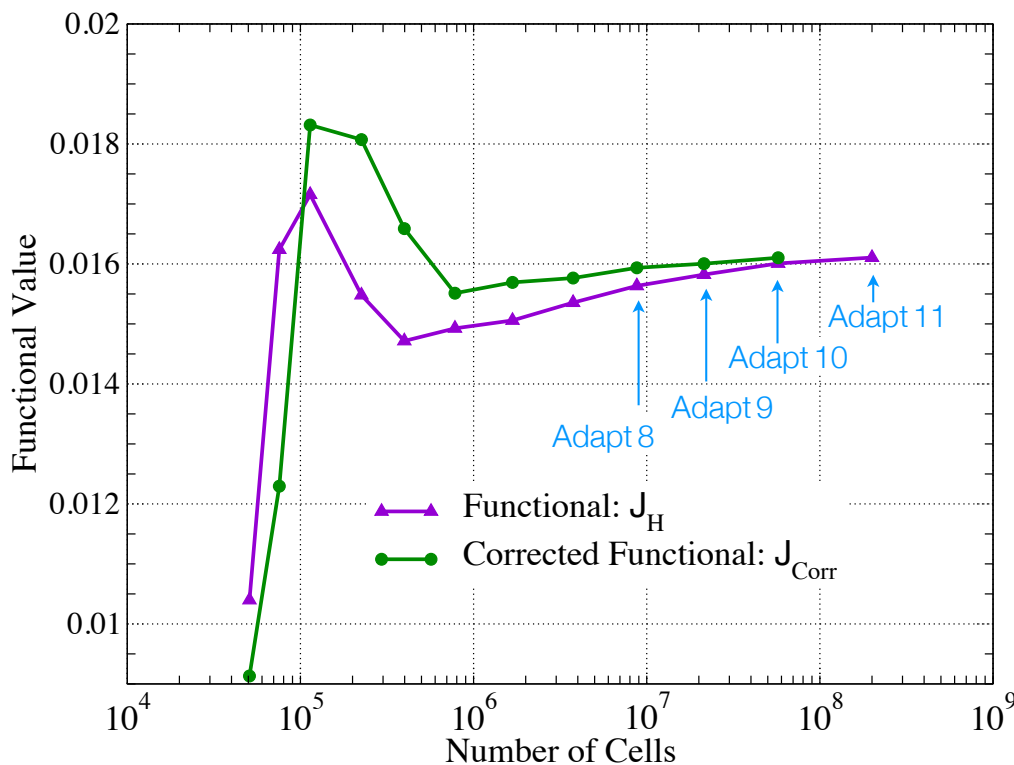
## Resources

- Run on 96 Intel sandy bridge cores (NAS's Endeavour)
- 2 hr 20 mins runtime (61 mins)
- 80 GB of memory (max)

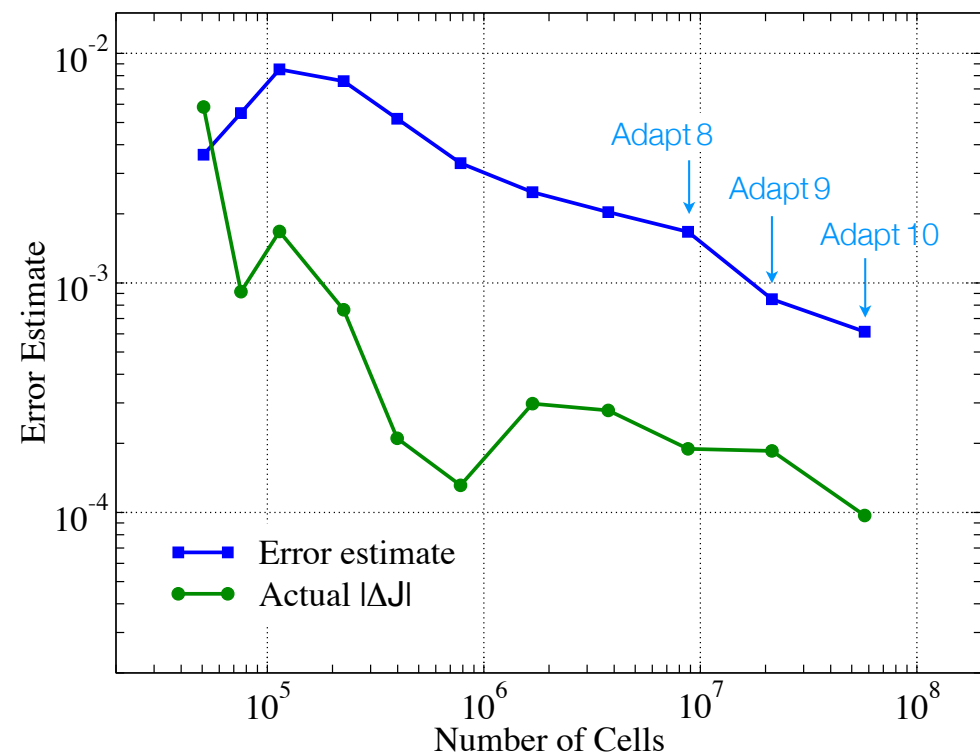


# LM 1021: Functional Convergence

- Results at 10<sup>th</sup> adaptation submitted to workshop
- Perform 2 more adaptations to assess degree of mesh convergence



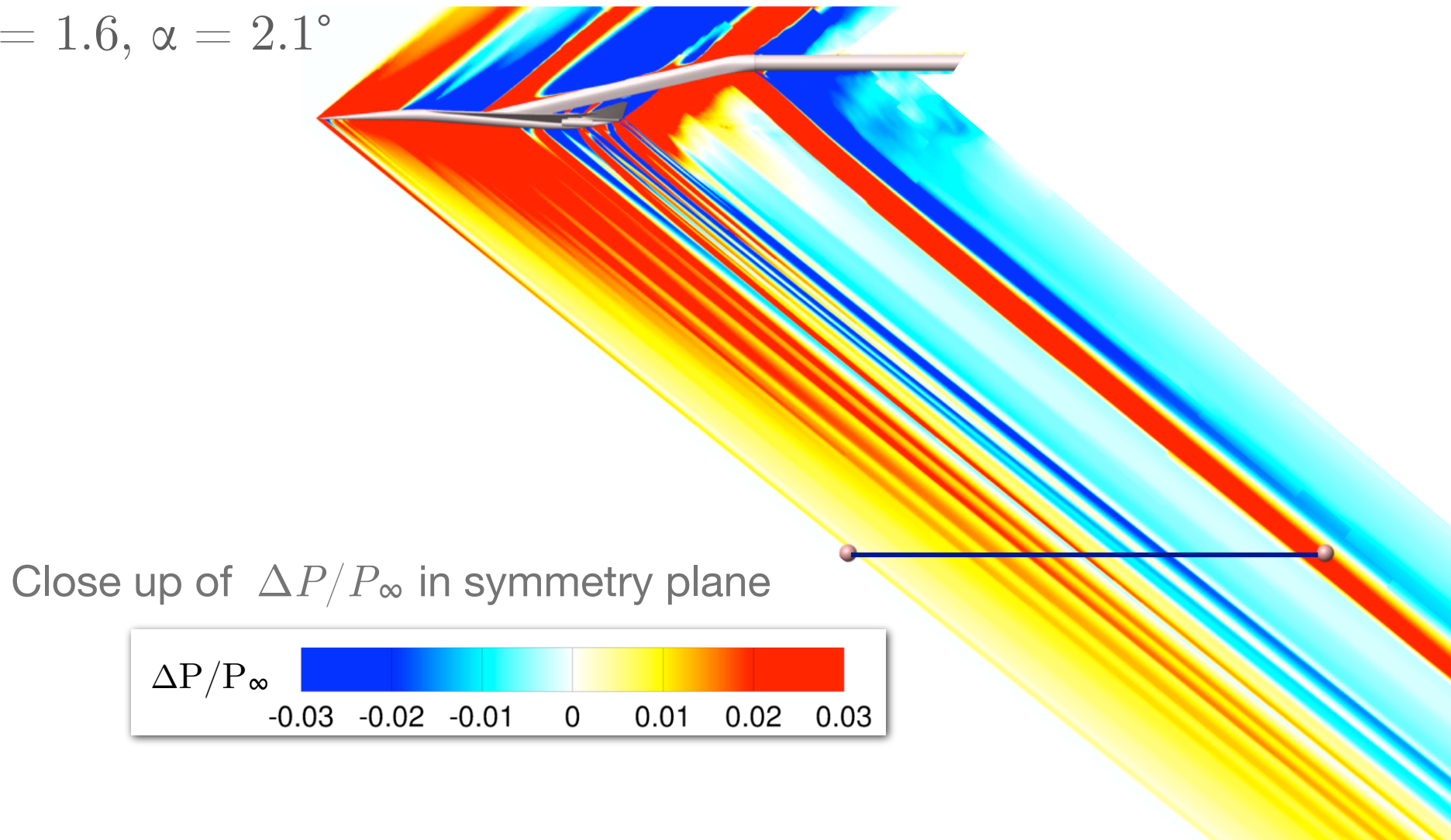
- Functional converges
- Correction *leads* functional
- Adjoint Correction vanishes



- Error-estimate bounds update |ΔJ|
- Remaining error converges asymptotically
- Very good convergence

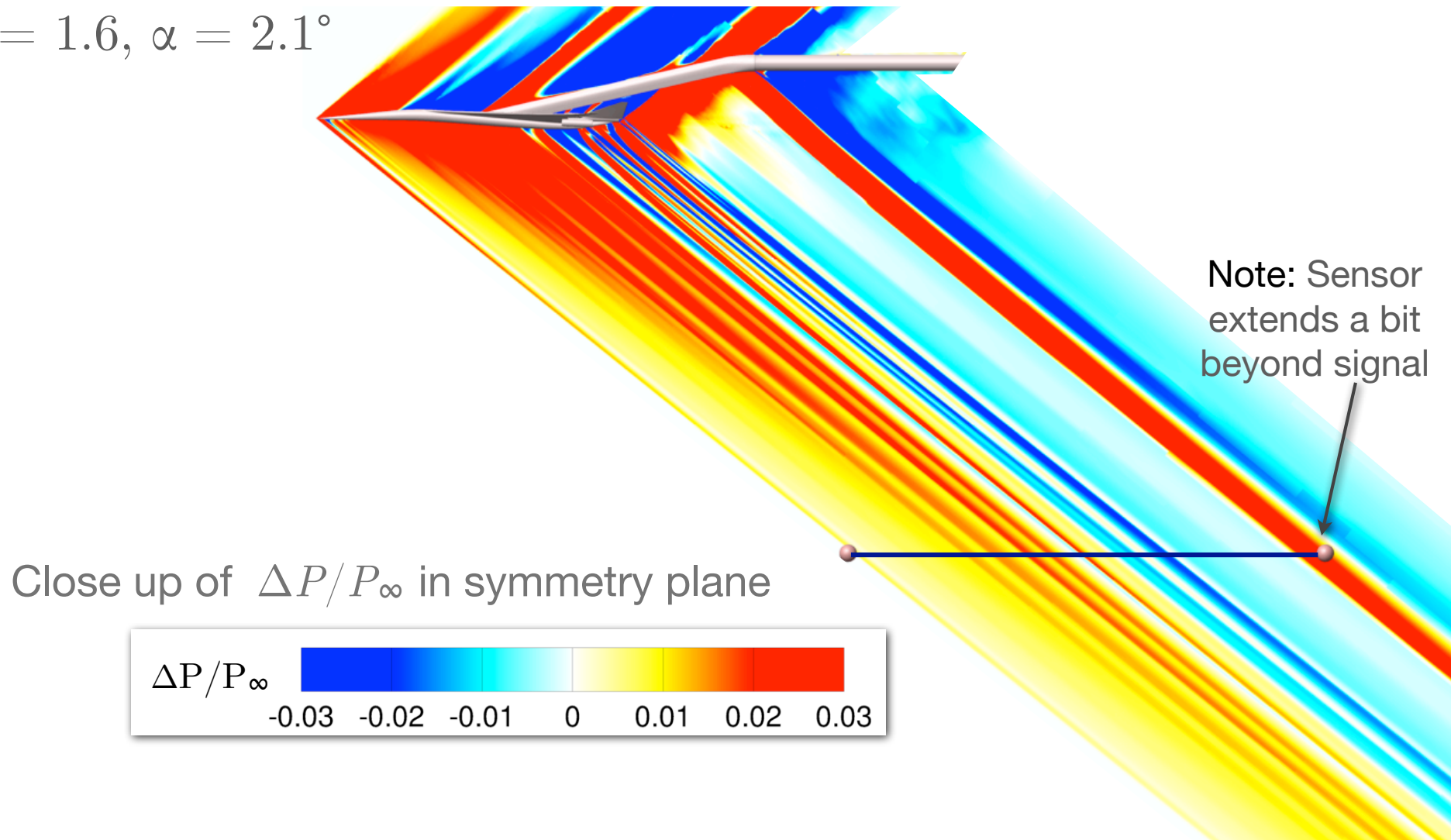
# LM 1021: Pressure field

$$M_\infty = 1.6, \alpha = 2.1^\circ$$



# LM 1021: Pressure field

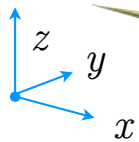
$$M_\infty = 1.6, \alpha = 2.1^\circ$$



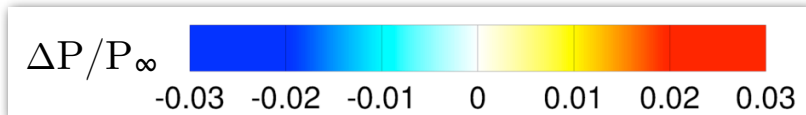


# LM 1021: Pressure Carpets

$$M_{\infty} = 1.6, \alpha = 2.1^{\circ}$$

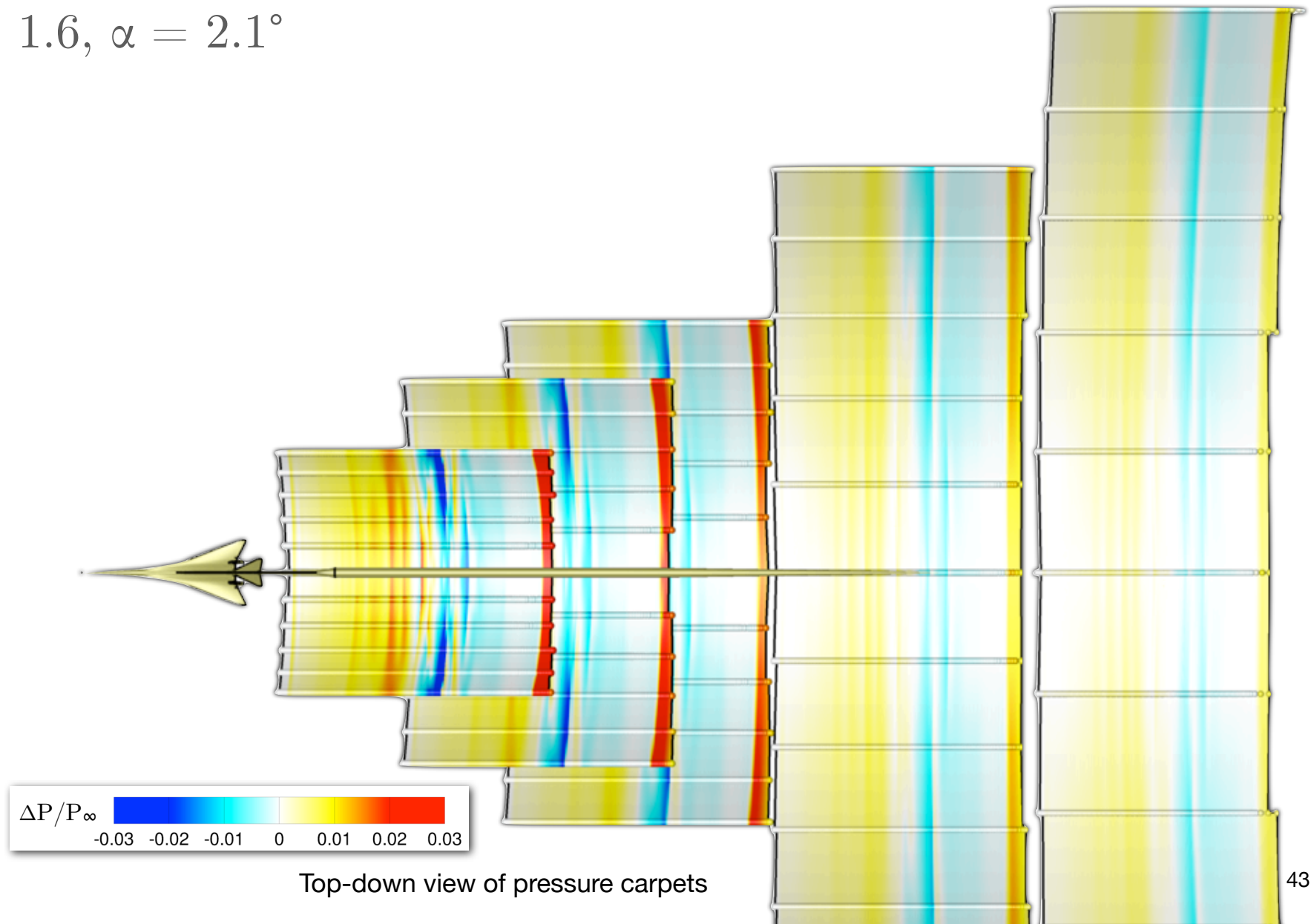


- $h = \{1.64, 2.65, 3.50, 5.83, 8.39\}$  ft
- $\Phi = \{0^{\circ}, 10^{\circ}, 20^{\circ}, 30^{\circ}, 40^{\circ}, 50^{\circ}\}$
- Construct pressure carpets by tessellating data along sensors at fixed  $h/L$



# LM 1021: Pressure Carpets

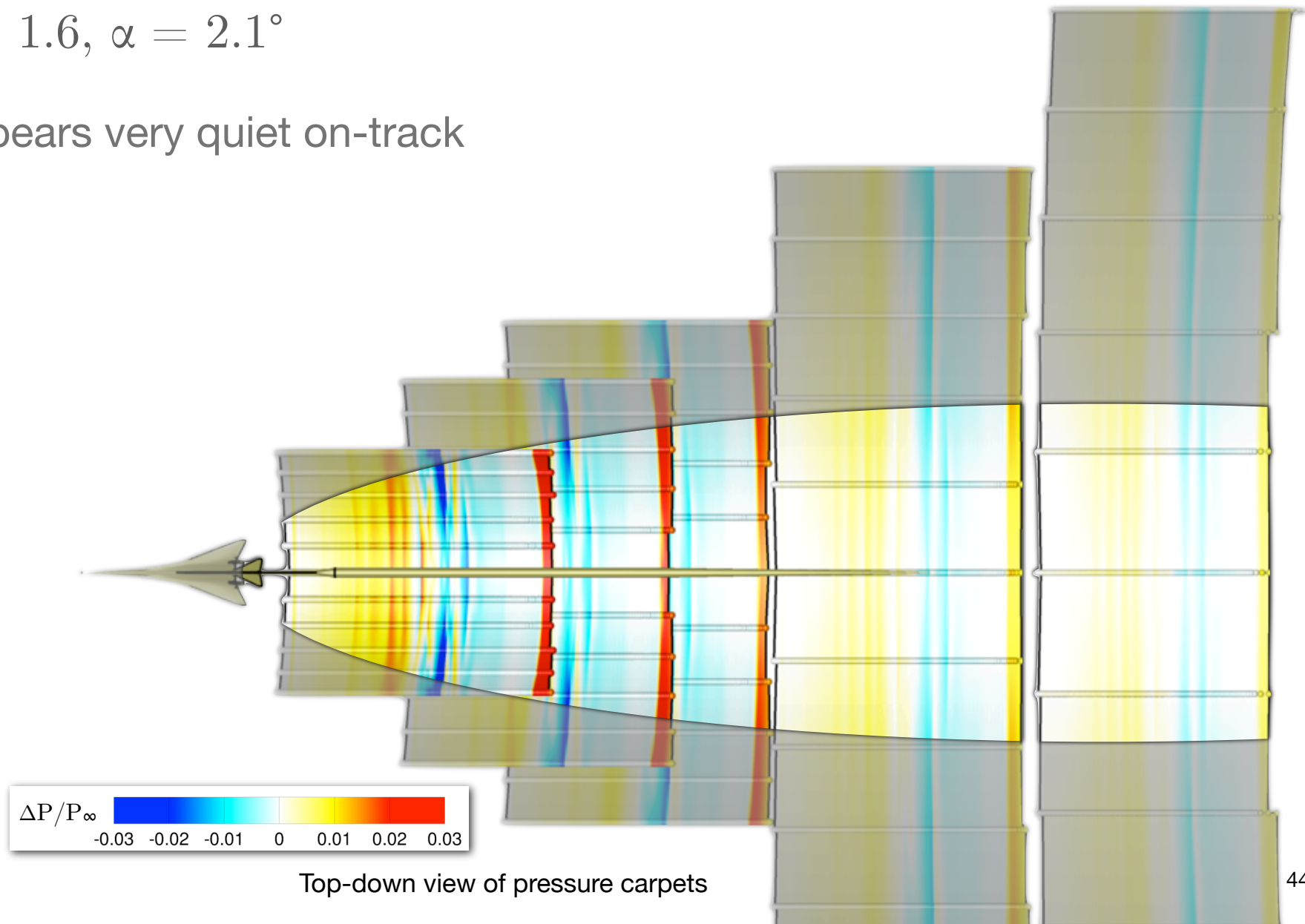
$$M_{\infty} = 1.6, \alpha = 2.1^{\circ}$$



# LM 1021: Pressure Carpets

$$M_\infty = 1.6, \alpha = 2.1^\circ$$

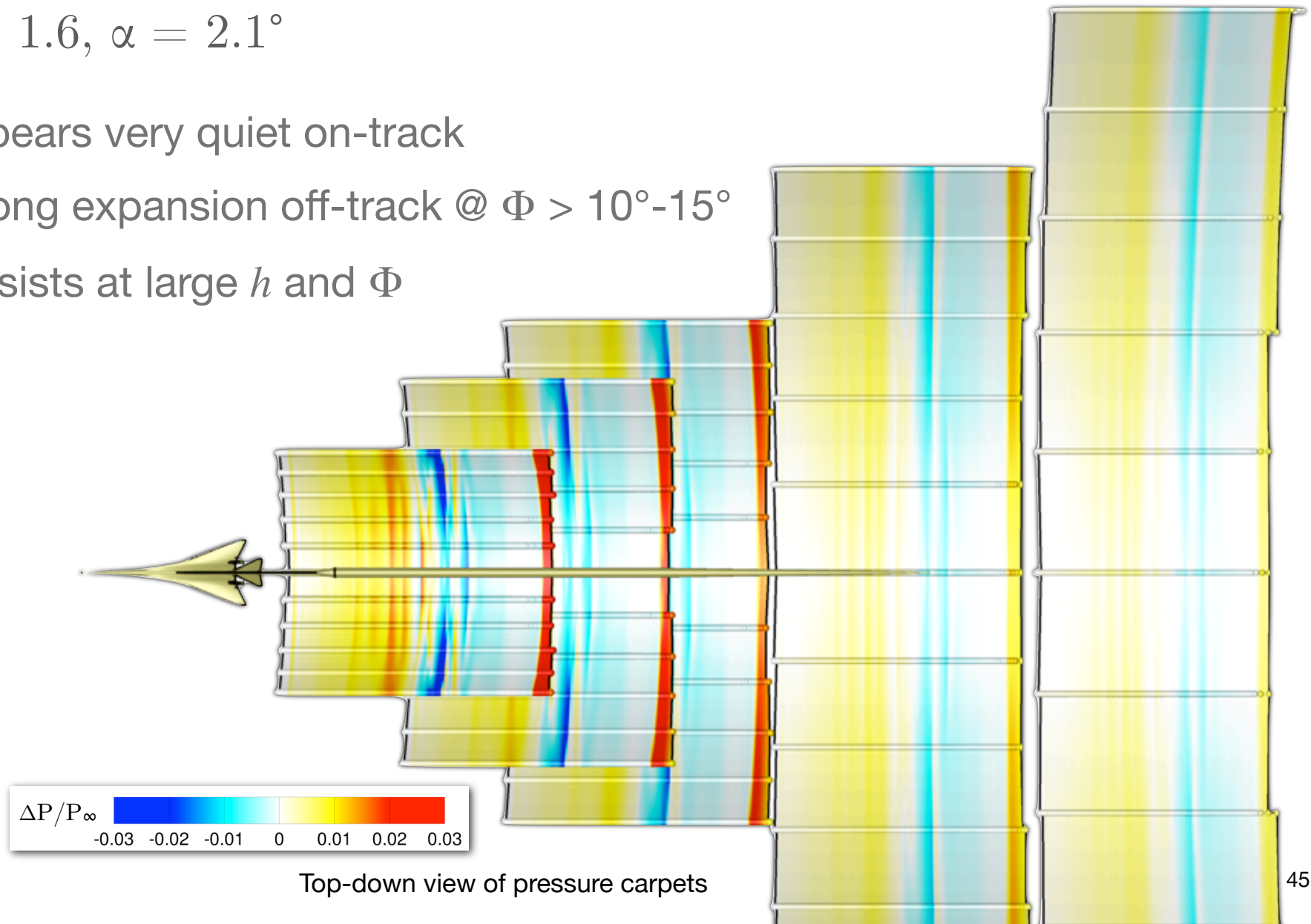
- Appears very quiet on-track



# LM 1021: Pressure Carpets

$$M_\infty = 1.6, \alpha = 2.1^\circ$$

- Appears very quiet on-track
- Strong expansion off-track @  $\Phi > 10^\circ$ - $15^\circ$
- Persists at large  $h$  and  $\Phi$

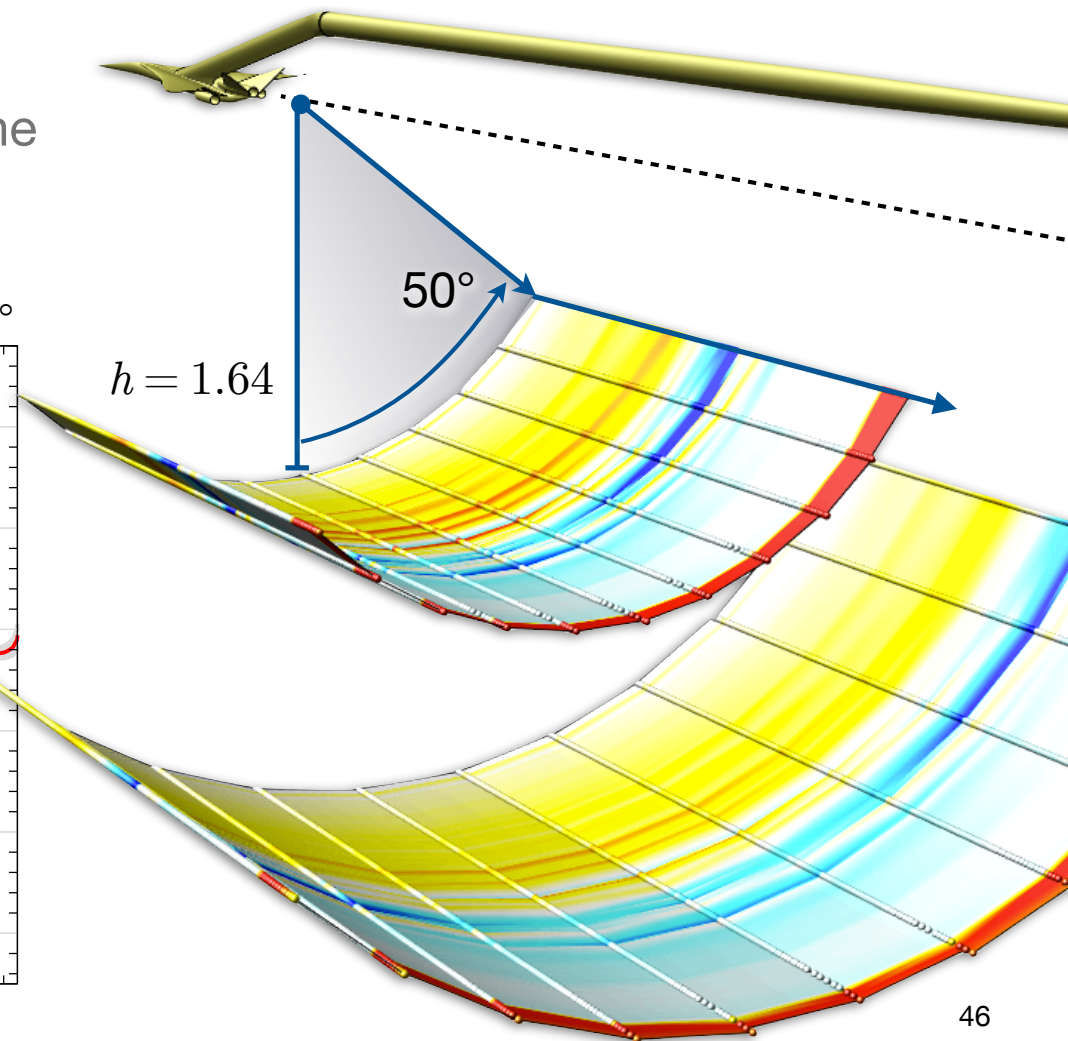
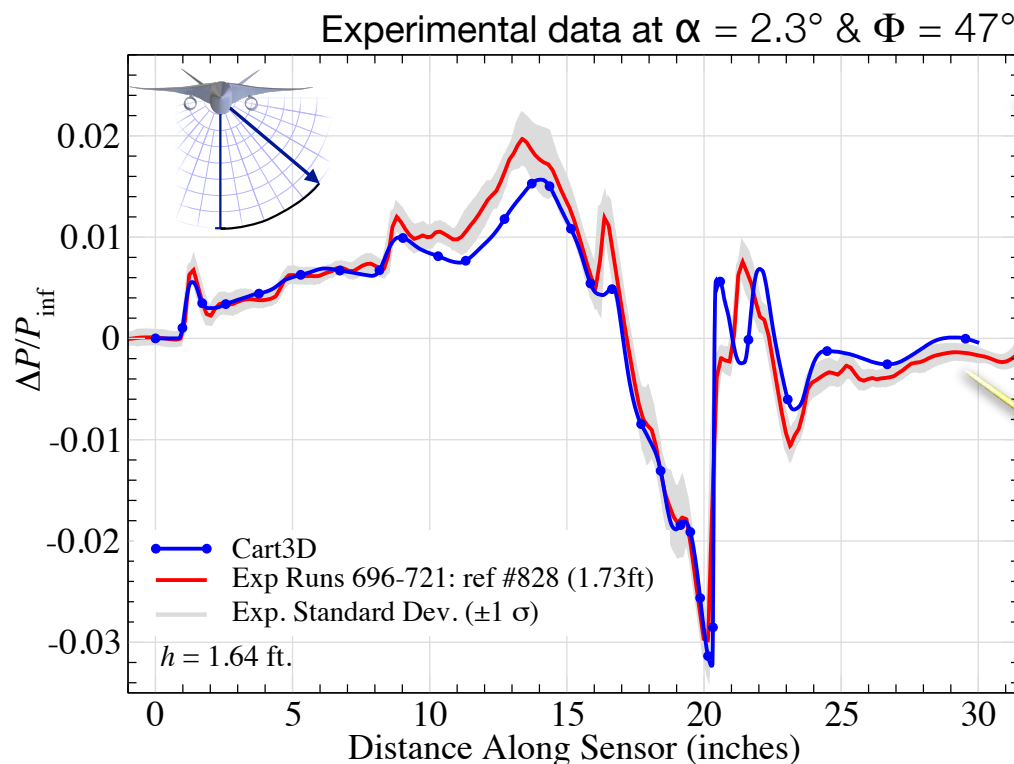




# LM 1021: Off-track Pressure Signature

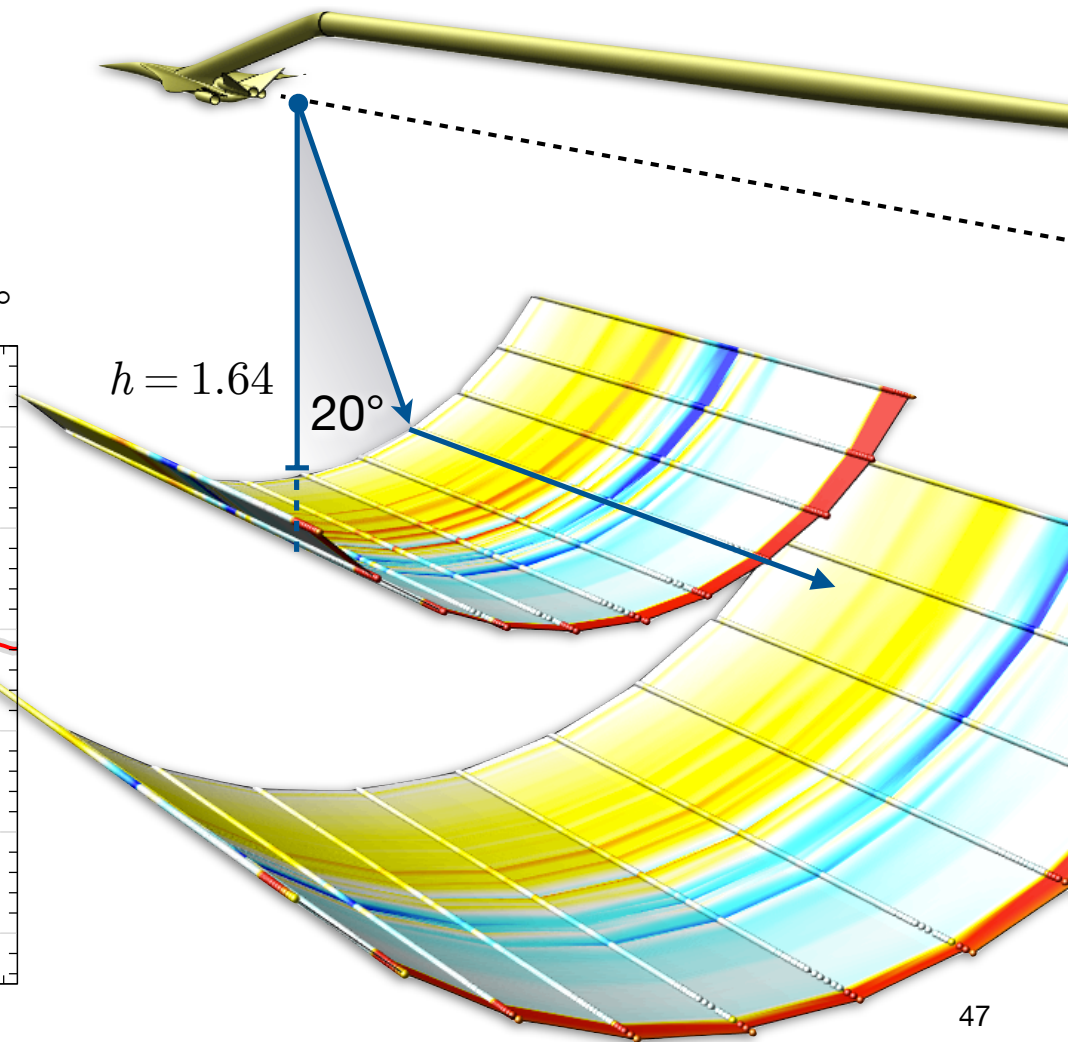
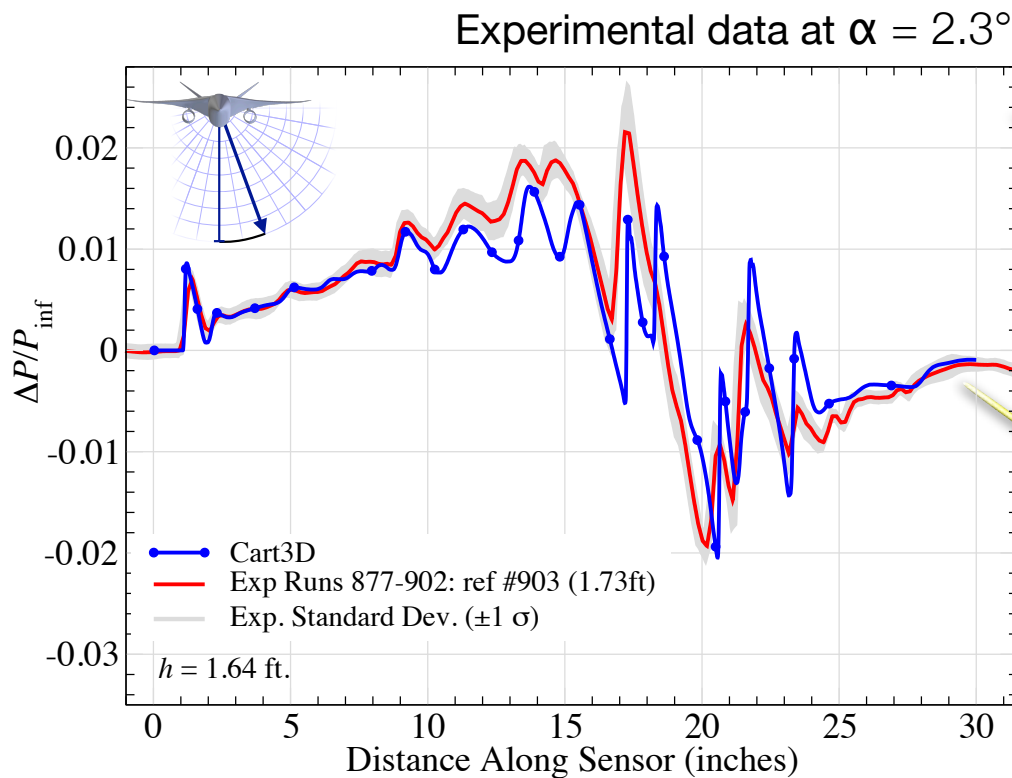
$$M_{\infty} = 1.6, \alpha = 2.1^{\circ}, \Phi = 50^{\circ}$$

- Good agreement
- Difference in alpha may account for the slightly lower peaks



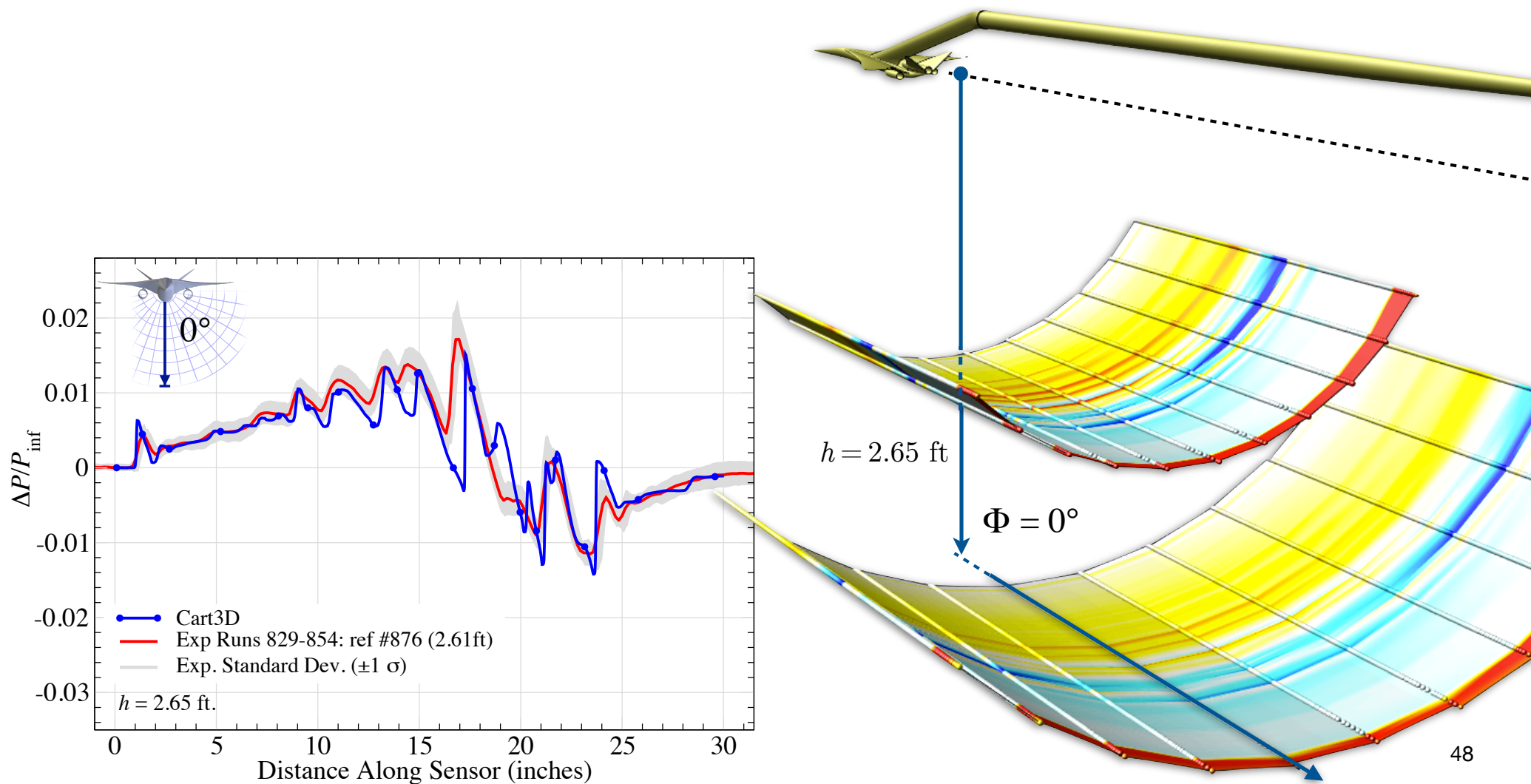
# LM 1021: Off-track Pressure Signature

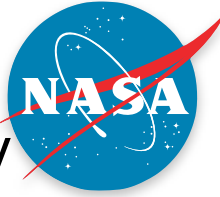
$$M_\infty = 1.6, \alpha = 2.1^\circ, \Phi = 20^\circ$$



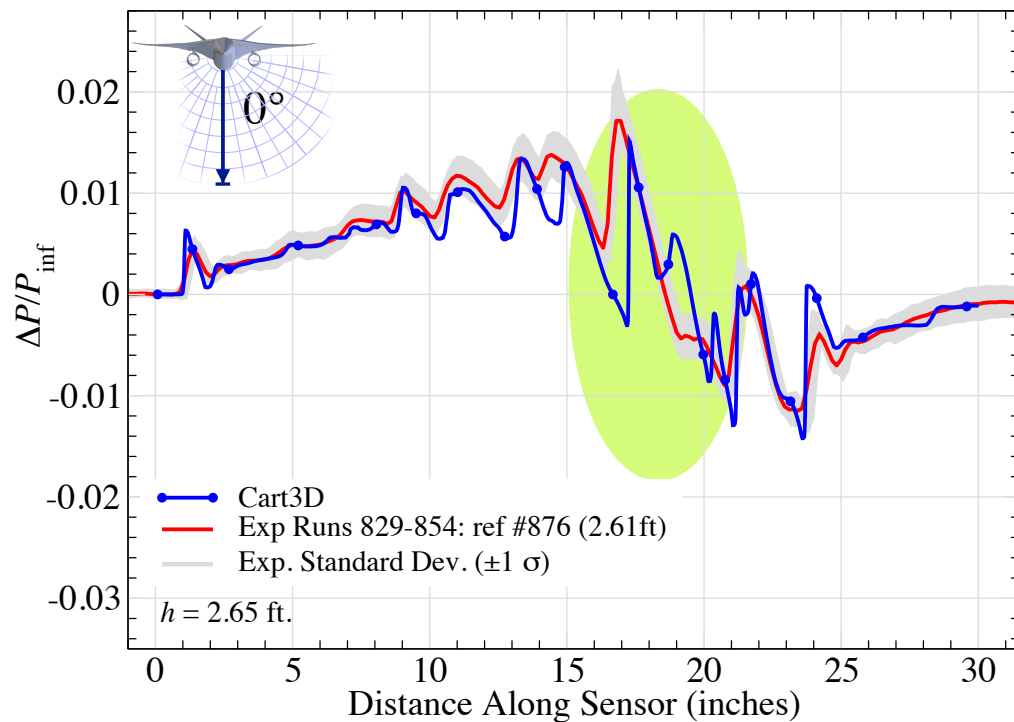
# LM 1021: On-track Pressure Signature

$$M_{\infty} = 1.6, \alpha = 2.1^{\circ}, \Phi = 0^{\circ}$$

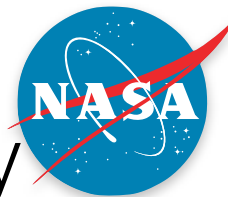




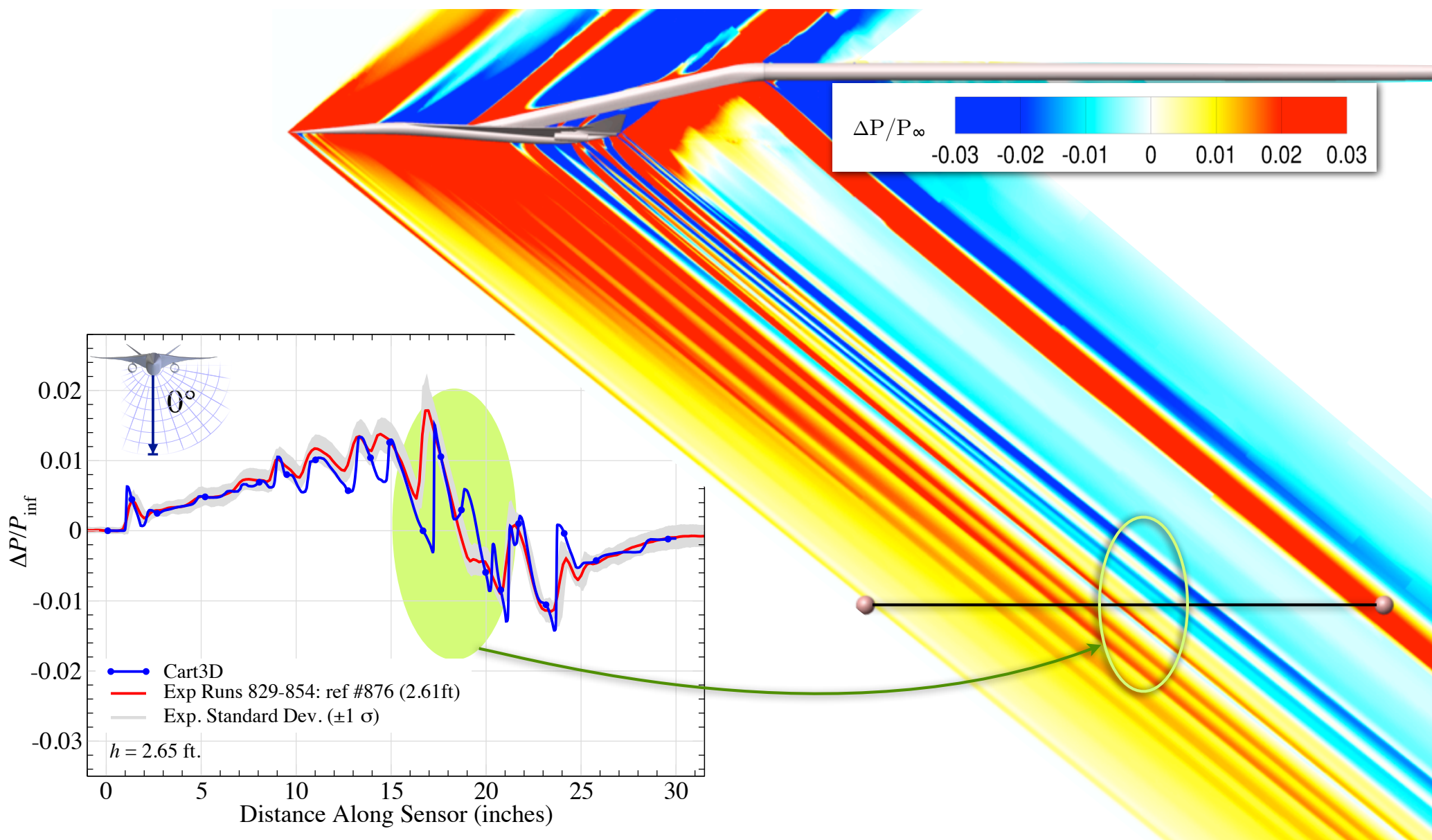
# LM 1021: Investigation of On-track Discrepancy

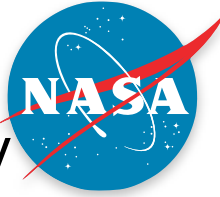




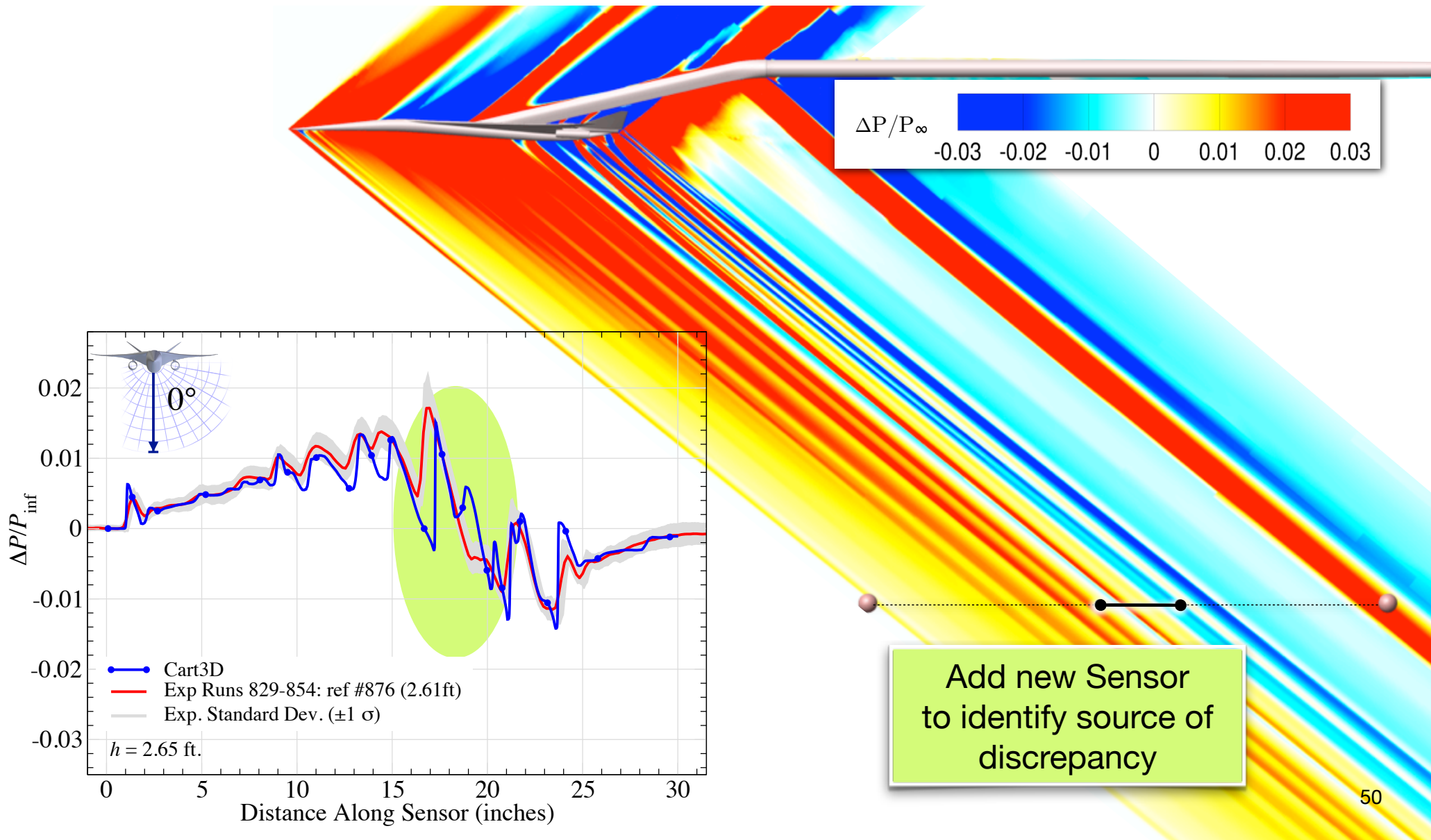


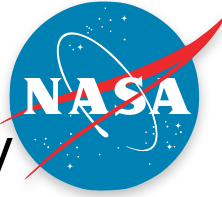
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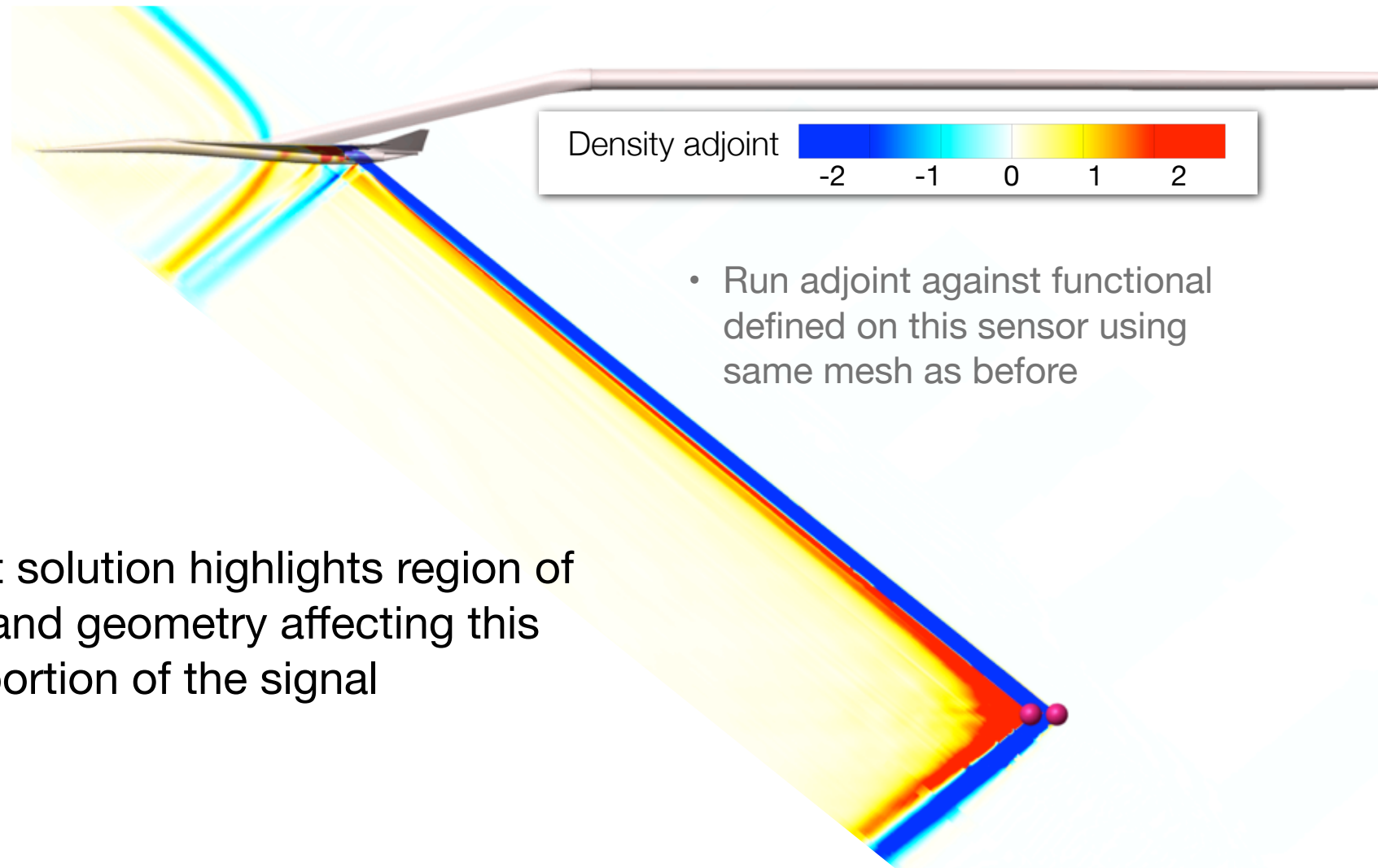


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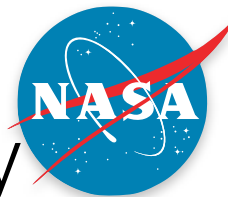




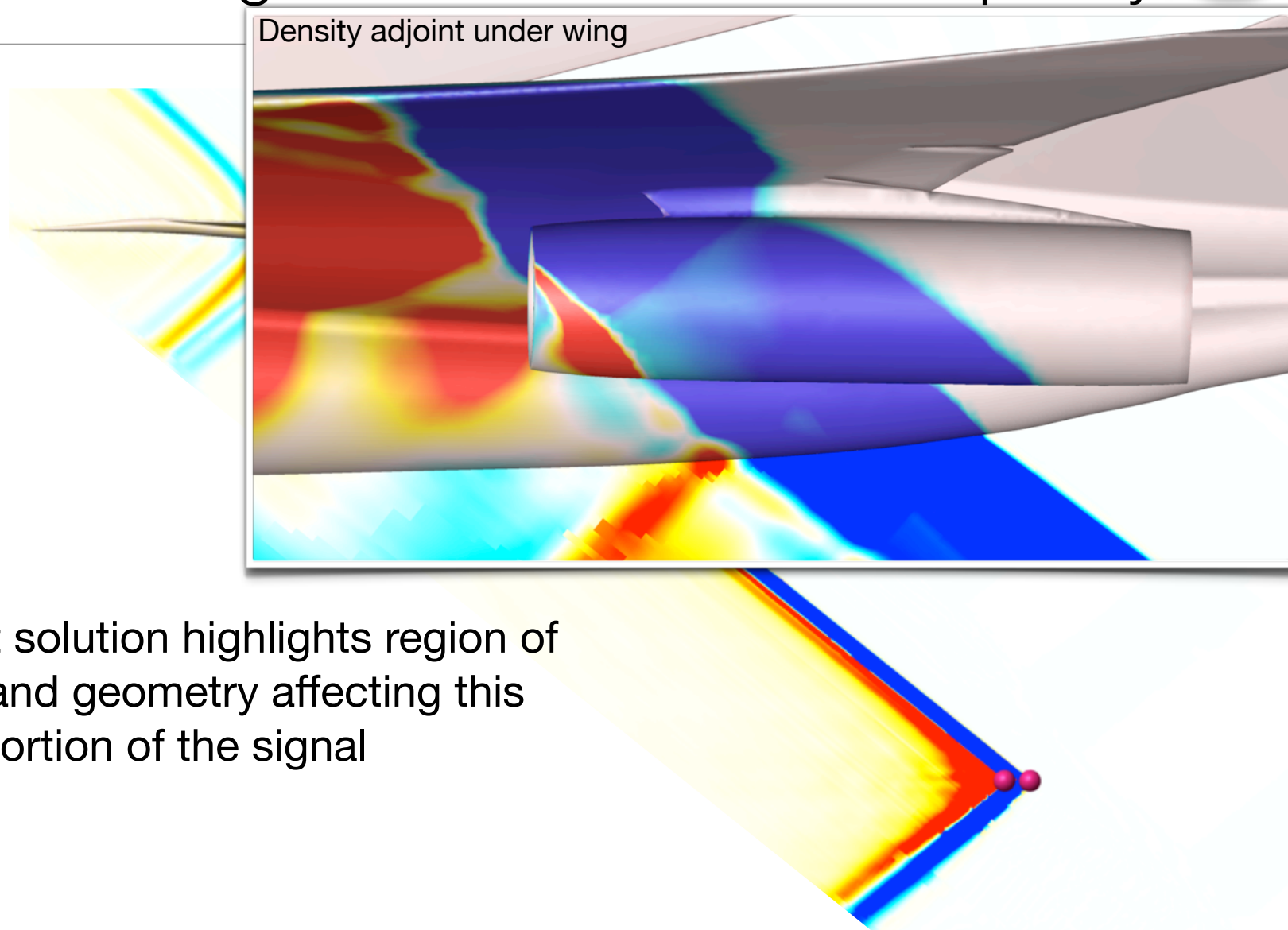
# LM 1021: Investigation of On-track Discrepancy



The adjoint solution highlights region of the flow and geometry affecting this portion of the signal



# LM 1021: Investigation of On-track Discrepancy



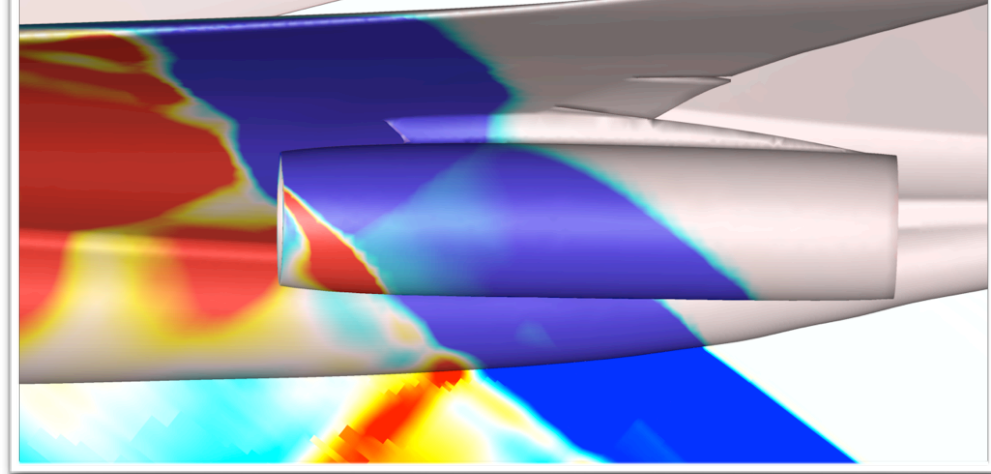
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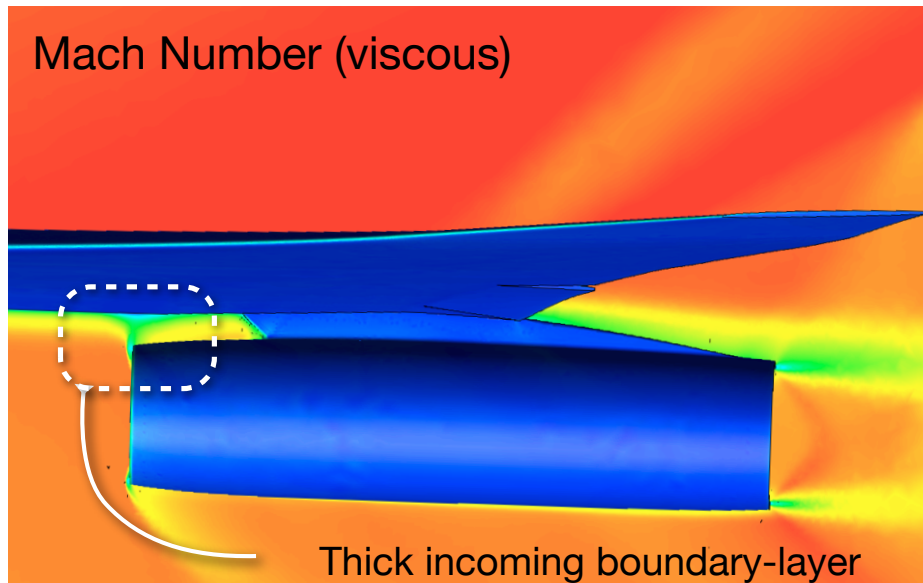
# LM 1021: Investigation of On-track Discrepancy

- Adjoint tells us where to look...
- Investigate physics of tunnel flow
- Viscous results from USM3D
- Tunnel  $Re_L$  is  $\sim 100x$  lower than flight
- Boundary layer extends to nacelle

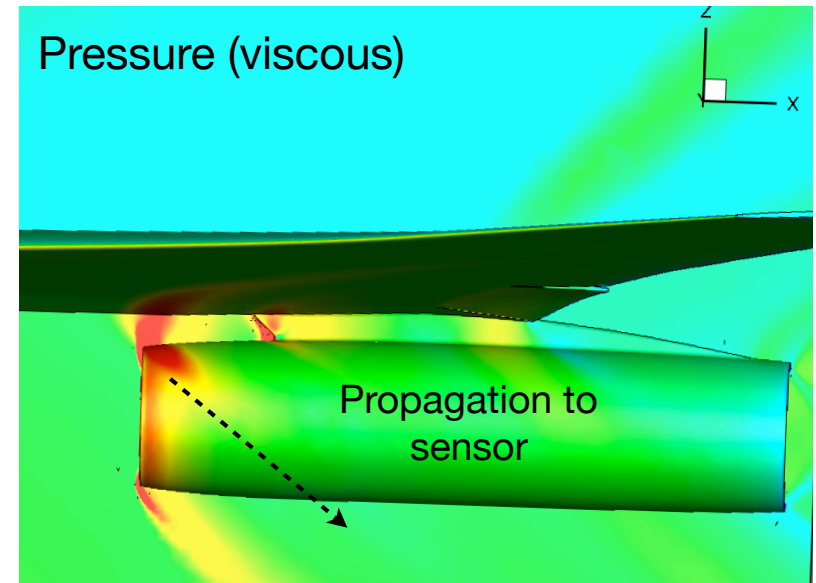
Density adjoint under wing



Mach Number (viscous)



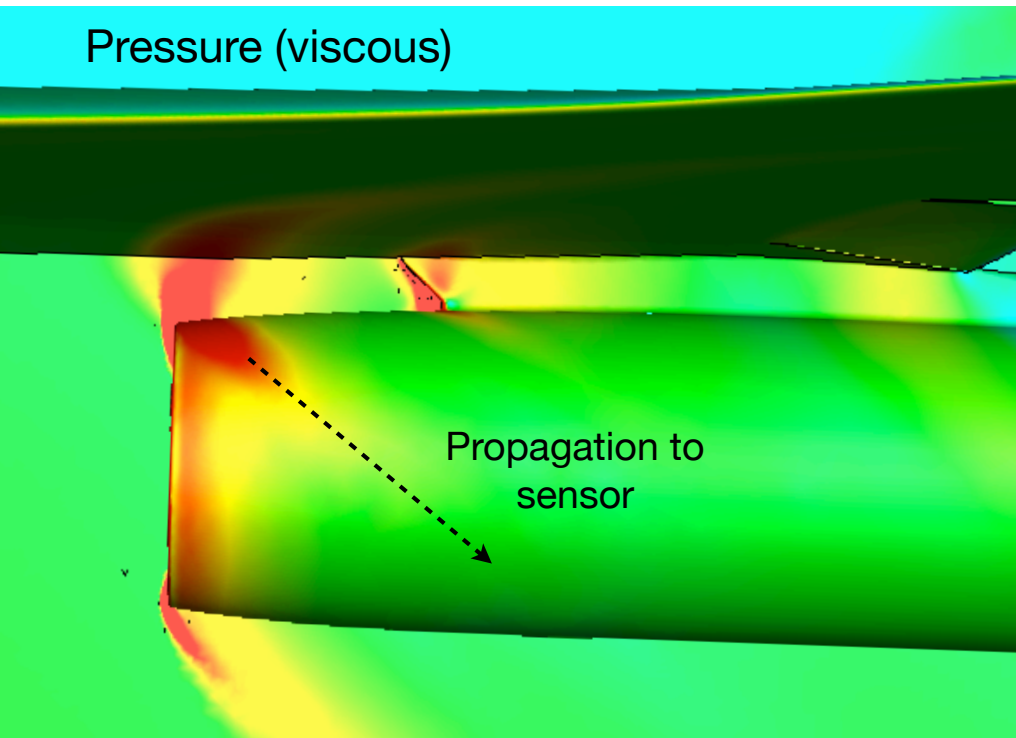
Pressure (viscous)



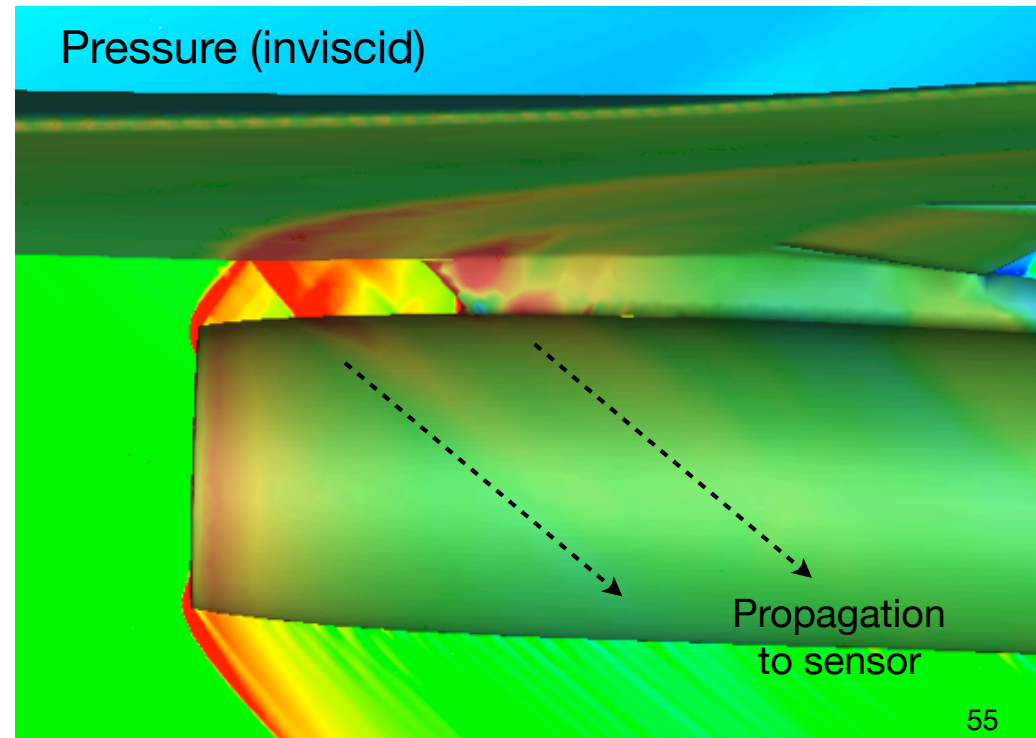
# LM 1021: Investigation of On-track Discrepancy

- Compare viscous and inviscid
- Boundary layer extends to nacelle
- Inviscid has supersonic flow between underside of wing and nacelle
- Inviscid shock is delayed (oblique)
- 2nd peak comes from pylon

Pressure (viscous)

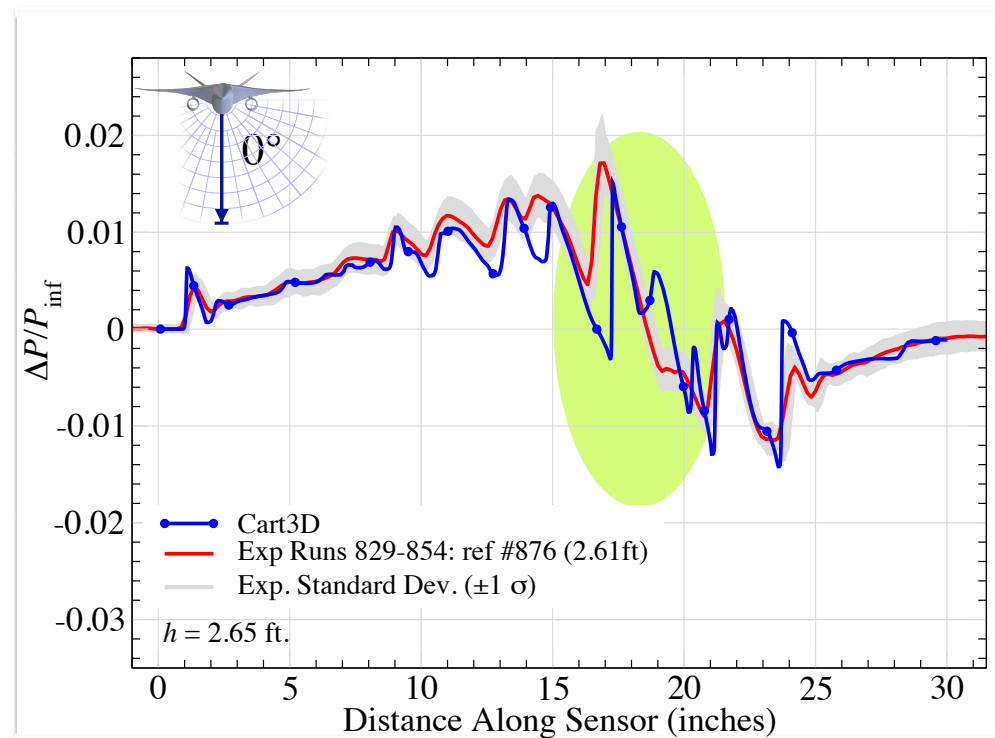


Pressure (inviscid)

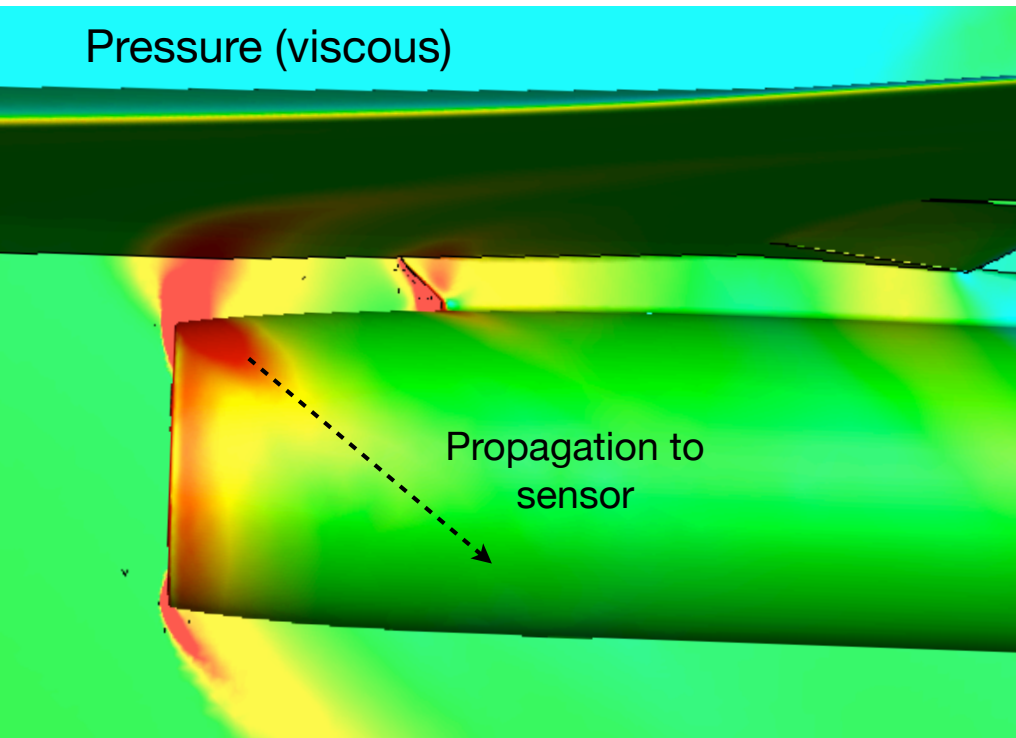


# LM 1021: Investigation of

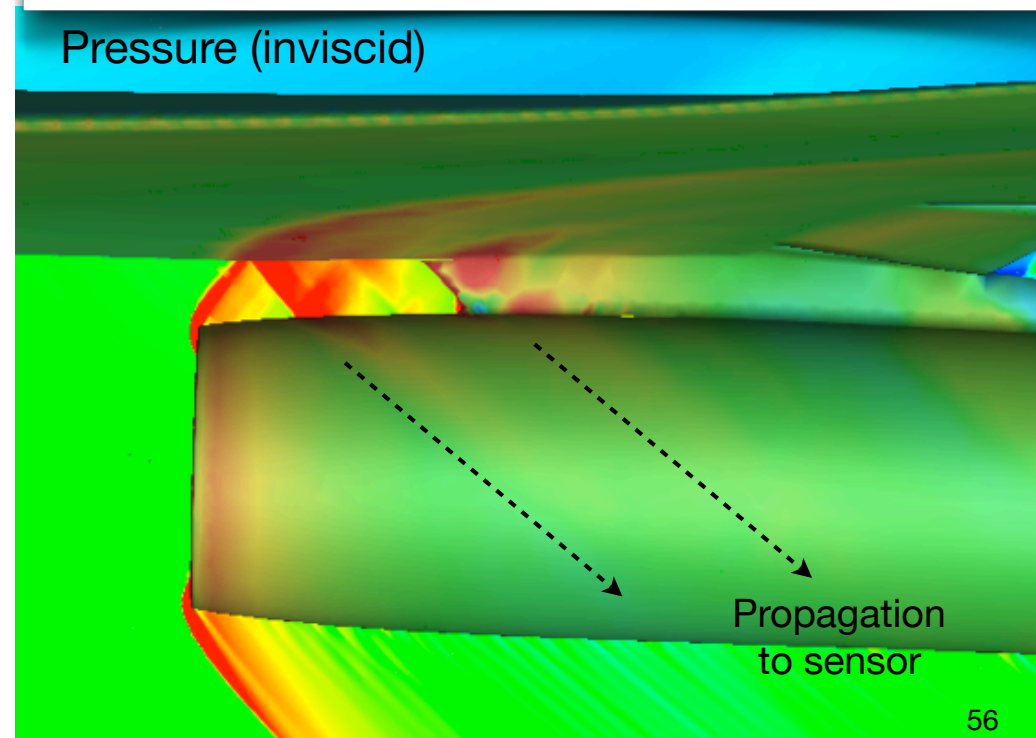
- Compare viscous and inviscid
- Boundary layer extends to nacelle
- Inviscid has supersonic flow between
- Inviscid shock is delayed (oblique)
- 2nd peak comes from pylon

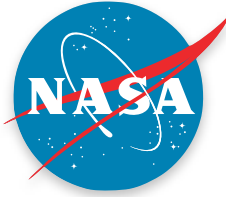


Pressure (viscous)



Pressure (inviscid)



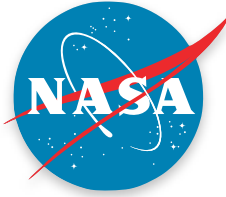


# Summary

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- Presented results for SEEB-ALR, DWB and LM 1021 using inviscid Cartesian method with
  - Automated meshing & adjoint-driven adaptation used for all cases
  - Presented evidence of mesh convergence
    - (1) Pressure signature
    - (2) Output Functional
    - (3) Adjoint correction and error estimate
  - Computational resources
    - Seeb-ALR: ~1hr on a quad-core laptop in ~3.6 Gb
    - LM 1021: Under 2.5hrs on 96 cores in 80 Gb

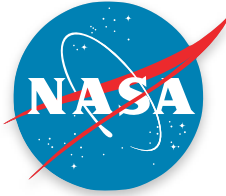




# Summary

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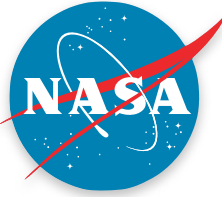
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    - Showed that differences in main expansion are likely due to influence of rail leading-edge compression impacting shoulder of model
    - Results are consistent w/ earlier studies
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    - Low tunnel Reynolds number results in differences in on-track signal
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# Thanks!

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- Fundamental Aeronautics High Speed Project for support & leadership
- Workshop Organizing committee
- Susan Cliff, Don Durston, David Rodriguez and Mathias Wintzer

# Questions?

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